

## Board of Adjustment Staff Report

Meeting Date: April 7, 2022

Agenda Item: 8A

SPECIAL USE PERMIT CASE NUMBER: WSUP22-0004 (Latour Excavation)

BRIEF SUMMARY OF REQUEST:

A grading permit for eight residential lots.

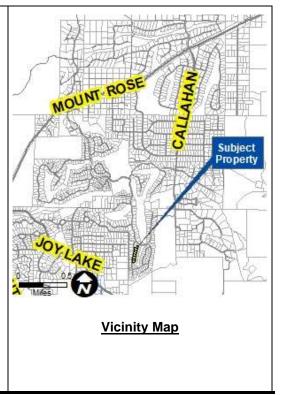
STAFF PLANNER:

Julee Olander, Planner Phone Number: 775.328.3627 Email: jolander@washoecounty.gov

## CASE DESCRIPTION

For hearing, discussion, and possible action to approve a special use permit to approve major grading of 9,150 cubic yards of cut material and 4,260 cubic yards of fill material with a net of 4,890 cubic yards to be exported and to disturb 122,204 SF (2.80 acres), for grading of eight new homes sites in the Montreux subdivision.

Applicant/Property Owner:	Ladera Ventures II, LLC.
Location:	8 lots on Latour Wy.
APN:	148-333-01, 02 & 03, 148-322-01, 02, 03, 04, & 08
Parcel Size:	0.287 to 0.510 acres
Faicei Size.	0.207 10 0.310 acres
Master Plan:	Suburban Residential (SR)
Regulatory Zone:	Low Density Suburban (LDS)
Area Plan:	Forest
Development Code:	Authorized in Articles 438, Grading and 810, Special Use Permits
Commission District:	2 – Commissioner Lucey



## STAFF RECOMMENDATION

APPROVE

APPROVE WITH CONDITIONS

DENY

#### POSSIBLE MOTION

I move that, after giving reasoned consideration to the information contained in the staff report and information received during the public hearing, the Washoe County Board of Adjustment approve with conditions Special Use Permit Case Number WSUP22-0004 for Ladera Ventures II, LLC., with the conditions included as Exhibit A to this matter, having made all five findings in accordance with Washoe County Code Section 110.810.30

(Motion with Findings on Page 7)

## Staff Report Contents

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Public Notice	Exhibit C
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## Special Use Permit

The purpose of a special use permit is to allow a method of review to identify any potential harmful impacts on adjacent properties or surrounding areas for uses that may be appropriate within a regulatory zone; and to provide for a procedure whereby such uses might be permitted by further restricting or conditioning them to mitigate or eliminate possible adverse impacts. If the Board of Adjustment grants an approval of the special use permit, that approval is subject to conditions of approval. Conditions of approval are requirements that need to be completed during different stages of the proposed project. Those stages are typically:

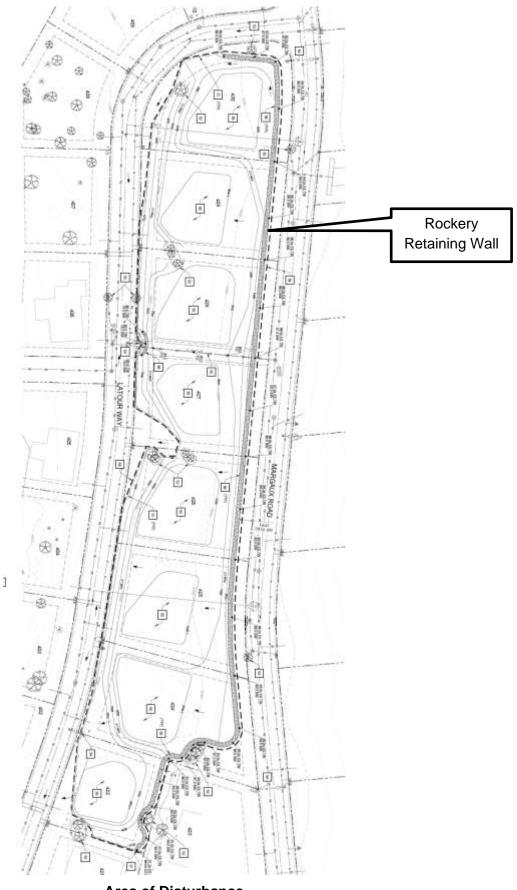
- Prior to permit issuance (i.e., a grading permit, a building permit, etc.)
- Prior to obtaining a final inspection and/or a certificate of occupancy on a structure
- Prior to the issuance of a business license or other permits/licenses
- Some conditions of approval are referred to as "operational conditions." These conditions must be continually complied with for the life of the business or project.

The conditions of approval for Special Use Permit Case Number WSUP22-0004 are attached to this staff report and will be included with the action order.

The subject property is designated as Low Density Suburban (LDS). The proposed grading is permitted with a special use permit per WCC 110.438.35. The applicant is seeking approval of this SUP from the Board of Adjustment.



Site Plan



Area of Disturbance

## Project Evaluation

The applicant is requesting a special use permit for major grading to prepare 8 lots for a new single-family development. These lots are located within the Montreux development, which is an approved residential subdivision. The proposed grading exceeds the major grading requirements for volume per 110.438.35(a)(1), Grading on slopes less than or flatter than 15%. The applicant is proposing to disturb 122,204 SF (2.80 acres) and cut 9,150 CY of material and fill 4,260 CY with a net of 4,890 CY to be exported from the site.

The applicant indicates that the grading is needed to be completed before the construction of rockery retaining wall, which will be up to 7-feet high and will cross property lines. The wall will be constructed along the backside of the properties adjacent to Margaux Road. The applicant will also be grading the 8 residential pads to prepare the sites for foundations on each lot. The foundations will be constructed after the retaining wall has been completed.

## **Reviewing Agencies**

The following agencies/individuals received a copy of the project application for review and evaluation.

Agency	Sent to Review	Responded	Provided Conditions	Contact
Washoe County	$\boxtimes$	$\boxtimes$	$\boxtimes$	Robert Wimer,
Engineering				rwimer@washoecounty.gov
WCHD – Air Quality	$\boxtimes$	$\boxtimes$		Genine Rosa,
-				grosa@washoercounty.us
WCHD – Environment	$\boxtimes$	$\boxtimes$		James English,
Health				jenglish@washocounty.gov
Washoe County Water	$\boxtimes$	$\boxtimes$		Timber Weiss,
Management	_	_		tweiss@washoecounty.gov
RTC Washoe	$\boxtimes$			
Washoe Storey	X			Jim Shaffer,
Conservation District	1			shafferjam51@gmail.com

All conditions required by the contacted agencies can be found in Exhibit A, Conditions of Approval.

## **Staff Comment on Required Findings**

WCC Section 110.810.30, Article 810, *Special Use Permits*, requires that all of the following findings be made to the satisfaction of the Washoe County Board of Adjustment before granting approval of the request. Staff has completed an analysis of the special use permit application and has determined that the proposal is in compliance with the required findings as follows.

(a) <u>Consistency.</u> That the proposed use is consistent with the action programs, policies, standards and maps of the Master Plan and the Forest Area Plan.

<u>Staff Comment:</u> Staff has reviewed the Master Plan and the Forest Area Plan and the project is consistent with these plans.

(b) <u>Improvements.</u> That adequate utilities, roadway improvements, sanitation, water supply, drainage, and other necessary facilities have been provided, the proposed improvements are properly related to existing and proposed roadways, and an adequate public facilities determination has been made in accordance with Division Seven. <u>Staff Comment:</u> The applicant is proposing to grade 8 residential lots to prepare the lots for further development. All required utilities and improvements have been planned on and will be a part of future permitting.

(c) <u>Site Suitability.</u> That the site is physically suitable grading and for the intensity of such a development.

<u>Staff Comment:</u> The applicant is proposing to grade 8 residential lots to prepare the lots for further development. These lots are within Montreux, which is an approved residential subdivision. The proposed grading will make the parcels suitable for the planned development of residential houses.

(d) <u>Issuance Not Detrimental.</u> That issuance of the permit will not be significantly detrimental to the public health, safety or welfare; injurious to the property or improvements of adjacent properties; or detrimental to the character of the surrounding area.

<u>Staff Comment</u>: The applicant is proposing to grade 8 residential lots to prepare the lots for further development, which will not be detrimental to the area. These lots are within Montreux, which is an approved residential subdivision. The grading will prepare the lots to be developed with residential house as the zoning allows.

(e) <u>Effect on a Military Installation.</u> Issuance of the permit will not have a detrimental effect on the location, purpose or mission of the military installation.

<u>Staff Comment:</u> There is no military installation within the area of required notice for this special use permit; therefore, the project will have no effect on a military installation.

#### **Recommendation**

After a thorough analysis and review, Special Use Permit Case Number WSUP22-0004 is being recommended for approval with conditions. Staff offers the following motion for the Board's consideration.

## <u>Motion</u>

I move that, after giving reasoned consideration to the information contained in the staff report and information received during the public hearing, the Washoe County Board of Adjustment approve with conditions Special Use Permit Case Number WSUP22-0004 for Ladera Ventures II, LLC., with the conditions included as Exhibit A to this matter, having made all five findings in accordance with Washoe County Code Section 110.810.30:

- (a) <u>Consistency.</u> That the proposed use is consistent with the action programs, policies, standards and maps of the Master Plan and the Forest Area Plan;
- (b) <u>Improvements.</u> That adequate utilities, roadway improvements, sanitation, water supply, drainage, and other necessary facilities have been provided, the proposed improvements are properly related to existing and proposed roadways, and an adequate public facilities determination has been made in accordance with Division Seven;
- (c) <u>Site Suitability.</u> That the site is physically suitable for grading and for the intensity of such a development;
- (d) <u>Issuance Not Detrimental.</u> That issuance of the permit will not be significantly detrimental to the public health, safety or welfare; injurious to the property or improvements of adjacent properties; or detrimental to the character of the surrounding area;

(e) <u>Effect on a Military Installation.</u> Issuance of the permit will not have a detrimental effect on the location, purpose or mission of the military installation.

## Appeal Process

Board of Adjustment action will be effective 10 calendar days after the written decision is filed with the Secretary to the Board of Adjustment and mailed to the applicant, unless the action is appealed to the Washoe County Board of County Commissioners, in which case the outcome of the appeal shall be determined by the Washoe County Board of County Commissioners. Any appeal must be filed in writing with the Planning and Building Division within 10 calendar days from the date the written decision is filed with the Secretary to the Board of Adjustment and mailed to the applicant.

Applicant/Owner:	Ladera Ventures II, LLC. Brittany.Weygandt@laderaventures.com
Representatives:	LakeCrest Builders INC. leslie@lakecrestbuilders.com



**Conditions of Approval** 

Special Use Permit Case Number WSUP22-0004

The project approved under Special Use Permit Case Number WSUP22-0004 shall be carried out in accordance with the conditions of approval granted by the Board of Adjustment on April 7, 2022. Conditions of approval are requirements placed on a permit or development by each reviewing agency. These conditions of approval may require submittal of documents, applications, fees, inspections, amendments to plans, and more. These conditions do not relieve the applicant of the obligation to obtain any other approvals and licenses from relevant authorities required under any other act.

<u>Unless otherwise specified</u>, all conditions related to the approval of this special use permit shall be met or financial assurance must be provided to satisfy the conditions of approval prior to issuance of a grading or building permit. The agency responsible for determining compliance with a specific condition shall determine whether the condition must be fully completed or whether the applicant shall be offered the option of providing financial assurance. All agreements, easements, or other documentation required by these conditions shall have a copy filed with the County Engineer and the Planning and Building Division.

Compliance with the conditions of approval related to this special use permit is the responsibility of the applicant, his/her successor in interest, and all owners, assignees, and occupants of the property and their successors in interest. Failure to comply with any of the conditions imposed in the approval of the special use permit may result in the institution of revocation procedures.

Washoe County reserves the right to review and revise the conditions of approval related to this Special Use Permit should it be determined that a subsequent license or permit issued by Washoe County violates the intent of this approval.

For the purpose of conditions imposed by Washoe County, "may" is permissive and "shall" or "must" is mandatory.

Conditions of approval are usually complied with at different stages of the proposed project. Those stages are typically:

- Prior to permit issuance (i.e., grading permits, building permits, etc.).
- Prior to obtaining a final inspection and/or a certificate of occupancy.
- Prior to the issuance of a business license or other permits/licenses.
- Some "conditions of approval" are referred to as "operational conditions." These conditions must be continually complied with for the life of the project or business.

The Washoe County Commission oversees many of the reviewing agencies/departments with the exception of the following agencies.

• The DISTRICT BOARD OF HEALTH, through the Washoe County Health District, has jurisdiction over all public health matters in the Health District. Any conditions set by the Health District must be appealed to the District Board of Health. FOLLOWING ARE CONDITIONS OF APPROVAL REQUIRED BY THE REVIEWING AGENCIES. EACH CONDITION MUST BE MET TO THE SATISFACTION OF THE ISSUING AGENCY.

## Washoe County Planning and Building Division

1. The following conditions are requirements of Planning and Building, which shall be responsible for determining compliance with these conditions.

Contact Name – Julee Olander, Planner, 775.328.3627, jolander@washoecounty.gov

- a. The applicant shall attach a copy of the action order approving this project to all permits and applications (including building permits) applied for as part of this special use permit.
- **b.** The applicant shall demonstrate substantial conformance to the plans approved as part of this special use permit. The Planning and Building Division shall determine compliance with this condition.
- **c.** The applicant shall submit construction plans, with all information necessary for comprehensive review by Washoe County, and initial building permits shall be issued within two years from the date of approval by Washoe County. The applicant shall complete construction within the time specified by the building permits. Compliance with this condition shall be determined by the Planning and Building Division.
- d. A note shall be placed on all construction drawings and grading plans stating:

#### NOTE

Should any cairn or grave of a Native American be discovered during site development, work shall temporarily be halted at the specific site and the Sheriff's Office as well as the State Historic Preservation Office of the Department of Conservation and Natural Resources shall be immediately notified per NRS 383.170.

- e. Construction work hours will be limited to 7am to 7pm Monday to Saturday.
- f. Any imported earthen materials shall be "certified weed free" in order to prevent the spread of noxious weeds within the county.
- g. The grading on site shall be in compliance with applicable best management practices to minimize erosion.
- h. The following **Operational Conditions** shall be required for the life of the business:
  - i. This special use permit shall remain in effect until or unless it is revoked or is inactive for one year.
  - ii. Failure to comply with any of the conditions of approval shall render this approval out of conformance and subject to revocation.
  - iii. The applicant and any successors shall direct any potential purchaser/operator of the site and/or the administrative permit to meet with Planning and Building to review conditions of approval prior to the final sale of the site and/or the administrative permit. Any subsequent purchaser/operator of the site and/or the administrative permit shall notify Planning and Building of the name, address, telephone number, and contact person of the new purchaser/operator within 30 days of the final sale.

## Washoe County Engineering and Capital Projects

2. The following conditions are requirements of the Engineering Division, which shall be responsible for determining compliance with these conditions.

## Contact Name – Robert Wimer, P.E, 775.328-2059, rwimer@washoecounty.gov

- a. A complete set of construction improvement drawings, including an on-site grading plan, shall be submitted when applying for a building/grading permit. Grading shall comply with best management practices (BMP's) and shall include detailed plans for grading, site drainage, erosion control (including BMP locations and installation details), slope stabilization, and mosquito abatement. Placement or removal of any excavated materials shall be indicated on the grading plan. Silts shall be controlled on-site and not allowed onto adjacent property.
- b. For construction areas larger than 1 acre, the developer shall obtain from the Nevada Division of Environmental Protection a Stormwater Discharge Permit or Waiver for construction and submit a copy to the Engineering Division prior to issuance of a grading permit.
- c. The developer shall complete and submit the Construction Permit Submittal Checklist and pay the Construction Stormwater Inspection Fee prior to obtaining a grading permit. The County Engineer shall determine compliance with this condition.
- d. Applicant shall indicate on the plans where exported materials will be taken and a grading permit shall be obtained for the import site.
- e. Exported materials shall not be sold without the proper business license.
- f. A grading bond of \$2,000/acre of disturbed area shall be provided to the Engineering Division prior to any grading.
- g. Cross-sections indicating cuts and fills shall be submitted when applying for a grading permit. Estimated total volumes shall be indicated.
- h. All disturbed areas left undeveloped for more than 30 days shall be treated with a dust palliative. Disturbed areas left undeveloped for more than 45 days shall be revegetated. Methods and seed mix must be approved by the County Engineer with technical assistance from the Washoe-Storey Conservation District. The applicant shall submit a revegetation plan to the Washoe-Storey Conservation District for review.

DRAINAGE (COUNTY CODE 110.416, 110.420, and 110.421)

Contact Information: Robert Wimer, P.E, 775.328-2059, rwimer@washoecounty.gov

a. The following note shall be added to the construction drawings; "All properties, regardless if they are located within or outside of a FEMA designated flood zone, may be subject to flooding. The property owner is required to maintain all drainage easements and natural drainages and not perform or allow unpermitted and unapproved modifications to the property that may have detrimental impacts to surrounding properties."

## Washoe County Health District- Air Quality

3. The following conditions are requirements of the Health District, which shall be responsible for determining compliance with these conditions.

## Contact Name - Genine Rosa, Environmental Engineer II, 775.784.7204, grosa@washoecounty.gov

a. Dust Control Permit will be required prior to breaking ground, failure to do so may result in enforcement action resulting in a Notice of Violation with associated fines. For Dust Control Permit questions call AQMD at 775-784-7200 or visit www.OurCleanAir.com. Link to application: Dust Control Permit Application

\*\*\* End of Conditions \*\*\*



WASHOE COUNTY COMMUNITY SERVICES DEPARTMENT Engineering and Capital Projects

1001 EAST 9<sup>TH</sup> STREET RENO, NEVADA 89512 PHONE (775) 328-3600 FAX (775) 328.3699

- Date: February 28, 2022
- To: Julee Olander, Planner
- From: Robert Wimer, P.E., Licensed Engineer
- Re: Special Use Permit for *Latour Excavation WSUP22-0004* APN 148-333-01, 02 & 03, 148-322-01, 02, 03, 04, & 08

## **GENERAL PROJECT DISCUSSION**

Washoe County Engineering staff has reviewed the above referenced application. The Special Use Permit is for the grading of eight new homes and is located on approximately 3.2 acres on the west side of Latour Way off of Bordeaux Way. The Engineering and Capital Projects Division recommends approval with the following comments and conditions of approval which supplement applicable County Code and are based upon our review of the site and the application prepared by LakeCrest Builders, Inc. The County Engineer shall determine compliance with the following conditions of approval.

For questions related to sections below, please see the contact name provided.

## **GENERAL CONDITIONS**

Contact Information: Robert Wimer, P.E. (775) 328-2059

- A complete set of construction improvement drawings, including an on-site grading plan, shall be submitted when applying for a building/grading permit. Grading shall comply with best management practices (BMP's) and shall include detailed plans for grading, site drainage, erosion control (including BMP locations and installation details), slope stabilization, and mosquito abatement. Placement or removal of any excavated materials shall be indicated on the grading plan. Silts shall be controlled on-site and not allowed onto adjacent property.
- 2. For construction areas larger than 1 acre, the developer shall obtain from the Nevada Division of Environmental Protection a Stormwater Discharge Permit or Waiver for construction and submit a copy to the Engineering Division prior to issuance of a grading permit.
- 3. The developer shall complete and submit the Construction Permit Submittal Checklist and pay the Construction Stormwater Inspection Fee prior to obtaining a grading permit. The County Engineer shall determine compliance with this condition.
- 4. Applicant shall indicate on the plans where exported materials will be taken and a grading permit shall be obtained for the import site.
- 5. Exported materials shall not be sold without the proper business license.

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Subject:Latour Excavation WSUP22-0004Date:February 28, 2022Page:2

- 6. A grading bond of \$2,000/acre of disturbed area shall be provided to the Engineering Division prior to any grading.
- 7. Cross-sections indicating cuts and fills shall be submitted when applying for a grading permit. Estimated total volumes shall be indicated.
- 8. All disturbed areas left undeveloped for more than 30 days shall be treated with a dust palliative. Disturbed areas left undeveloped for more than 45 days shall be revegetated. Methods and seed mix must be approved by the County Engineer with technical assistance from the Washoe-Storey Conservation District. The applicant shall submit a revegetation plan to the Washoe-Storey Conservation District for review.

## DRAINAGE (COUNTY CODE 110.416, 110.420, and 110.421)

Contact Information: Robert Wimer, P.E. (775) 328-2059

1. The following note shall be added to the construction drawings; "All properties, regardless if they are located within or outside of a FEMA designated flood zone, may be subject to flooding. The property owner is required to maintain all drainage easements and natural drainages and not perform or allow unpermitted and unapproved modifications to the property that may have detrimental impacts to surrounding properties."

## TRAFFIC AND ROADWAY (COUNTY CODE 110.436)

Contact Information: Mitch Fink, P.E. (775) 328-2050

1. There are no traffic related comments.

## UTILITIES (County Code 422 & Sewer Ordinance)

Contact Information: Tim Simpson, P.E. (775) 954-4648

1. There are no utility related comments.



March 1, 2022

Washoe County Community Services Planning and Development Division

RE: Latour Excavation; 148-333-01, 02, 03 148-322-01 Special Use Permit; WSUP22-0004

Dear Washoe County Staff:

The following conditions are requirements of the Washoe County Health District, Environmental Health Division, which shall be responsible for determining compliance with these conditions.

#### Contact Name, James English, jenglish@washoecounty.us

a) Condition #1: WCHD has no issues with this application as submitted.

If you have any questions or would like clarification regarding the foregoing, please contact James English, EHS Supervisor at jenglish@washoecounty.us regarding all Health District comments.

Sincerely,

Jarhes Enòlish. RE1/4S. CP-FS **EHS Supervisor Environmental Health Services** Washoe County Health District





## Washoe-Storey Conservation District

Bret Tyler Chairmen Jim Shaffer Treasurer Cathy Canfield Storey app Jean Herman Washce app

1365 Corpotate Blvd. RenoNV 89502 775 857-8500 ext. 131 nevadaconservation.com

February 25, 2022

Washoe County Community Services Department

C/O Julee Olander, Planner

1001 E Ninth Street, Bldg. A

Reno, NV 89512

R: WSUP22-0004 Latour Excavation

Dear Julee,

In reviewing the special use permit for grading for eight new homes, the Conservation District has the following comments.

The District will require review of the vegetation plan that includes a seed mix based on the soil, contingency water plan, fertilizer plan, erosion control structures and a monitoring plan with updates provided to the Conservation District after the growing season (October 31) for a three-year period.

To prevent the spread of noxious weeds in the export of 4,800 cubic yards of material, the applicant develops an onsite weeds management plan to ensure weed seeds do not impact other areas.

With 174 Ponderosa and Jeffrey pines removed, to mitigate this loss a minimum 1.5 to 1 ratio planting of the same tree variety.

With rockery walls proposed, the District will require the voids in the face of the rockery walls entire height filled with smaller rock to prevent the undermining by small animals.

In the geotechnical investigation if the applicant constructs post tension slab one can avoid mold and insect issues from standing water with raised foundations.

Thank you for providing us the opportunity to review the project that may have impacts on our natural resources and any questions call us (775) 750 8272.

Sincerely,

Jim Shaffer



WASHOE COUNTY COMMUNITY SERVICES

INTEGRITY COMMUNICATION SERVICE

Reno, Nevada 89520-0027 Phone: (775) 328-3600 Fax: (775) 328-3699

February 22, 2022

TO: Julee Olander, Planner, CSD, Planning & Development Division

FROM: Timber Weiss, Licensed Engineer, CSD

SUBJECT: Special Use Permit Case Number WSUP22-0004 (Latour Excavation)

## **Project description:**

The applicant is proposing to approve grading of 9,150 cubic yards (CY) of cut material for eight new homes in the Montreux subdivision.

Location: Latour Way, Montreux Subdivision. Assessor's Parcel Numbers: 148-333-01, 02 & 03, 148-322-01, 02, 03, 04, & 08.

The Community Services Department (CSD) recommends approval of this project with the following Water Rights comments and/or conditions:

## **Comments:**

Recommend approval of this permit.

The only anticipated water demand would be for dust control. It is assumed that water trucks would be used to meet this demand. These parcels are located within TMWA's service area. Discuss potential water use requirements with their new construction division.

## **Conditions:**

There are no conditions of approval as for water rights and water resources.



WSUP22-0004 EXHIBIT B

From:	Rosa, Genine
То:	Olander, Julee
Subject:	RE: WSUP22-0004 Latour grading
Date:	Wednesday, March 2, 2022 2:21:02 PM
Attachments:	image007.png
	image008.png
	image009.png
	image010.png
	image011.png

Comments below:

Dust Control Permit will be required prior to breaking ground, failure to do so may result in enforcement action resulting in a Notice of Violation with associated fines. For Dust Control Permit questions call AQMD at 775-784-7200 or visit <u>www.OurCleanAir.com</u>. Link to application: <u>Dust Control Permit Application</u>

Feel free to contact me with any questions.

Thank you,

**Genine** Environmental Engineer II O: (775) 784-7204

www.OurCleanAir.com | Subscribe to get Air Quality Updates!



## Please take our customer satisfaction survey by clicking here

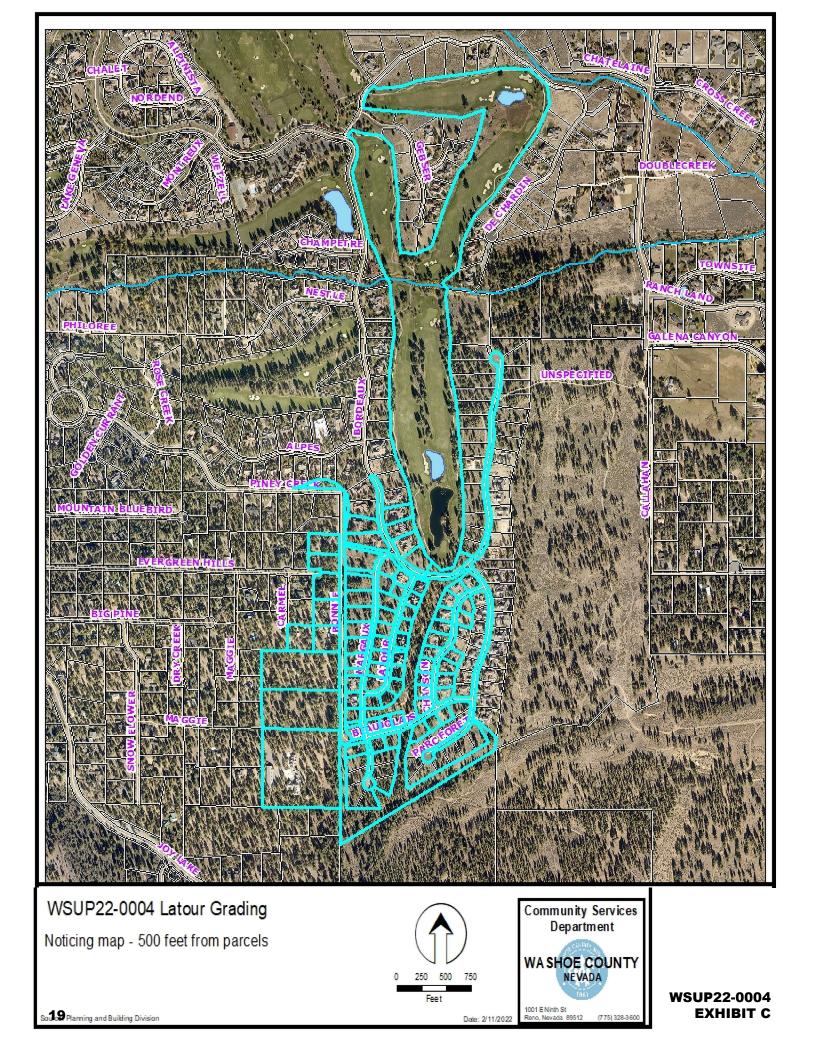
From: Olander, Julee <JOlander@washoecounty.gov>
Sent: Wednesday, March 2, 2022 1:41 PM
To: Rosa, Genine <GRosa@washoecounty.gov>
Subject: WSUP22-0004 Latour grading

Do you have comments for this permit?



## Please tell us how we did by taking a quick survey

Julee Olander Planner, Planning & Building Division | Community Services Department jolander@washoecounty.gov | Direct Line: 775.328.3627 My working hours: Monday-Friday 8:00 am to 4:30 pm Visit us first online: www.washoecounty.gov/csd Planning Division: 775.328.6100 | Planning@washoecounty.gov CSD Office Hours: Monday-Friday 8:00am to 4:00pm 1001 East Ninth Street, Reno, NV 89512 () () () () ()



# Community Services Department Planning and Building SPECIAL USE PERMIT FOR GRADING (see page 9)

## APPLICATION



Community Services Department Planning and Building 1001 E. Ninth St., Bldg. A Reno, NV 89512-2845

Telephone: 775.328.6100

## Washoe County Development Application

Your entire application is a public record. If you have a concern about releasing personal information, please contact Planning and Building staff at 775.328.6100.

Project Information	:	Staff Assigned Case No.:		
Project Name: Latour	Excavation			
Project Grading for 8 Description:	new homes.			
Project Address: Latour Way F	Reno NV 89511			
Project Area (acres or square	eet): 3.33 Acres			
Project Location (with point of	reference to major cros	s streets AND area locator):		
Bordeaux Dr. F	Reno NV 89	9511		
Assessor's Parcel No.(s):	Parcel Acreage:	Assessor's Parcel No.(s):	Parcel Acreage:	
148-333-01 & 148-333-02	0.451 & 0.430	148-322-02 & 148-322-03	0.401 & 0.454	
148-333-03 & 148-322-01	0.408 & 0.389	148-322-04 & 148-322-08	0.510 & 0.287	
Case No.(s). N/A		Is associated with this applica		
Applicant Ir	formation (attach	n additional sheets if neces	sary)	
Property Owner:		Professional Consultant:		
Name: Ladera Ventures II LLC	,	Name: LakeCrest Builders INC		
Address: 16475 Bordeaux Driv	ve Reno NV	Address: 16475 Bordeaux Driv	Address: 16475 Bordeaux Drive Reno NV	
	Zip: 89511		Zip: 89511	
Phone: 775.849.9444	Fax:	Phone: 775.849.9690 Fax: 775.849.31		
Email: Brittany.Weygandt@lac	eraventures.com	Email: leslie@lakecrestbuilders.com		
Cell: N/A Other:		Cell: N/A Other:		
Contact Person: Brittany Weygandt		Contact Person: Leslie Ayala		
Applicant/Developer:		Other Persons to be Contacted:		
Name:		Name:		
Address:		Address:		
	Zip:		Zip:	
Phone: Fax:		Phone:	Fax:	
Email:		Email:		
Cell: Other:		Cell: Other:		
Contact Person:		Contact Person:		
	For Office	e Use Only		
Date Received:	Initial:	Planning Area:		
County Commission District:		Master Plan Designation(s):		
CAB(s):		Regulatory Zoning(s):		

## **Property Owner Affidavit**

## Applicant Name: James Pickett

The receipt of this application at the time of submittal does not guarantee the application complies with all requirements of the Washoe County Development Code, the Washoe County Master Plan or the applicable area plan, the applicable regulatory zoning, or that the application is deemed complete and will

STATE OF NEVADA COUNTY OF WASHOE

mes

(please print name)

being duly sworn, depose and say that I am the owner\* of the property or properties involved in this application as listed below and that the foregoing statements and answers herein contained and the information herewith submitted are in all respects complete, true, and correct to the best of my knowledge and belief. I understand that no assurance or guarantee can be given by members of Planning and Building.

(A separate Affidavit must be provided by each property owner named in the title report.)

Assessor Parcel Number(s): 148-322-08; 148-322-04; 148-322-03; 148-322-02; 148-322-01; 148-333-03; 148-333-02; 148-333-01

F	Printed Name_ James Pickett
	Signed
	Address #6475 Bordeaux Dr
Subscribed and sworn to before me this	- Rono NV 89511

(Notary Stamp)

LORENE DEVITO Notary Public - State of Nevada

Appointment Recorded in Storey County No: 10-3481-16 - Expires Dec. 02, 2022

the day of Januar

Notary Public in and for said county and state

My commission expires: December 2, 2022

\*Owner refers to the following: (Please mark appropriate box.)

Owner

25

- Corporate Officer/Partner (Provide copy of record document indicating authority to sign.)
- Power of Attorney (Provide copy of Power of Attorney.)
- Owner Agent (Provide notarized letter from property owner giving legal authority to agent.)
- Property Agent (Provide copy of record document indicating authority to sign.)

EGOL

Letter from Government Agency with Stewardship

## Special Use Permit Application for Grading Supplemental Information

(All required information may be separately attached)

1. What is the purpose of the grading?

Prep for new residential homes.

2. How many cubic yards of material are you proposing to excavate on site?

# 9,150 CY (CUT)

3. How many square feet of surface of the property are you disturbing?

122,204 SF (2.80 AC)

4. How many cubic yards of material are you exporting or importing? If none, how are you managing to balance the work on-site?

4,890 CY (CUT) "Exporting"

5. Is it possible to develop your property without surpassing the grading thresholds requiring a Special Use Permit? (Explain fully your answer.)

No, because these lots will have rock walls cross property lines which requires all lots to be graded at the same time. There are 8 lots total, each lot separately doesn't surpass any thresholds. ALL roadways and utilities are existing and will NOT be changed.

6. Has any portion of the grading shown on the plan been done previously? (If yes, explain the circumstances, the year the work was done, and who completed the work.)

No

7. Have you shown all areas on your site plan that are proposed to be disturbed by grading? (If no, explain your answer.)

9

Yes, all areas are shown.



8. Can the disturbed area be seen from off-site? If yes, from which directions and which properties or roadways?

No, unless you're standing directly in front of the property.

9. Could neighboring properties also be served by the proposed access/grading requested (i.e. if you are creating a driveway, would it be used for access to additional neighboring properties)?

No. All surrounding roadways are already in place.

10. What is the slope (horizontal/vertical) of the cut and fill areas proposed to be? What methods will be used to prevent erosion until the revegetation is established?

Rockery retaining walls per attached plan. Lots will be finished with full landscaping and proper drainage to prevent erosion.

11. Are you planning any berms?

Yes No X	If yes, how tall is the berm at its highest?	
----------	--	--

12. If your property slopes and you are leveling a pad for a building, are retaining walls going to be required? If so, how high will the walls be and what is their construction (i.e. rockery, concrete, timber, manufactured block)?

Rockery retaining walls are required, see attached wall details for more info.

13. What are you proposing for visual mitigation of the work?

# Fully landscaped new homes.

14. Will the grading proposed require removal of any trees? If so, what species, how many and of what size?

Yes, Ponderosa & Jeffrey Pines, approx. 174 existing trees to be removed. See plans for sizing.

15. What type of revegetation seed mix are you planning to use and how many pounds per acre do you intend to broadcast? Will you use mulch and, if so, what type?

10

# Lots will be FULLY landscaped at finish

16. How are you providing temporary irrigation to the disturbed area?

Hand watering during construction using existing Washoe County water meters.

17. Have you reviewed the revegetation plan with the Washoe Storey Conservation District? If yes, have you incorporated their suggestions?

## Yes and yes

18. Are there any restrictive covenants, recorded conditions, or deed restrictions (CC&Rs) that may prohibit the requested grading?

Yes No X	If yes, please attach a copy.
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25



300 Western Road, #3, Reno, NV 89506 • (775) 852-7475 FAX (775) 852-7488

February 2, 2022 2405-03C

Lake Crest Builders 16475 Bordeaux Drive Reno, Nevada 89511

> Geotechnical Investigation Proposed Residential Development Lots 404 through 515 Reno, Nevada

#### Introduction

This report presents the results of our geotechnical investigation for the proposed new residential Parc Foret lots subdivision unit to be located between Latour Way and Margaux in the Montreux Community, designated as Lots 404 through 515. We have not yet received the building plans for this project but we understand that this project involves construction of new one or two story residential units. We anticipate that the buildings will be constructed of wood framing and utilize joist supported foundations.

Our scope of work was to con a subsurface investigation with testing and analysis to deter-mine site conditions and the engineering properties of the underlying soils and any rock as well as to provide recommendations for slope stability and retaining wall design. We are to provide conclusions and recommendations concerning geologic hazards and seismic design, site prepara-tion and grading, design criteria for foundations and retaining walls, including estimates of settle-ment and support of interior and exterior flat-work. Recommendations for structural fill and drain-age are also presented.

## Site, Soil and Rock Conditions

The development will be located on Parc Foret lots that are located between Latour Way and Margaux Road in the Montreux Community. The two building zones showing Test Pits 1 through 5 and Test Pits 6 and 7 indicated on the Site and Exploration Plan, Pate 1, are presently under residential construction. They are presented to reveal previous investigation work conducted in the subject properties vicinity. The vegetation on the lots consists of medium sized brush, weeds and grasses, with trees, tree stumps and boulders. No free ground water was encountered. For on-site soil conditions, we logged a large approximately 8 foot deep excavation cut on one northern lot along Margaux Road. See discussion below.

We logged the cut profile as a pseudo test pit and compared it with the plan indicated Test Pits 6 and 7, the nearest pits to the subject lots. The on-site pit log is vary similar to the previous profiles.- The materials encountered in the cut were logged and a representative sample was obtained for laboratory classification and direct shear testing. The site plan with the approximate locations of the previous test pits is shown on Plate 1 and a log of the pseudo Test Pit A is presented on Plate 2. The soils are classified in accordance with the Unified Soil Classification System, which is described on Plate 3. Laboratory classification and direct shear test results are shown on Plates (Figures) 4 and 5.



## **Geologic and Flooding Considerations**

The site is located north of Mount Rose Highway in Washoe County. The present topography of the site appears to be derived from a geologic unit known as Older Alluvium and Alluvial Fan Deposits (NVQToa;0) as well as Felsic Phaneritic Intrusive Rocks (NVTJfi;0). (Crafford, A.E.J., 2007, Geologic Map of Nevada: U.S. Geological Survey Data Series 249, 1 CD-ROM, 46 p., 1 plate; Scale 1:250,000.)

A known fault of late Quaternary age (within the last 15,000 years) lies within 50 feet of the proposed development, it runs roughly from north to south and is considered part of the Mount Rose Fault Zone. The faults in the area were mapped by earlier studies performed by Black Eagle Consulting as well as by the U.S. Geological Survey. The approximate trace of the fault is shown on Plate 1 in yellow. Nortech recommends a minimum building setback of 50 feet from the fault zone. Due to the proximity to an active fault, seismic design criteria values are higher than average for the Reno area.

There is a regional potential for moderate to large magnitude earthquakes in the mid and western portions of Nevada. Washoe County currently requires the use of the site characterization criteria found in the 2018 International Residential Code (IRC) for design. The 2018 IRC directly references the ASCE 7-16. The seismic design criteria is found in code and the USGS website. The IRC requires that the Site Class be determined by soil and rock parameters described per ASCE 7-16, Chapter 11, Section 11.4.3:"Site Class" and Chapter 20, Section 20.1: "Site Classification", the Site Class defaults to "D" without confirming soil and rock data to a depth of 100 feet below the ground surface. We have shear wave velocity data from a previous site study very near the subject lots which would be representative of the new unit. The data is presented on Plate 6 (Vs30 Shear Wave Velocity). The maximum considered earthquake ground motion spectral accelerations for short periods and for one second periods are given on figures in the International Building Code (IBC) code. Using the site latitude and longitude as input, the USGS website provides accurate site specific acceleration values along with the respective site coefficients and design spectral response acceleration parameters in their Design Maps Summary Report. Only the Design Spec-tral Response Acceleration for Short Periods, SD<sub>s</sub> is needed for design. The Residential Seismic Design Category is also given in the IRC. Based on this research, the site specific seismic design criteria for the subject property is presented below:

TABLE 1 - 2018 IRC SEISMIC DESIGN CRITERIA	
Spectral Response at Short Periods, S <sub>s</sub> (USGS)	2.090
Spectral Response at 1-Second Period, S1 (USGS)	0.742
Site Class (USGS)	D
Site Coefficient F <sub>a</sub> (USGS)	1.000
Site Coefficient Fv (USGS)	
Design Spectral Response Acceleration, Short Periods, $SD_s = 2/3 \times F_a \times S_s$ (USGS)	1.393
Residential Seismic Design Category (IRC Table R301.2.2.1.1.)	E
Peak Ground Acceleration (PGA)	0.906



Site Coefficient  $F_v$  (mapped risk targeted maximum considered earthquake (MCER) spectral response acceleration parameter at 1-second period) value is determined by table 11.4.2 from ASCE 7-16 according to site class, this is done in lieu of performing a site hazard analysis. The Site Class used is D, "Stiff Soil".

The Federal Emergency Management Agency (FEMA) Study Flood Boundary and Floodway Map (Map Number 32031C3327G, March 16, 2009) indicates that the subject property is located in Zone X. The Zone X designation describes those areas outside the 0.2 % Annual Chance Flood-plain.

## Conclusions

Based upon the results of our current and previous investigations, we conclude that, from a geotechnical engineering standpoint, we believe that in general, conventional site grading techniques, building foundations and floor slab construction can be used for the development. The residential structures and flatwork can be supported on firm compacted native soil, and/or the structural fill placed. The exterior foundation excavations will be at least 24 inches deep below lowest exterior grade. Some new fill may be needed for pad leveling. Native sand excavation material can be used as fill if needed and as available, but screening will be required to remove any oversize rock. Material can also be imported. All fill should be approved by the geotechnical engineer and be placed and compacted as recommended in subsequent sections of this report.

We anticipate that for the shallow foundations designed and constructed in accordance with our recommendations, the post construction differential settlement will be on the order of ½ to 3/4 inch. Any post construction differential settlement for footings bearing entirely on large boulders and/or bedrock would be negligible.

An evaluation of the slope stability based on the existing slope geometry and for terraced walls has been designed as required for permitting. We recommend that the walls nearest to the roadway be located at least 15 feet away for the curb line, mainly for safety concerns. The stability analysis was performed using the Stablpro computer software program developed by Ensoft Inc. The Bishop Method of analysis, widely accepted in the industry, was used to calculate the factor of safety against failure for the embankment slopes. The wall designs and the results of the analyses are submitted under separate cover.

## **Recommendations**

Initially, areas to be developed should be cleared of any surface vegetation and any debris. These materials should be removed from the site. All stripped and any excavated soil surfaces not designated to be removed should be moisture conditioned and compacted to at least 90 percent relative compaction (per ASTM D1557) prior to any fill placement or installation of structural components.

Only select structural materials should be used for fill and backfill as needed. Structural materials imported to the site should be free of organic and other deleterious matter, have low to negligible expansion potential and conform in general to the following requirements:



Percent Passing (by dry weight)
100 70 - 100
50 - 100 10 - 35

Liquid Limit = 35 maximum Plasticity Index = 15 maximum

We anticipate that generally based on laboratory testing, the on-site, the sand and gravel materials generated by any new excavation will be suitable for use as structural fill as available, but screening will be needed. All existing and imported fill materials should be approved by the geotechnical engineer prior to use. All structural fill and backfill should be spread in 8- to 10-inch, moisture conditioned, loose lifts and compacted to at least 90 percent relative compaction.

Conventional spread foundations should be supported entirely on native soils and/or new and reused structural fill. To provide confinement and for adequate frost protection, building perimeter and any other exterior footings should bottom at least 24 inches below lowest adjacent exterior grade. Footings supported as above, on fill can be designed to impose dead plus long-term live load bearing pressures of no greater than 2,500 pounds per square foot (psf). This allowable bearing pressure can be increased by one-third for consideration of all live loads including wind or seismic.

Prior to installation of reinforcing steel, all bearing surfaces should be observed by the geotechnical engineer to ensure satisfactory support is being achieved and that there are no objectionable materials present. Any loose material should be removed from the footing trenches prior to pouring concrete.

Resistance to lateral loads can be obtained from passive earth pressures and soil friction. We recommend the following design criteria:

Passive Earth Resistance - 300 pounds per cubic foot (pcf), equivalent fluid

Soil Friction Factor - 0.35

We recommend that any unrestrained (cantilever) or restrained retaining walls be designed to resist the active or "at rest" pressures imposed by soils with equivalent fluid unit weights of 35 or 55 pcf, respectively. Wall backdrains, with a four inch diameter collector pipe (at the base of the wall), should be installed along the retaining walls to collect any seepage that may accumulate and discharge it to planned outlet points or drainage areas. The gravel (drain rock) should extend to within 12 inches of the final grade and should be covered with a fabric inter-layer. Native soils should be placed on the top of the drain rock and fabric. All walls should be backfilled with structural material as design pressure calculations are based on the use of on-site or imported granular soils.



For seismic design pressures on retaining walls greater than 4 feet in height, use:

Resultant Seismic Force , =  $0.375^{*}K_{h}^{*}Y^{*}H^{2}$ 

Seismic design Coefficient ( $K_h$ ), = Sd<sub>s</sub>/2.5

Total Soil Unit Weight (Y) = 120 pcf

The pressure distribution is inverted semi-triangular (with the maximum pressure at the top of the wall) and the resultant acts at 0.6 X H above the wall base. The 0.6 reference is from the RetainPro manual.

Interior floor slabs can be supported on firm, approved compacted fill. Floor slabs should be underlain by at least six inches of free draining crushed rock base or aggregate base. Exterior concrete flatwork such as driveways, curbs, sidewalks and patios supported on firm, native soils or structural fill should be underlain by at least six inches of aggregate base. Aggregate base material used in these interior and exterior areas should be compacted to at least 95 percent relative compaction. To provide uniform slab section support, all subgrade sur-faces (upper six inches) should be scarified, moisture conditioned, and compacted to at least 90 percent relative compaction. The resulting subgrade and base surfaces should be smooth, firm and non-yielding.

If a vapor barrier is to be used, we recommend Stego-Wrap or equal. It should be installed with proper procedures and care so as not to expose the concrete slabs to a potential for curling.

Concrete mix proportions and construction techniques, including the addition of water and improper curing, can adversely affect the finished quality of the concrete and result in cracking and spalling of the slabs and other flatwork. We recommend that all placement and curing be performed in accordance with procedures outlined by the American Concrete Institute (ACI). Special consideration should be given to concrete placed and cured during hot or cold weather conditions. Proper control joints and reinforcing should be provided where applicable to minimize any cracking resulting from shrinkage.

Backfilling around building walls needed to attain final grade in non structural areas should be moisture conditioned, placed in 12 inch maximum thickness lifts, and be compacted to at least 85 percent minimum relative compaction. Field density testing of the backfill operations should be performed to ensure compaction is being achieved.

The ground surface around the structure should be permanently sloped to drain away from the building so that water is not allowed to pond against perimeter walls. The finish grading around the structure should be in accordance with current building code requirements. Finish grading should be verified by the Civil Engineer.

In addition to adequate surface drainage, a system of roof gutters and downspouts is recommended to collect roof drainage and direct it away from the walls and foundations. Foundation drainage is also recommended. Drains along foundations should be graded to drain to a collection point, with a pipe provided to daylight to an exterior discharge area.



There has been an increase in ground water rising to, and seeping out of concrete floor slab and/or collecting in crawl spaces in many mountain communities. Many project design plans show that the drain pipe and rock (or Mira-drain type systems) around the exterior foundation is to be located on the top of the footing. We strongly recommended that the drains be installed along the side of the footing and be placed at the foundation grade. These drains along foundations should be graded to drain to a collection point, with a pipe provided to daylight to an exterior discharge area. Details for the various foundation and wall systems are presented on the attached Plate 11.

Site drainage should also be designed to restrict infiltration from entering any flatwork sections. Periodic crack sealing and surface sealing should be implemented to increase service life of the concrete slabs and any pavements. Upon occupancy and/or any sale of the individual residence, the Builder, the design and project managing Architect and Civil Engineer, and Nortech will have no control over any alteration of the respective site grades and drainage conveyance. Therefore, it is the responsibility of the current, and any future property owners, to maintain proper surface and subsurface drainage on this lot.

## Additional Geotechnical Engineering and Inspection Services

The conclusions and recommendations presented in this report are based on the results of current field exploration and our understanding of the proposed construction. This report has been prepared in accordance with current, generally accepted, geotechnical engineering standards of practice for the limited scope of work authorized. It is believed that the soil and rock information compiled presents an accurate representation of the subsurface conditions and variations to be expected within the areas studied. However, there is a possibility that conditions other than those found in this investigation exist on-site. In the event that unanticipated conditions are encountered during construction, we should be given budget allowances to evaluate the condition(s) and make timely new recommendations or modify our existing report to satisfy the project needs.

We should provide on-site observations, together with field and laboratory testing during site preparation and grading, excavation and foundation installation. These observations and tests would allow us to verify that the soil conditions are as anticipated and that the Contractor's work is in conformance with this report and the approved plans and specifications.

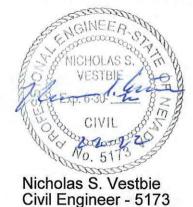
In addition, Nortech can provide any and all IBC Special Inspection services such as masonry, concrete, steel (welding, bolting, dry pack, etc.), fireproofing and any other construction or installations requiring such services. We have ICC certified inspectors on staff and would be pleased to submit a proposal for any inspection services prior to construction.



We trust this provides the information needed; however, if you have any questions regarding this report, please contact our office.

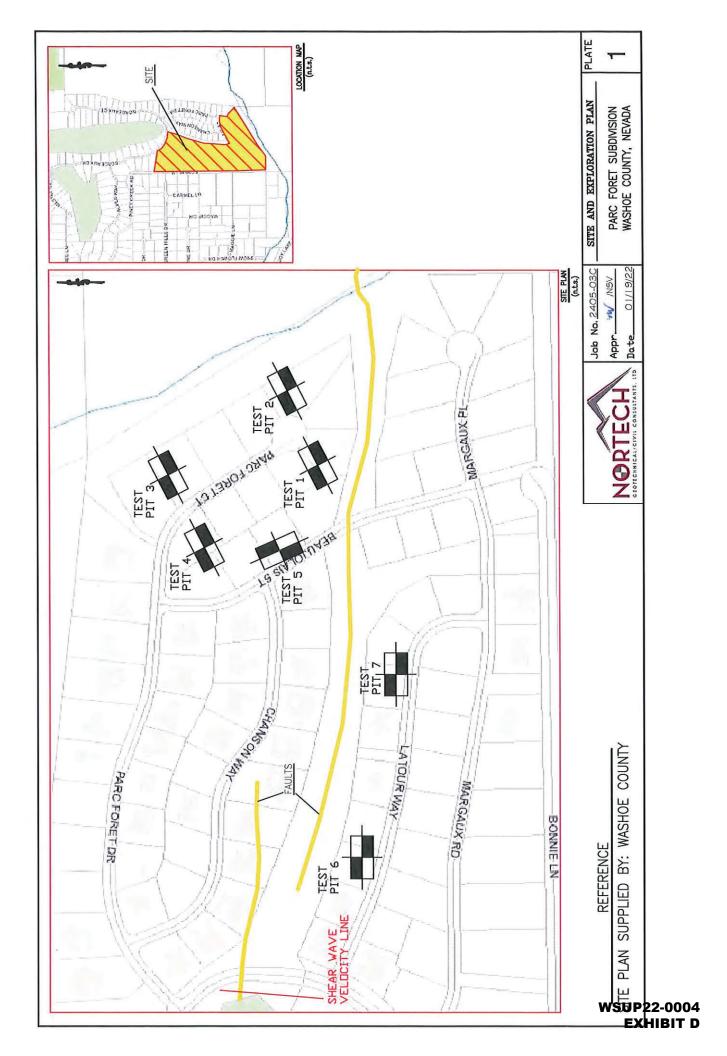
Yours very truly,

NORTECH Geotechnical/Civil Consultants, Ltd.



CRW/IIm

Enclosures: Plate 1: Site and Exploration Plan Plate 2: Logs of Pseudo Test Pit A Plate 3: Unified Soil Classification Chart Figure 4: Particle Size Distribution Report Figure 5: Direct Shear Test Report Plate 6: Vs30 Shear Wave Velocity Plate 7: Foundation Drain Details

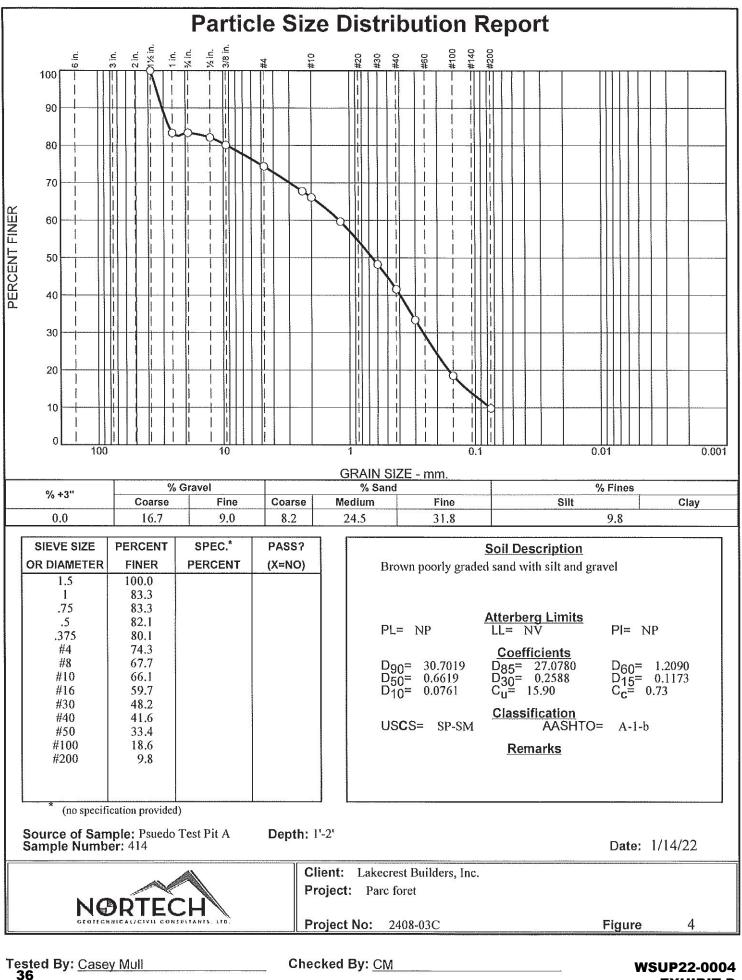


Laboratory Tests (and other info.)	DECNENT (%) MOISTURE CONTENT (%) DENSITY (PCF)	Test Pit No.:       Pseudo Test Pit A         (:       Equipment:       Hand Sample         H       H       Elevation:       N/A         H       H       Date:       01/08/22
*SIEVE ANALYSIS and DIRECT SHEAR TESTS (See Figures 4 and 5)		BROWN SAND (SP-SM) With silt, gravel and roots, moist, medium dense, cobbles 6" size LIGHT BROWN SANDY GRAVEL (GP) Moist, medium dense, cobbles and boulders to 2' size
		8 - No Free Water Encountered
		12-
TEST PIT LOCATION: LATITUDE: 39.351796 LONGITUDE: —119.823564 Estimated Error: 5 to 6' radius from mid point		
NORTECH 32FOTECHNICAL/CIVIL CONSULTANTS, LTD	Date: 01/	B-O3C       LOG OF PSEUDO TEST PIT A       PLATE         /nsv       PARC FORET 8 LOT UNIT       PLATE         14/22       LATOUR WAY AND MARGAUX ROAD       WASHOE, NEVADA         WASHOE, NEVADA       WSUP22-0004         EXHIBIT D

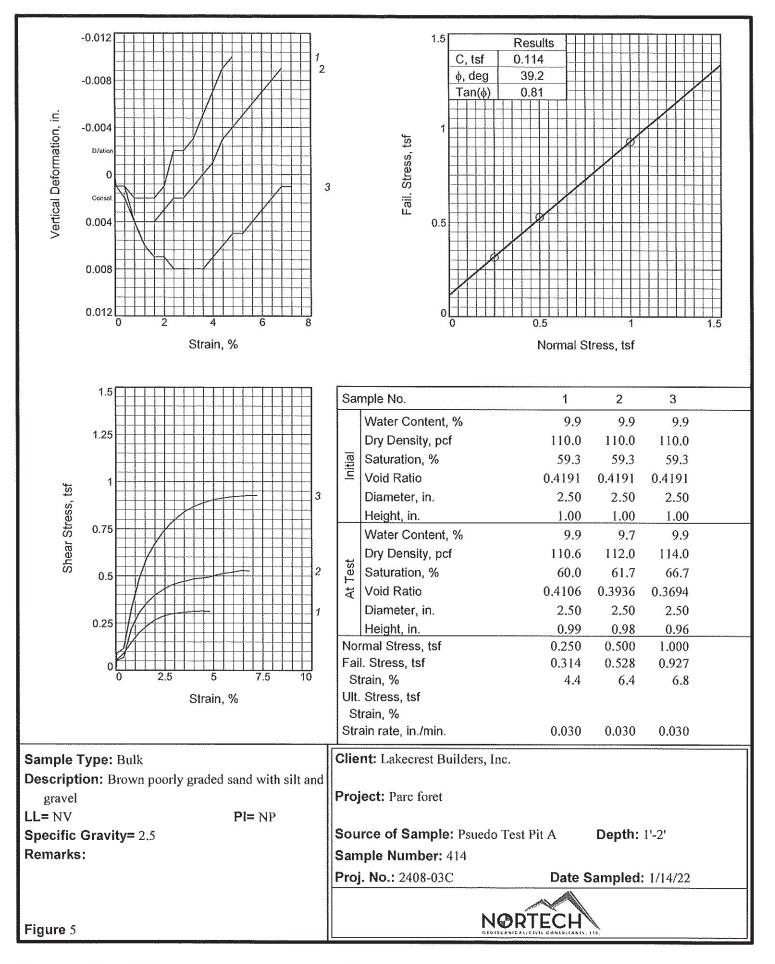
MAJOR DIVISIONS					TYPICAL NAMES		
COARSE GRAINED SOILS more than half is larger than # 200 sieve	GRAVELS MORE THAN HALF COARSE FRACTION IS LARGER THAN NO. 4 SIEVE SIZE	CLEAN GRAVELS WITH LITTLE OR NO FINES	GW		WELL GRADED GRAVELS, GRAVEL-SAND MIXTURES		
			GP		POORLY GRADED GRAVELS, GRAVEL-SAND MIXTURES		
		gravels with over 12% fines	GM		SILTY GRAVELS, POORLY GRADED GRAVEL-SAND- SILT MIXTURES		
			GC		CLAYEY GRAVELS, POORLY GRADEO GRAVEL- SAND-CLAY MIXTURES		
	SANDS MORE THAN HALF COARSE FRACTION IS SMALLER THAN NO. 4 SIEVE SIZE	CLEAN SANDS WITH LITTLE OR NO FINES	SP	· · ·	POORLY GRADED SANDS, GRAVELLY SANDS		
			SW	· · · · · ·	WELL GRADED SANDS, GRAVELLY SANDS		
		Sands With Over 12% Fines	SM	· · · · · · · · · · · · · · · · · · ·	SILTY SANDS, POORLY GRADED SAND-SILT MIXTURES		
			SC		CLAYEY SANDS, POORLY GRADED SAND-CLAY MIXTURES		
FINE GRAINED SOILS MORE THAN HALF IS SMALLER THAN # 200 SIEVE	SILTS AND CLAYS LIQUID LIMIT LESS THAN 50		ML		INORGANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTY OR CLAYEY FINE SANDS, OR CLAYEY SILTS WITH SLIGHT PLASTICITY		
			CL		INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS		
			OL		ORGANIC CLAYS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY		
	SILTS AND CLAY LIQUID LIMIT GREATER THAN 50		мн		INORGANIC SILTS, MICACEOUS OR DIATOMACIOUS FINE SANDY OR SILTY SOILS, ELASTIC SILTS		
			СН		INORGANIC CLAYS OR HIGH PLASTICITY, FAT CLAYS		
			он		ORGANIC CLAYS OF MEDIUM TO HIGH PLASTICITY, ORGANIC SILTS		
	HIGHLY ORGANIC SOILS				PEAT AND OTHER HIGHLY ORGANIC SOILS		

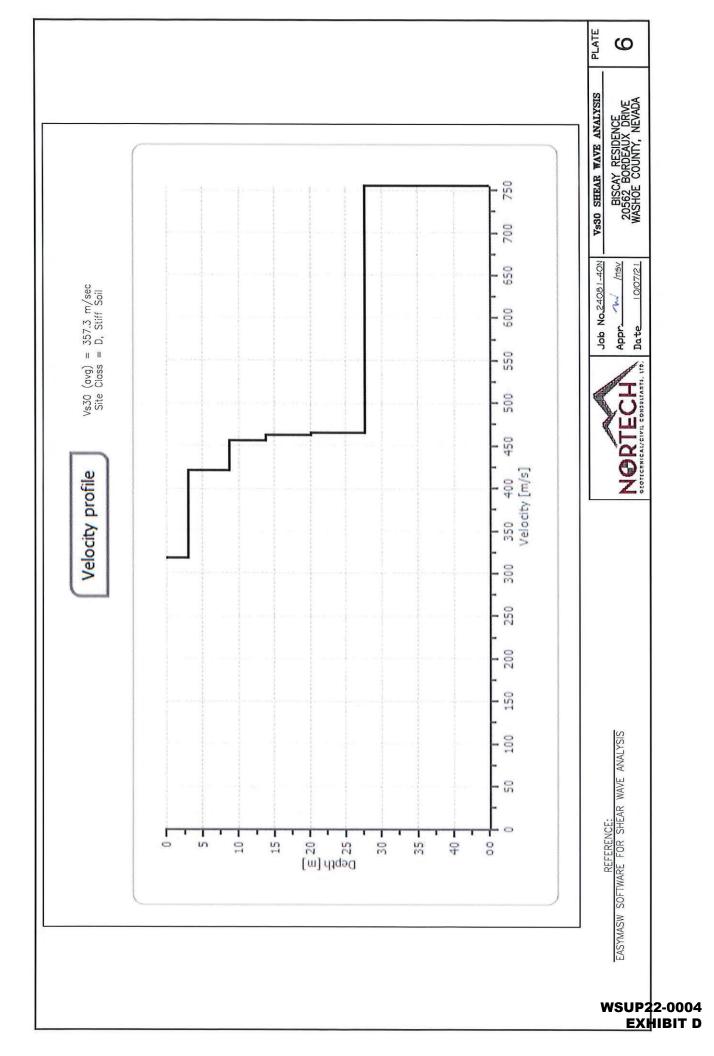


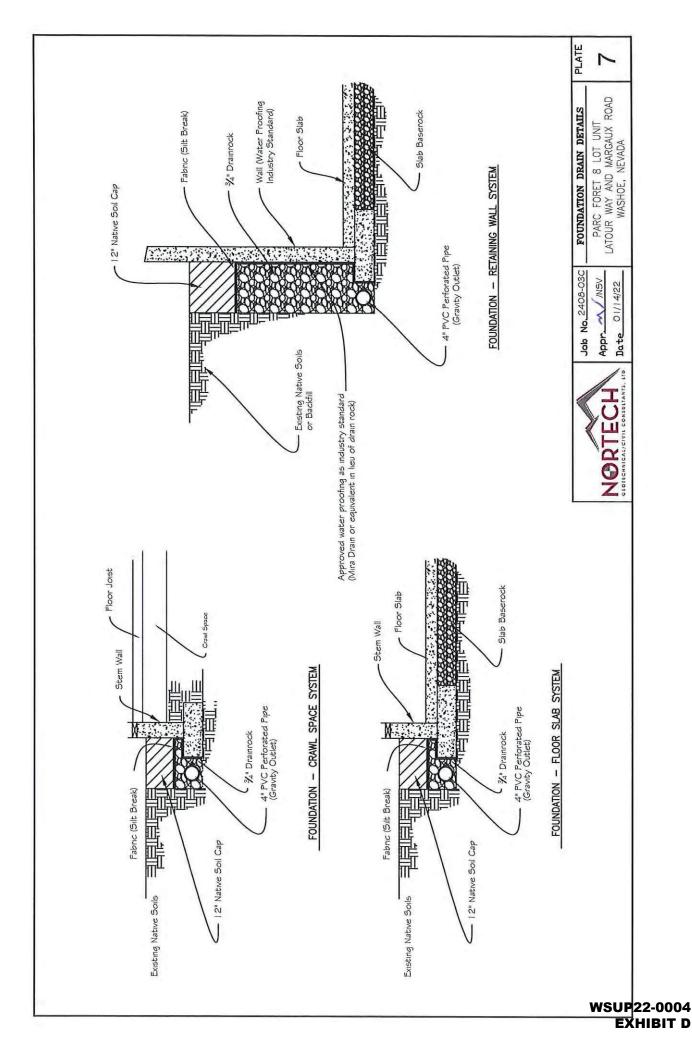
	Job #_	2408-03C	UNIFIED SOIL CLASSIFICATION CHART	PLATE
	Appr	√ /nsv	PARC FORET 8 LOT UNIT	2
, LTD.	Date: _	01/14/22	LATOUR WAY AND MARGAUX ROAD Washoe, Nevada wsup2	2-0004



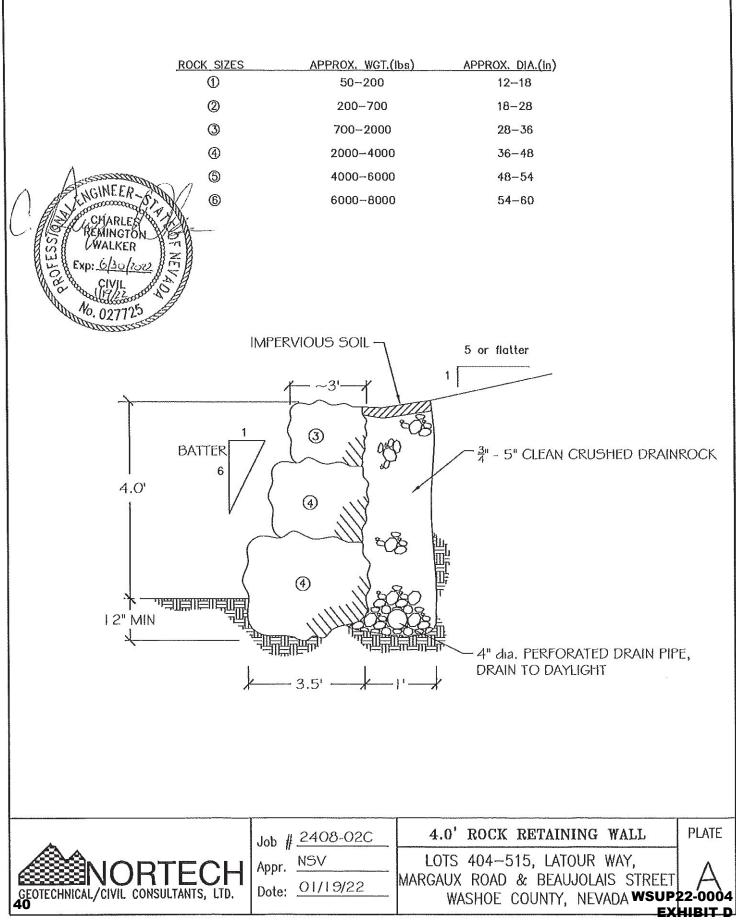
**EXHIBIT D** 







#### RETAINING WALL DETAIL



#### GENERAL NOTES

- SURVEY PROVIDED BY OTHERS, CONTRACTOR TO VERIFY EXISTING CONDITIONS AND VERDICALHORIZONTAL DATUM PRIOR TO THE START OF CONSTRUCTION. CONTRACTOR TO COORDINATE WITH THE SURVEYOR OF RECORD.
- CONSTRUCTION LAYOUT (ALL ACTUAL LINES AND GRADES) SHALL BE STAKED BY A PROFESSIONAL SURVEYOR, REGISTERED IN THE STATE OF NEVADA, BASED ON COORDINATES, DIMENSIONS, BEARINGS, AND ELEVATIONS, AS SHOWN, ON THE PLANS.
- PROJECT CONTROL SHALL BE FIELD VERIFIED AND CHECKED FOR RELATIVE HORIZONTAL AND VERTICAL POSITION PRIOR TO BEGINNING CONSTRUCTION LAYOUT.
- WHEN DIMENSIONS AND COORDINATE LOCATIONS ARE REPRESENTED DIMENSIONS SHALL HOLD OVER COORDINATE LOCATION. NOTIFY THE CIVIL ENGINEER OF RECORD IMMEDIATELY UPON DISCOVERY OF ANY DISCREPANCES.
- BUILDING SETBACK DIMENSIONS FROM PROPERTY LINES SHALL HOLD OVER ALL OTHER CALLOUTS. PROPERTY LINES AND ASSOCIATED BUILDING SETBACKS SHALL BE VERIFIED PRIOR TO CONSTRUCTION LAYOUT.
- CARE INCLUENCEMENT. CONTRACTOR SHALL RESERVE AND PROTECT FROM DAMAGE ALL EXISTING MONUMENTATION DURING CONSTRUCTION THE CONTRACTOR IS DESPONIBLE FOR COORDINATION AND PAYING FOR THE REPLACEMENT OF ANY MOMENTS DAMAGED OR RESIZVED DURING CONSTRUCTION. NEW MONUMENTS SHALL BE REESTABLISHED BY A LICENSED SURVEYOR.
- 7. ALL CONSTRUCTION AND MATERIALS SHALL CONFORM TO THESE PLANS, THE PROJECT SPECIFICATIONS AND THE APPLICABLE REQUIREMENTS OF WASHOE COUNTY.
- 8 THE COMPLETED INSTALLATION SHALL CONFORM TO ALL APPLICABLE FEDERAL, STATE, AND LOCAL CODES, ORDINANCES AND REGULATIONS. ALL PENNTS, LICENSES AND INSPECTIONS REQUIRED BY THE GOVERNING AUTHORITIES FOR THE EXECUTION AND COMPLETION OF WORK SHALL BE SECURED BY THE CONTRACTOR PRIOR TO COMMENSING CONSTRUCTION.
- THE LOADING OF KIRKING CONTROL ON PROOF TO COMMERCING CONSTRUCTOR. THE LOADING OF KIRKING INSTRUMENTS IN THE SHORE ON THE FLARE ARE FOR INFORMATING ON YAR DUE NOT GUARANTEE THE COLLER CONTROL OF THE SHALL HERP LEDATION (IP SEE AND INTERIOL THESE OF ALL INCREMENTATION THE SHALL HERP LEDATION (IP SEE AND INTERIOL THESE OF ALL INCREMENTATION THE SHALL HERP LEDATION (IP SEE AND INTERIOL THESE OF ALL INCREMENTATION TO HERE THE COLLEGATION (IP SEE AND INTERIOL THESE OF ALL INCREMENTATION TO HERE THE COLLEGATION (IP SEE AND INTERIOL THESE OF ALL INCREMENTATION TO HERE INTERIOR AND ALL INVESTIGATION TO SERVER OF CONSTRUCTION TO HERE INTERIOR AND ALL INVESTIGATION TO SERVER OF ALL INCREMENTATION TO HERE INTERIOR AND ALL INVESTIGATION OF ALL INVESTIGATION OF HERE INTERIOR AND ALL INVESTIGATION OF ALL INFORMATION OF ALL INVESTIGATION OF HERE INTERIOR AND ALL INVESTIGATION OF ALL INVESTIGATION OF HERE INTERIOR AND ALL INVESTIGATION OF ALL INVESTIGATION OF HERE INTERIOR AND ALL INVESTIGATION OF ALL INVESTIGATION OF HERE INTERIOR AND ALL INVESTIGATION OF ALL INVESTIGATION OF HERE INTERIOR AND ALL INVESTIGATION OF ALL INVESTIGATION OF HERE INTERIOR AND ALL INVESTIGATION OF ALL INVESTIGATION OF HERE INTERIOR AND ALL INVESTIGATION OF ALL INVESTIGATION OF HERE INTERIOR AND ALL INVESTIGATION OF ALL INVESTIGATION OF HERE INTERIOR AND ALL INVESTIGATION OF ALL INVESTIGATION OF ALL INVESTIGATION OF HERE INTERIOR AND ALL INVESTIGATION OF ALL INVESTIGATION OF
- 10. THE ENGINEER OR OWNER IS NOT RESPONSIBLE FOR THE SAFETY OF THE CONTRACTOR OR HIGHER CREW. ALL 0.5.H.A. REGULATIONS SHALL BE STRICTLY ADHERED TO IN THE PERFORMANCE OF THE WORK.
- 11. THE CONTRACTOR IS RESPONSIBLE FOR MAINTAINING ALL ROADWAYS, KEEPING THEM CLEAN AND FREE OF CONSTRUCTION MATERIALS AND DEBRIS, AND PROVIDING DUST CONTROL AS
- 12. PROPER AND SAFE TRAFFIC CONTROL SHALL BE PROVIDED IN ACCORDANCE WITH WASHOE COUNTY BY THE CONTRACTOR THROUGHOUT CONSTRUCTION.
- 13. CONTRACTOR SHALL PREVENT SEDIMENTS AND SEDIMENT LADEN WATER FROM ENTERING THE STORM DRAINAGE SYSTEM OR PUBLIC RIGHT-OF-WAY.
- ALL CONSTRUCTION MATERIALS SHALL BE NEW AND CONFORM TO WASHOE COUNTY STANDARDS AND CODE: THE USE OF MANUFACTURERS INMERS, MODELS, AND NUMERS IS INTRODED TO ESTALISHS TYLE, CULILIT, PAPERAANCE, AND USE INLESS, PROPOSED SUBSTITUTIONS WILL REQUIRE WRITTEN APPROVAL FROM ENGINEER PRIOR TO INSTALLATION.
- CONCRETE FOR CURBS, SIDEWALK AND DRIVEWAYS SHALL HAVE A MINIMUM COMPRESSIVE STRENOTH OF 3,300 PSI AT 28 DAYS UNLESS OTHERWISE SPECIFIED BY WASHOE COUNTY OR GEOTECHNICAL ENGINEER OF RECORD.

- WINTERIZATION NOTES
  WINTERIZATION IS REQUIRED ON ALL CONSTRUCTION SITE WHICH ARE INACTIVE DURING THE ALL TEMPORARY EROSION CONTROL AND BMP FEATURES SHALL BE REPAIRED AND FUNCTIO PROPERLY PROR TO WINTER SHUTDOWN.
- 3. TEMPORARY VEGETATION PROTECTION FENCING SHALL BE IN PLACE AND/OR INSPECTED.
- 4. DISTURBED AREAS SHALL BE STABILIZED (SEE EROSION CONTROL NOTES FOR MORE INFO).
- ON-SITE CONSTRUCTION SLASH AND DEBRIS SHALL BE CLEANED UP AND REMOVED FROM THE SITE.
- ANENT BMPS SHALL BE INSTALLED WHERE POSSIBLE PER PLAN.
- 7. ALL FILL MATERIAL RETAINED FOR FUTURE BACKFILL MUST BE PROTECTED BY SEDIMENT BARRIERS AND BE COVERED WITH PLASTIC OR OTHER IMPERVIOUS MATERIAL.
- 8. ANY EXCESS EXCAVATED EARTHEN MATERIALS SHALL BE REMOVED FROM SITE IN ACCOR WITH COUNTY GUIDELINES.

#### CONSTRUCTION NOTES

- SUBGRADE DRY DENSI SPECIFICAT PERMITTED DE AND TRENCH BACKFILL SHALL BE COMPACTED TO AT LEAST 15% OF THE MAXIMUM ISITY AS DETERMINED BY ASTM D-468 OR IN ACCORDANCE WITH WASHOE COUNTY ATIONS, FLOCONIG OR JETTING THE BACKFILLED TRENCHES WITH WATER IS NOT
- THE CONTRACTOR SHALL BE RESPONSIBLE FOR DEMOLITION AND DISPOSAL OF EXISTING AC, CURBS, SIDEWALKS, TREES, AND OTHER SITE ELEMENTS WITHIN THE SITE AREA IDENTIFIED IN THE PLANS.
- EXCEPT FOR MATERIALS INDICATED TO BE STOCKPILED OR TO REMAIN ON OWNER'S PROPERTY, CLEARED MATERIALS SHALL BECOME CONTRACTOR'S PROPERTY, REMOVED FROM THE SITE, AND DISPOSED OF PROPERLY.
- 3. ITEMS INDICATED TO BE SALVAGED SHALL BE CAREFULLY REMOVED AND STORED AT THE PROJECT SITE AS DIRECTED BY THE OWNER.
- ALL LANDSCAPING, PAVEMENT, CURBS AND SIDEWALKS, BEYOND THE IDENTIFIED SITE AREA, DAMAGED DURING THE CONSTRUCTION SHALL BE REPLACED TO THEIR ORIGINAL CONDITION OR BETTER BY THE CONTRACTOR.
- 5. SAWCUT STRAIGHT MATCHLINES TO CREATE A BUTT JOINT BETWEEN THE EXISTING AND NEW PAVEMENT.
- UTILITIES ADJUST ALL INCIDENTAL STRUCTURES, MANHOLES, VALVE BOXES, CATCH BASINS, FRAMES AND COVERS, ETC. TO FINISHED GRADE.
- CONTRACTOR SHALL ADJUST ALL EXISTING AND/OR NEW FLEXIBLE UTILITIES (WATER, TV, TELEPHONE, ELEC., ETC.) TO CLEAR ANY EXISTING OR NEW GRAVITY DRAIN UTILITIES (STORM DRAIN, SAMTRAY SEWER, ETC.) F CONFLICT OCCURS.
- CONTRACTOR SHALL COORDINATE WITH PRIVATE UTILITY COMPANIES FOR THE INSTALLATION OF OR ADJUSTMENT TO GAS, ELECTRICAL, POWER AND TELEPHONE SERVICE.
- 4. BEFORE BACKFILLING ANY SUBGRADE UTILITY IMPROVEMENTS CONTRACTOR SHALL SURVEY AND RECORD MEASUREMENTS OF EXACT LOCATION AND DEPTH AND SUBMIT TO OWNER.
- 5. ALL UTILITIES SHALL BE INSTALLED IN ACCORDANCE WITH WASHOE COUNTY, TMWA AND THE APPROPRIATE UTILITY PROVIDER COMPANY STANDARDS.
- PROVIDE A MINIMUM OF TWELVE INCHES VERTICAL CLEARANCE BETWEEN ADJACENT UTILITY PIPES AT UTILITY CROSSING UNLESS OTHERWISE NOTED ON THE PLANS OR BY AGENCY BEGIN LATIONS
- 7. USE H-20 RATED LITLITY BOXES AND LIDS IN PAVED AREAS OR AS REQUIRED BY WASHOE COUNTY, TMWA OR APPROPRIATE UTILITY COMPANY FOR TRAFFIC RATING.
- IF UNDERGROUND UTILITIES (W, SO, SS, GAS, ELEC, TELE, IRRIG, ETC) ARE DISCOVERED BY NOT SHOWN ON THESE PLANS, NOTIFY THE ENGINEER BEFORE PROCEEDING IF MODIFICATIONS ARE NECESSARY.
- REFER TO WASHOE COUNTY STANDARDS FOR ADDITIONAL PIPE TRENCHING AND BEDDING INSTALLATION PROCEDURES.
- ALL EXCAVATIONS FOR UTILITY INSTALLATION SHALL BE ADEQUATELY QUARDED WITH BARRERS AND LIGHTS SO AS TO PROTECT THE FRAIL OF FOUN HAZARO. STREETS, SIDEWALKS, PARKWAYS AND OTHER PROPERTY DISTURBED IN THE COURSE OF THIS WORK SHALL BE RESTORED IN A MANNERS ASTISFACTORY TO THE OWNER.

#### RECORD DRAWINGS NOTE

In the second second

- WASHOE COUNTY NOTES
- THE CONTRACTOR SHALL CALL THE WARKER COUNTY ENGINEERING DAYISON FORTY-GIRM ( W) HOURS PROR TO THE START OF CONSTRUCTION. THE CONTRACTOR SHALL CALL TWENTY-FOUR CALHORS PROR TO REQUED SNEPCTONN ADD TSTITUL THE REQUIRED SNEPCTORY ON TSTITULA VEL STED ON THE SNEPCTON RECORD SINGLE WITH EACH PRIMIT. THE CONTRACTOR HUST HAVE THE PERSIM TWINEER AND THE DESCRIPTION LISTED ON THE INSPECTION RECORD TO SOLUCINE DEVICETORY AND TSTITULA VEL SUBJECT AND THE DESCRIPTION LISTED ON THE INSPECTION RECORD TO SOLUCINE DEVICED IN THE PERSIM TANKED AND THE DESCRIPTION LISTED ON THE INSPECTION
- ALL WORK SHALL CONFORM TO THE STANDARD SPECIFICATIONS AND DETAILS FOR PUBLIC WORKS CONSTRUCTION AS
  ADOPTED BY WASHOE COUNTY.
- DETALS NOT SHOWN ON THESE DRAWINGS SHALL BE AS CONTAINED IN THE BOOK OF STANDARD DETAILS FOR PUBLIC WORKS CONSTRUCTION AS ADOPTED BY WASHOE COUNTY.
- ALL LAND CLEARING OR FILLING OF LAND IS SUBJECT TO THE REGULATIONS OF THE NEVADA DEPARTMENT OF ENVIRONMENTAL PROTECTION. ANY LAND CLEARING OR FILLING OF LAND OF ONE (1) ACRE OR MORE WILL REQUIRE A PERMIT FROM THE NEVADA DEPARTMENT OF ENVIRONMENTAL PROTECTION.
- ALL WATERLINE, AND RISERS SHALL BE DISINFECTED IN ACCORDANCE WITH STATE HEALTH DEPARTMENT REQUIREMENTS AND AWWA DBI PRIOR TO ACCEPTANCE. THE CONTRACTOR SHALL BE RESPONSIBLE FOR COLLECTING ALL REQUIRED SAMPLES AND THE COST OF ANALYSIS AT A NEWADA APPROVED LABORATORY.
- PRIOR TO THE RELEASE OF ANY FINANCIAL ASSURANCES FOR PRIVATE IMPROVEMENTS, A LETTER, STAMPED AND SIGNED BY A LICENSED ENGINEER, SHALL BE SUBMITTED TO WASHOE COUNTY ENGINEERING CERTIFYING THAT THE PRIVATE IMPROVEMENTS HAVE BEEN CONSTRUCTED IN ACCORDANCE WITH THE APPROVED FAMIL.
- 7. CONTRACTOR TO VERIFY SEWERWATER UTILITY CONNECTIONS WITH WASHOE COUNTY AND TIMINA INSTALL ALL UTILITIES IN AN APPROVED TRENCH AND IN ACCORDANCE WITH ALL APPLICABLE CODES AND ORDINANCES.
- ALL PARCELS WITHIN ANY APPROVED SUBDIVISION SHALL REQUIRE THAT A NEVADA REGISTERED CIVIL ENGINEER OR A NEVADA REGISTERED LAND SURVEYOR SUBMIT A CERTIFICATION LETTER TO THE BUILDING OF RICAL PRIOR TO THE SCHEDRING OF BURGETONIE OR THE ECU LIVING.
- Longitude value
   Longitude
   Longi

# EROSION CONTROL & RE-VEGETATION NOTES

EROSION AND SEDIMENT CONTROL MATERIALS SHALL BE CERTIFIED AS WEED-FREE 3. THE USE OF STRAW OR HAY BALES AS AN EROSION CONTROL METHOD IS PROHIBITED

- The Dec 9 Hold Conference on Hold Conference o
- the CONTRACTOR SHALL MAN TAKE ADEQUATE DUST CONTROL PRIS TATE AND ADDRESS TO STARALING SPECIFICATIONS
   to CONTRACT SHALL MAN TAKE ADEGUATE DUST CONTROL PRIS TATE AND ADDRESS TO STARALING SPECIFICATIONS
   to CONTRACT MAKING ADDRESS ADDRE
- WINTEROLITON, EROBON CONTROL MEASURES AND DETAILS AS SHOWN ON THIS PLAN ARE INTERIOED AS A QUICE A MEE BUICESTED MINIAU METRODO DE CONTROLLANS TRADICIÓN DURANS CONTROLTON THE CONTROLTON EN ADMINIÓN DE ANTROLOGIA DE CONTROL MEASURES AND DETAILS AS SHOWN ON THIS PLAN ARE INTERNOT. THE CONTROLTON EN ADMINIÓN EROBONICONTROL MEASURES AND MEETRODO DE ADMINIÓN DURAN CONTROL DE ADMINIÓN ADMINIÓN DE ADMINIÓN ADMINIÓN ADMINIÓN DE ADMINIÓN ADMINIÓN DE ADMINIÓN DE ADMINIÓN AD
- FINCLENENT WEATHER IS FORECAST, CONTRACTOR SHALL TAKE NECESSARY STEPS TO PROTECT AREAS DISTURE BY CONSTRUCTION FROM REGISTION ADUORS BUSICIENT DISCHARGE OF EARTHEN MATERIALS FROM THE STEL 8. STOCHALES SHALL BE PROTECTED FROM EROSION. THIS MAY CONSIST OF PLACING BMP FENCINGI DIKES AROUND STOCHALES AND/OR COVERNM WITH FLASTIC.
- ALL TEMPORARY EROSION CONTROL FEATURES SHALL BE INSPECTED DALY AND PRIOR TO INCLEMENT WEATHER AND CORRECTIVE ACTION TAKEN AS NECESSARY TO INSURE PROPER FUNCTION.
- 10. THE AREA OF SOIL AND VEGETATION DISTURBANCE SHALL BE LIMITED TO WHAT IS REQUIRED FOR CONSTRUCTION PURPOSES. EXCEPT WHERE REQUIRED FOR ACCESS, THERE SHALL BE IND INSTURBANCE IN AREAS TO BE LEFT IN A NATURAL STATE CONSTRUCTION TRAFFIC SHALL BE LIMITED TO AREAS TO BECOME PERMANENT CIRCULATION (E.G., ROUDINIYS AND PARKING AREAS, ETC.)
- 11. DEWATERNOL IF NECESSARY, SHALL BE COMPLETED IN A MAININER SO AS TO ELIMINATE THE DISCHARGE OF EARTHEN MATERNALS FROM THE BITE
- 12. ALL BARREN AREAS DISTURBED BY CONSTRUCTION SHALL BE RE-VEGETATED IN ACCORDANCE WITH THE GOVER AGENCY REGULATIONS. APPLICATION OF A MULCH MAY ENHANCE VEGETATIVE ESTABLISHMENT.
- 13. RETULLITON NO MANTENNES OF ERGON CONTOL LEGISLES AND ADMINIST COMPLAND, AND RESPONDENT OF THE CONTRUCTOR THE CONTOL SHALL BE RED REMARKED EF OF THE PREVENTION OF SUMPCANT ENGINE AND SILTATON INTERNO THE STORM DRAIN SYSTEM, MATURAL DRAINAGE COURSES AND/OR INTELINOU DVIA JULCENT ROUTINARY AND PROPERTIES.
- 14. VEGETATION DISTURBANCES SHALL BE LINITED TO THOSE AREAS IDENTIFIED ON THE CONSTRUCTION PLANS AND AS SLATED FOR DEVELOPMENT OR CONSTRUCTION STADING.
- 15. NATIVE AND COMPATIBLE NON-NATIVE SPECIES, ESPECIALLY DROUGHT RESISTANT SPECIES, SHALL BE USED FOR RE-VEGETATION IN ACCORDANCE WITH COUNTY STANDARDS.

ABBREVIATIONS ASPHALT CONCRETE AREA CRAN BUILDING BUILDING BUILDING BUILDING BUTTOM OF WALL CATCH BUSIN CONTRELINE CONTRUCATED METAL PIPE CONTRUCATED METAL PIPE CONTRUCATED METAL DIST CONTROL FORM CONTROL POINT DELTA MIN OF OVHICH PLLE PVG PVG PVG R R R R SSUM R C.UW S SD SSW SSW S SSW S SSW T T T R ANS. TC TD T TP TRANS. TC TD TP UGE UGE UNO W W W W W MNIMUM OUTFALL OVERHEAD OUTFALLO OWENERATION PROCESSITY LINE REPORT OF THE ADDRESS PROCESSITY LINE ROUTE OF THE STOCK DOWN MARKALE MAR CONTRELE POINT DELTA DELTA DELTA DELTA DELTA DENTERNAT DUCTE EIRON PIPE EVISTING PINSH GRADE FINSH GRADE FINSH GRADE FINSH GRADE FINSH GRADE FINSH GRADE FUNDATION GRADE BREAK GLAS LINE HEICHT HIGH POINT NVERT ELEVATION INVERT ELEVATION CP DW DIA\_Ø DIP EXIST./E FF FG FH FL FND G8 GL /EX



	NI ROJE ITTI PROJECT SITE
DEMOLITION PLAN	The second
IECTIONS	VICINITY MAP NOT TO SCALE

SHEET INDEX

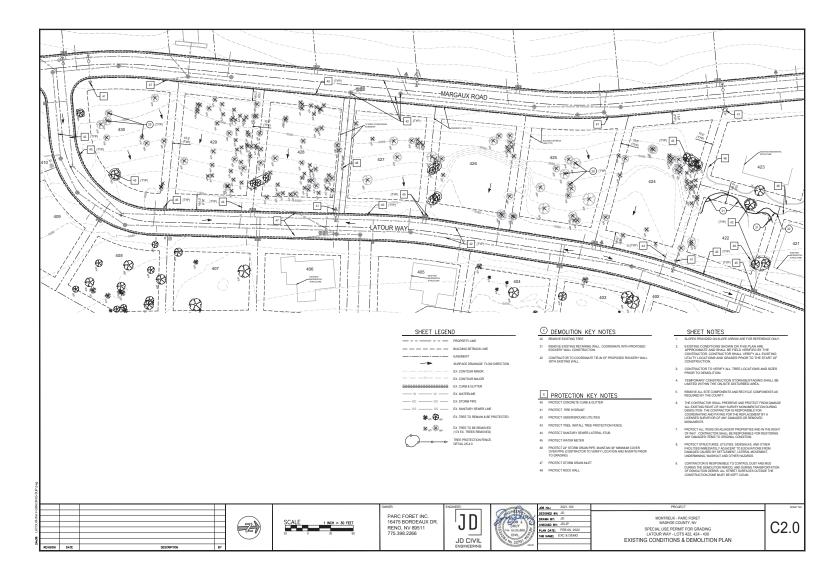
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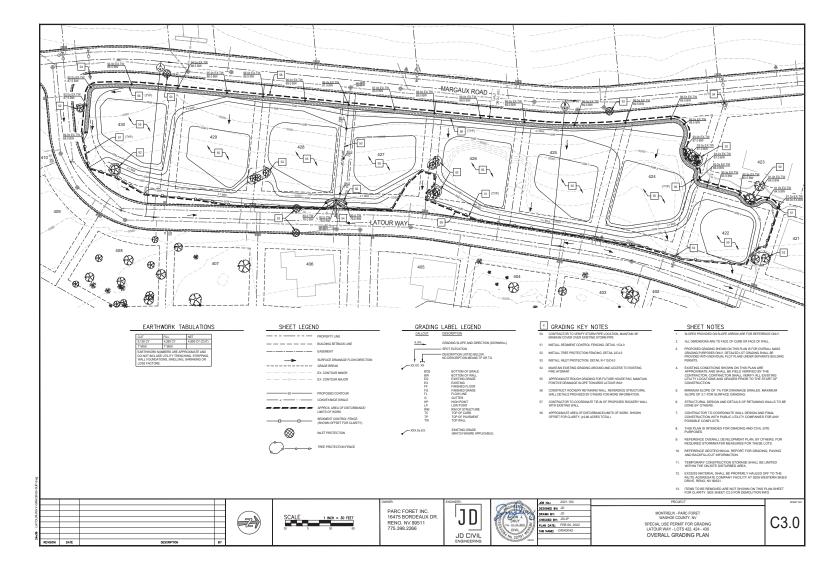
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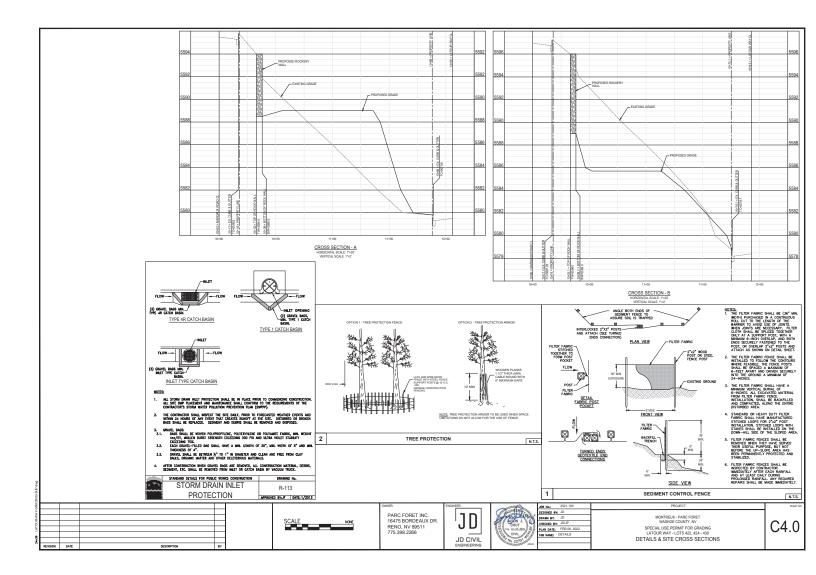
DETAILS & SITE CROS

GRA						OWNER:	ENGINEER:	denter and	JOB No.: 2021.100	PROJECT	SHEET ND.
24636 LATOURWAY					SCALE NONE	PARC FORET INC. 16475 BORDEAUX DR. RENO, NV 89511 775.398.2266		A LALAND A LA	DESIGNED (MY: JD DRAWN (MY: JD CHEOXED (MY: JD(JP) PLAN DATE: FEB 06, 2022 TAG NAME: NOTES	MONTRELIX - PARC FORET WASHIG COUNTY, NY SEEQLU, USE PRIMIT FOR GRADING LATOUR WIY - LOTS 422, 424 - 430 GENERAL, CIVIL, NOTES	C1.0
R	VISION	DATE	DESCRIPTION	BY			ENGINEERING				









#### Gravity Retaining Wall LIC#: KW-06014449, Build:20.22.1.12

**DESCRIPTION**; 4 foot wall

NORTECH

Project File: Parc foret walls.ec6 (c) ENERCALC INC 1983-2021

#### Criteria Soil Data **Retained Height** 4.0 ft Allow Soil Bearing = 3,000.0 psf E. R and and Wall height above soil Ξ ft **Coulomb Soil Presure calculation** Slope Behind Wal = 3 Soll Friction Angle 32.0 deg == Height of Soil over Toe == in Active Pressure:Ka\*Gamma= 0.0 psf/ft Soil Density 0.0 psf/ft = 108.0 pcf Passive Pressure:Kp\*Gamma Footing||Soil Friction 0.40 = Soil height to ignore for passive pressure = 12 in Thumbnail Surcharge Loads Lateral Load Applied to Stem Adjacent Footing Load Surcharge Over Heel psf Adjacent Footing Load = lbs Lateral Load #/ft >>>Used To Resist Sliding & Overturning ...Height to Tor Footing Width --ft = ft Surcharge Over Toe psf Eccentricity ---in ...Height to Boltom = ft Used for Sliding & Overlurning Wall to Ftg CL Dist = ft Footing Type Line Load Base Above/Below Soil ft at Back of Wall Wind on Exposed Stem = psf Poisson's Ratio -0.3 Kae for seismic earth pressure = 0.6916 508.86 lbs Earth Pressure Seismic Load Added seismic base force Ka for static earth pressure = 0.3147 Design Kh 0.20 g <<---- Notel These are horizontal components 0.3769 Difference: Kae - Ka = Using Mononobe-Okabe / Seed-Whitman procedure **Design Summary** Rubble masonry, mortar bonded Stem Analysis Data (Unreinforced material) **Total Bearing Load** 2,675.43 lbs Wall Material Weight 150.0 pcf -Resultant Exceeds Ftg. Width! ...resultant ecc. Fc : Max. Allow, Compression = 100 psi Fc ; Max, Allow, Tension 10 psi = Soil Pressure @ Toe 1,476.03 psf NG = Front Batter Distance 8.0 in = Soil Pressure @ Heel = 0.0 psf NG Thickness @ Top of Stem ...... 38.0 in Allowable psf = **Back Batter Distance** in Soil Pressure Less Than Allowable ACI Factored @ Toe 2,066.44 psf @ Height #1 @ Height #2 @ Height #3 = ACI Factored @ Heel = 0.0 psf Footing Shear @ Toe = 0.0 psi OK **Height above Footing** = 4 ft 2 ft 0.0 ft Footing Shear @ Heel = 0.0 psi OK 38.0 in Wall Thick. @ Height = 42.0 in 46.0 in Allowable 82.158 psi = Section Modulus = 2,888.0 in^3 3,528.0 in^3 4,232.0 in^3 **Sliding Stability Ratio** 1.146 Ratio < 1.1 = Moment @ Height ----0.0 ft-# 604.40 ft-# 2.332.46 ft-# Sliding Calcs (Vertical Component NOT Used) Vertical Load @ Height = 0.0 lbs 1,000.0 lbs 2,100.0 lbs Lateral Sliding Force lbs 0.0 lbs less 100% Passive Force -2.809 psi Actual Unit Tension 11 0.0 psi 0.07165 osi less 100% Friction Force= -1,070.17 lbs Actual Unit Compression == 0.0 psi 4.040 psi 10.418 psi 0.0 lbs OK Added Force Reg'd = Shear @ Section = 0.0 lbs 552.07 lbs 1,165.35 lbs ....for 1.5 Stability = 330.4 lbs NG Actual Unit Shear 17 0.0 psi 0.0 psi 0.0 psi Load Factors **Building Code** Dead Load 1.200 1.600 Live Load Earth, H 1.600 Wind, W 1.000

Seismic, E

1.000

# Gravity Retaining Wall

#### LIC#: KW-06014449, Build:20.22.1.12 DESCRIPTION: 4 foot wall

# Footing Strengths & Dimensions

Toe Width	=	ft
Heel Width	= 33	3333333
Total Footing Widtł	=	3.833
Footing Thickness	-	12.0 in
Key Width	=	24 in
Key Depth	=	in
Key Distance from Toe	12	2 ft
Footing Concrete Densi	Fy = ly =	60000 psi 150 pcf
Min. As %	=	0.0018
Cover @ Top = 2i	in @E	ltm.≓ 3 in

#### NORTECH

Project File: Parc foret walls.ec6 (c) ENERCALC INC 1983-2021

Footing Design	Res	sults	
		<u>Toe</u>	<u>Heel</u>
Factored Pressure	=	2,066.44	0.0 psf
Mu' : Upward	=	0.0	0.0 ft-#
Mu': Downward	Ħ	0.0	0.0 ft-#
Mu: Design	=	0	0 ft-#
Actual 1-Way Shear	=	*Beyond Toe	0.0 psi
Allow 1-Way Shear *Critical section for o	= ne-w	43.818 ay shear falls beyor/	43.818 psi nd the end of the toe.
Toe Roinforcing Heel Reinforcing Key Reinforcing	¥	None Spec'd None Spec'd # 7 @ 12.00 in	
Other Acceptable SI Toe: phiMn = phi'5' Heel: phiMn = phi'5' Key: No key define	iamb Iamb	da'sqrl(fc)'Sm	

# Summary of Overturning & Resisting Forces & Moments

		OV	OVERTURNING				
Item		Force lbs	Distance ft	Moment ft-#			
Heel Active Pressure	=						
Surcharge Over Toe	=	0.0	0.0	0.0			
Adjacent Fooling Load	=	0.0	0.0	0.0			
Added Lateral Load	=	0.0	0.0	0.0			
Load @ Stem Above Soll	₽	0.0	0.0	0.0			
Seismic Load	<b>=</b>	508,86	3.0	1,526.57			
Seismic Stem Self Wt	=		0.0				
Total	-	933.71	0.T.M.	2,234.66			
Resisting/Overturnin	ig R	atio	=	= 2,447			
Vertical Loads use	d fo	r Soll Press	ure =	2,675.43 lbs			

		R		TING	
		Force lbs	D	lstance ft	Moment ft-#
Soil Over Heel	=	0.0		3.833	0.0
Sloped Soll Over Heel	1	.0000130		3.833	.0000480
Surcharge Over Heel	Ħ	0.0		0.0	0.0
Adjacent Footing Load	=	0.0		0.0	0.0
Axial Dead Load on Ste	m ≕	0.0		0.0	0.0
Soil Over Toe Surcharge Over Toe	=	0.0		0.0	0.0
	=	0.0		0.0	0.0
Stem Weight	=	2,100.25		2.078	4,364.85
Earth above Sloping Ste	en =	0.180		3.833	0.690
Footing Woight	=	575.0		1.917	1,102.08
Key Weight	=	0.0		3.0	0.0
Verl. Component	=	0.0		0.0	0.0
Tot	al =	2,675.43	lbs	R.M.=	5,467.62

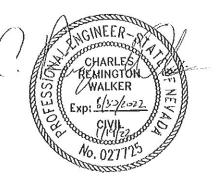
Vertical component of active pressure NOT used for soil pressure

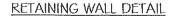
#### Tilt

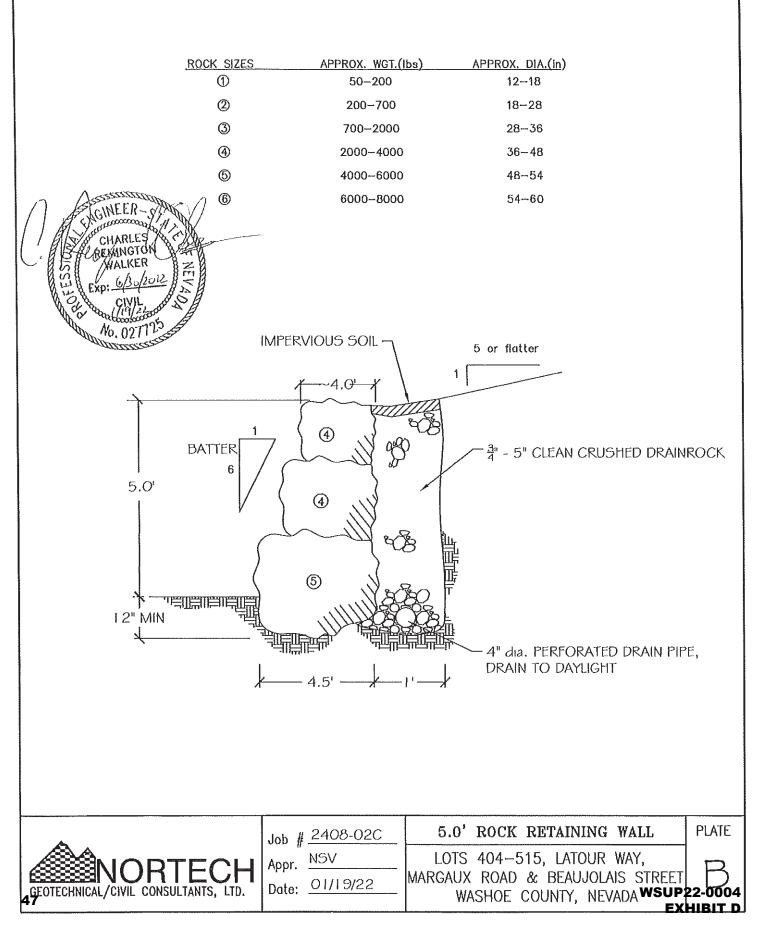
#### Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

Soil Spring Reaction Modulus	pØ50
Horizontal Dell @ Top of Wall (approximate only)	0.04278
The above calculation is not valid if the heel soil bea	aring pressure exceeds that of the toe, /
because the wall would then tend to rotate into the r	retained soil.







ravity Retainin	-		NORTECH			Project File: Parc (c) ENERC/	LC INC 1983-202
ESCRIPTION: 5 f	oot wall						
Criteria			Soil Data				
Retained Height Mall height above soil Slope Behind Wal Height of Soil over Toe Soil Density	= 5.0 ft = ft = 3 = it = 108.0 p	1	Allow Soil Bearing = 3,0 Coulomb Soil Presure calculation Soil Friction Angle = Active Pressure:Ka*Gamma= Passive Pressure:Kp*Gamma Footing  Soil Friction = Soil height to ignore for passive pressure =	000.0 psf 32.0 deg 0.0 psf/ft 0.0 psf/ft 0.40 12 In			
						Thumbnail	
Surcharge Loads			Lateral Load Applied to	Stem	Adjacent	Footing Load	
Surcharge Over Heel >>>Used To Resist S Surcharge Over Toe Used for Sliding & Ove	liding & Overtu	osf rning osf	Lateral Load = Height to Top = Height to Bottorr =	#//ft ft ft	Adjacent Foc Footing Widt Eccentricity Wall to Ftg C Footing Type Base Above/	h = EL Dist =	lbs ft in ft Line Load
			Wind on Exposed Stem =	psf	at Back of	Prop.	ft
Earth Pressure S Design Kh Using Mononobe-Okab Design Summary	= 0.20 g e / Seed-Whitr	)	Kae for seismic earth pressure Ka for static earth pressure Difference: Kae - Ka dure Rubble masonry, morta	= 0.6916 = 0.3483 = 0.3434	<< Note! T	hic base force These are horizon <b>is Data</b> <u>(Unreh</u>	•
Total Bearing Load	= 3,738,0	4 lbs	Wall Material Weight =	150.0 pcf			
.,resultant ecc. Resultant Excee Soil Pressure @ Toe Soil Pressure @ Heel Allowable	= 1,767.2	8 psf NG 0 psf NG	Front Balter Distance = Thickness @ Top of Stem =	10.0 in 44.0 in	Fc : Max. Allow Fc : Max. Allow	r. Compression = r. Tension ==	
Soil Pressure Les ACI Factored @ Toe	s Than Allowal = 2,474.1		Back Batter Distance =	in @ Heig	ht#1 @	9 Height #2	@ Height #3
ACI Factored @ Heel Footing Shear @ Toe Footing Shear @ Heel Allowable Sliding Stability Ratio Sliding Catcs (Vertical Lateral Sliding Force less 100% Passive Fo less 100% Friction For Added Force Req'd for 1.5 Stability	$\begin{array}{rcl} = & 0. \\ = & 0. \\ = & 82.15 \\ = & 1.11 \\ Component NC \\ = \\ rcce & - & 0. \\ cce & - & 1.495.2 \\ = & 0. \end{array}$	0 psi OK 0 psi OK 8 psi 2 Ratio < 2T Used) lbs 0 lbs	Height above Footing Wall Thick. @ Height Section Modulus 1.: Moment @ Height Vertical Load @ Height Actual Unit Tension Actual Unit Compression Shear @ Section	= 4,23 = 170.3 = 562 = -0.53 = 1.4 = 297	2.50 lbs 360 psi 502 psi 1.30 lbs	2 ft 50.0 in 5,000.0 in^3 1,521.32 ft-# 1,762.50 lbs 0.7137 psi 6.589 psi 965.63 lbs	0.0 ft 54.0 in 5,832.0 in <sup>4</sup> 4,193.35 ft- 3,062.50 lbs 3.902 ps 13.354 ps 1,732.28 lbs
oad Factors Building Code Dead Load		200	Actual Unit Shear	22	0.0 psi	0.0 psi	0.0 ps

....

# **Gravity Retaining Wall**

#### LIC#: KW-06014449, Build:20.22.1.12 DESCRIPTION: 5 foot wall

Footing Strengths	& Din	nensions
Toe Width	Ξ	ft
Heel Width	=	4.5
Total Fooling Width	=	4.50
Footing Thickness	Ħ	12.0 in
Key Width	=	24 in
Key Depth	÷	in
Key Distance from Toe	=	2 ft
ľc = 3000 psi	Fy ≕	60000 psi
Footing Concrete Densi	ly =	150 pcf
Min. As %	=	0.0018
Cover@Top ≃ 2	in @B	lm.= 3 in

# NORTECH

Project File: Parc foret walls.ec6

(c) ENERCALC INC 1983-2021

Footing Design	Re	sults	
		Τοθ	Hoel
Factored Pressure	=	2,474.19	0.0 psf
Mu': Upward	t:2	0.0	0.0 ft-#
Mu': Downward	Ħ	0.0	0.0 ft-#
Mu: Design	=	0	0 ft-#
Actual 1-Way Shear	÷	*Beyond Toe	0.0 psi
Allow 1-Way Shear *Critical section for o	= ne-∖	43.818 way shear falls be	43.818 psi yond the end of the toe.
Toe Reinforcing Heel Reinforcing Key Reinforcing	=	None Spec'd None Spec'd # 7 @ 12.00 in	
Other Acceptable Si Toe: phiMn = phi'5' Heel: phiMn = phi'5' Key: No key define	lam Iam	bda'sqrl(fc)'Sm	

# Summary of Overturning & Resisting Forces & Moments

		OV	ERTURNI	۱G
Itom	_	Force Ibs	Distance ft	Moment ft-#
Heel Aclive Pressure	=			
Surcharge Over Toe	=	0.0	0.0	0.0
Adjacent Footing Load	=	0.0	0.0	0.0
Added Lateral Load	₩	0.0	0.0	0.0
Load @ Stem Above Soil	=	0.0	0.0	0.0
Seismic Load	÷	667.53	3.60	2,403.09
Seismic Stem Self Wt	=		0.0	
Total	=	1,344.54	O.T.M.	3,757.13
Resisting/Overturnin	g F	latio	Ħ	2.403
Vertical Loads use	d fo	r Soil Press	ure =	3,738.04 lbs

		R	ESISTING	
_		Force Ibs	Distance ft	Moment ft-#
Soil Over Heel	=	0.0	4.50	0.0
Sloped Soil Over Heel	=	.0000130	4.50	.0000560
Surcharge Over Heel	=	0.0	0.0	0.0
Adjacent Footing Load	=	0.0	0.0	0.0
Axial Dead Load on Ste	em =	0,0	0.0	0.0
Soil Over Toe	=	0.0	0,0	0.0
Surcharge Over Toe	=	0.0	0.0	0.0
Stem Weight	=	3,062.81	2.451	7,508.35
Earth above Sloping St	en =	0.2250	4.50	1.013
Footing Weight	=	675.0	2.250	1,518.75
Key Weight	÷	0.0	3.0	0.0
Vert. Component	<b>=</b>	0.0	0.0	0.0
To	otal ≈	3,738.04	lbs R.M.≓	9,028.11

Vertical component of active pressure NOT used for soil pressure

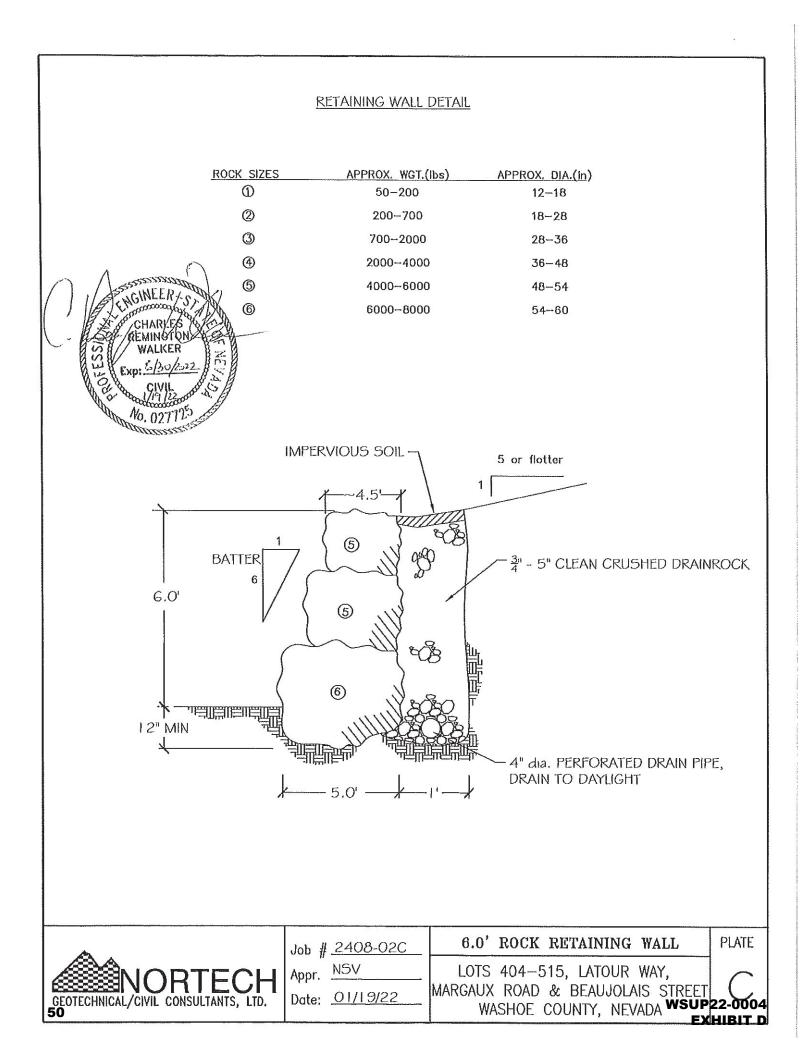
#### Tilt

# Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

Soil Spring Reaction Modulus	p <b>é</b> /50
Horizontal Defl @ Top of Wall (approximate only)	0.05455
The above calculation is not valid if the heel soil bea	ring pressure exceeds that of the toe,
because the wall would then tend to rotate into the re-	etained soil.





# Gravity Retaining Wall LIC# : KW-06014449, Build:20.22.1.12

DESCRIPTION: 6 foot wall

Criteria			Soil Data				
Retained Height	=	6.0 ft	Allow Soil Bearing = 3	,000.0 psf	9 <b>7</b>		
Wall height above soil	=	ft	Coulomb Soil Presure calculatio	•		, 1	and the second second
Slope Behind Wal	Π	3	Soil Friction Angle	32.0 deg			and the second s
Height of Soil over Toe	=	in	Active Pressure:Ka*Gamma=	0.0 psf/ft	1.12.24.27.24.24	E.	
Soil Density	=	108.0 pcf	Passive Pressure:Kp*Gamma	0.0 psf/ft			
o on poneny		100.0 poi		oto positi			
			Footing  Soil Friction =	0.40			
			Soil height to ignore	0.40			
			for passive pressure =	12.0 in			
					The second second second		
						Thumbnail	
						папрпав	
Surcharge Loads			Lateral Load Applied to	Stem	Adjacent Foo	oting Load	
Surcharge Over Heel	=	psf	Lateral Load =	#/ft	Adjacent Footing	Load =	lbs
>>>Used To Resist S			Height to Top =	ft	Footing Width	=	ft
Surcharge Over Toe Used for Sliding & Ov	= orfurn	psf	Height to Botton =	ft	Eccentricity	=	in
osca for bilding a Ov	citum	ing			Wall to Ftg CL D	ist =	ft
					Footing Type	Dall	Line Load
					Base Above/Belo at Back of Wa		ft
			Wind on Exposed Stem =	psf	at back of wea		
					Poisson's Ratio		0.3
Earth Pressure S	Seisn	nic Load	Kae for seismic earth pressure	= 0.6916	Added seismic b	ase force	908.61 lbs
Design Kh	=	0,20 q	Ka for static earth pressure	= 0.3482	<< Note! Thes	e are horizon	al components
			Difference: Kae - Ka	= 0.3434			
Using Mononobe-Okab		ed-vvniman proce	( <u> </u>				
Design Summary			Rubble masonry, mort			Data <u>(Unreh</u>	forced material)
Total Bearing Load	11	5,150.65 lbs	Wall Material Weight =	150.0 pe	:f		
resultant ecc. Resultant Excer		11.450 in a. Width!			Fc : Max. Allow. Co		AND - 1923
Soil Pressure @ Toe	=	2,005.11 psf NG	Front Batter Distance =	12.0 in	Fc : Max. Allow. Te	nsion =	= 10 psl
Soil Pressure @ Heel	=	0.0 psf NG	Thickness @ Top of Stem =				
Allowable	=	psf	Back Batter Distance =				
Soil Pressure Les ACI Factored @ Toe	s ina					ight #2	@ Height #3
ACI Factored @ Heel	=	2,807.15 psf 0,0 psf		- CB ITE	ngnu#i @in	ngnit #£	@Theight #5
Footing Shear @ Toe	=	0.0 psi OK	Hatatat alcave Faatos	_	4.6	0.4	0.04
		0.0 psi OK	Height above Footing Wall Thick. @ Height	=	4 ft 56.0 in	2 ft 30.0 in	0.0 ft 64.0 in
	=		Section Modulus			00.0 in^3	8,192.0 in^
Footing Shear @ Heel Allowable	11 11	82.158 psi		0,	212.01110 7,2		25
Footing Shear @ Heel Allowable		82.158 psi 1.126 Ralio < 1	11	- 7	N N N N N N N N N N N N N N N N N N N		
Footing Shear @ Heel Allowable Stiding Stability Ratio Stiding Calcs (Vertical	11 II	1.126 Ratio < onent NOT Used)	1.4 Moment @ Height			9.92 ft-#	
Footing Shear @ Heel Allowable Sliding Stability Ratio Sliding Calcs (Vertical Lateral Sliding Force	= = Comp =	1.126 Ralio < oonent NOT Used) lbs	1.( Moment @ Height Vertical Load @ Height	= 1,	350.0 lbs 2,8	00.0 lbs	4,350.0 lbs
Footing Shear @ Heel Allowable Sliding Stability Ratio Sliding Calcs (Vertical Lateral Sliding Force less 100% Passive Fo	= ≡ Comp ≡ (ce= ·	1.126 Ratio < bonent NOT Used) lbs . 0.0 lbs	1.4 Moment @ Height Vertical Load @ Height Actual Unit Tension	= 1, = -0	350.0 lbs 2,8 .4923 psi 1	00.0 lbs .361 psi	4,350.0 lbs 4.649 psi
Footing Shear @ Heel Allowable Sliding Stability Ratio Sliding Calcs (Vertical Lateral Sliding Force less 100% Passive Fo less 100% Friction For	= ≡ Comp ≡ (ce= ·	1.126 Ralio < oonent NOT Used) lbs 0.0 lbs 2,060.26 lbs	1.( Moment @ Height Vertical Load @ Height	= 1, = -0	350.0 lbs 2,8 .4923 psi 1	00.0 lbs	7,040.42 ft-# 4,350.0 lbs 4.649 psi 15.977 psi
Footing Shear @ Heel Allowable Sliding Stability Ratio Sliding Calcs (Vertical Lateral Sliding Force less 100% Passive Fo	Comp frce= -	1.126 Ratio < bonent NOT Used) lbs . 0.0 lbs	1.4 Moment @ Height Vertical Load @ Height Actual Unit Tension	= 1, = •0 on =	350.0 lbs 2,8 .4923 psi 1 3.526 psi 9	00.0 lbs .361 psi	4,350.0 lbs 4.649 psi
Footing Shear @ Heel Allowable Sliding Stability Ratio Sliding Catcs (Vertical Lateral Sliding Force less 100% Passive Fo less 100% Friction For Added Force Req'd for 1.5 Stability	Comp = rce= - =	1.126 Ratio < onent NOT Used) ibs . 0.0 ibs - 2,060.26 ibs 0.0 ibs OK	1.! Moment @ Height Vertical Load @ Height Actual Unit Tension Actual Unit Compressio	= 1, = •0 on =	350.0 lbs 2,8 .4923 psi 1 3.526 psi 9	00.0 lbs .361 psi .139 psi	4,350.0 lbs 4.649 psi 15.977 ps 2,437.29 lbs
Footing Shear @ Heel Allowable Sliding Stability Ratio Sliding Calcs (Vertical Lateral Sliding Force less 100% Passive Fo less 100% Friction For Added Force Req'd	Comp = rce= - =	1.126 Ratio < onent NOT Used) ibs . 0.0 ibs - 2,060.26 ibs 0.0 ibs OK	1.! Moment @ Height Vertical Load @ Height Actual Unit Tension Actual Unit Compressio Shear @ Soction	= 1, = .0 on = 7	350.0 lbs         2,8           .4923 psi         1           3.526 psi         9           14.13 lbs         1,52	00.0 ibs 361 psi 139 psi 6.56 ibs	4,350.0 lbs 4.649 psi 15.977 psi 2,437.29 lbs
Footing Shear @ Heel Allowable Sliding Stability Ratio Sliding Calcs (Vertical Lateral Sliding Force less 100% Passive Fo less 100% Friction For Added Force Req'd for 1.5 Stability oad Factors	Comp = rce= - =	1.126 Ratio < onent NOT Used) ibs . 0.0 ibs - 2,060.26 ibs 0.0 ibs OK	1.! Moment @ Height Vertical Load @ Height Actual Unit Tension Actual Unit Compressio Shear @ Soction	= 1, = .0 on = 7	350.0 lbs         2,8           .4923 psi         1           3.526 psi         9           14.13 lbs         1,52	00.0 ibs 361 psi 139 psi 6.56 ibs	4,350.0 lbs 4.649 psi 15.977 psi 2,437.29 lbs
Footing Shear @ Heel Allowable Sliding Stability Ratio Sliding Calcs (Vertical Lateral Sliding Force less 100% Passive Fo less 100% Friction For Added Force Req'd for 1.5 Stability coad Factors Building Code	Comp = rce= - =	1.126 Ratio < conent NOT Used) lbs 0.0 lbs 2,060.26 lbs 0.0 lbs OK 684.8 lbs NG	1.! Moment @ Height Vertical Load @ Height Actual Unit Tension Actual Unit Compressio Shear @ Soction	= 1, = .0 on = 7	350.0 lbs         2,8           .4923 psi         1           3.526 psi         9           14.13 lbs         1,52	00.0 ibs 361 psi 139 psi 6.56 ibs	4,350.0 lbs 4.649 psi 15.977 psi
Footing Shear @ Heel Allowable Sliding Stability Ratio Sliding Calcs (Vertical Lateral Sliding Force less 100% Passive Fo less 100% Friction For Added Force Req'd for 1.5 Stability coad Factors Building Code Dead Load Live Load Earth, H	Comp = rce= - =	1.126 Ratio < bonent NOT Used) ibs - 0.0 lbs - 2,060.26 lbs 0.0 lbs OK 684.8 lbs NG 1.200 1.600 1.600	1.! Moment @ Height Vertical Load @ Height Actual Unit Tension Actual Unit Compressio Shear @ Soction	= 1, = .0 on = 7	350.0 lbs         2,8           .4923 psi         1           3.526 psi         9           14.13 lbs         1,52	00.0 ibs 361 psi 139 psi 6.56 ibs	4,350.0 lbs 4.649 psi 15.977 psi 2,437.29 lbs
Footing Shear @ Heel Allowable Sliding Stability Ratio Sliding Calcs (Vertical Lateral Sliding Force less 100% Passive Fo less 100% Friction For Added Force Req'd for 1.5 Stability oad Factors Building Code Dead Load Live Load	Comp = rce= - =	1.126 Ratio < bonent NOT Used) 1bs - 0.0 lbs - 2,060.26 lbs 0.0 lbs OK 684.8 lbs NG 1.200 1.600	1.! Moment @ Height Vertical Load @ Height Actual Unit Tension Actual Unit Compressio Shear @ Soction	= 1, = .0 on = 7	350.0 lbs         2,8           .4923 psi         1           3.526 psi         9           14.13 lbs         1,52	00.0 ibs 361 psi 139 psi 6.56 ibs	4,350.0 lbs 4.649 psi 15.977 ps 2,437.29 lbs

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Project File: Parc foret walls.ec6

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Seismic, E

1.000

# Gravity Retaining Wall

LIC#: KW-06014449, Build:20.22.1.12 DESCRIPTION: 6 foot wall

Footing Strengths	& Di	nensions
Toe Width	=	ft
Heel Width	= 33	3333333
Total Footing Width	=	5.333
Footing Thickness	=	12.0 in
Key Width	=	24 in
Key Depth	1111	in
Key Dislance from Toe	=	2 ft
	Fy =	60000 psi
Fooling Concrete Densil	y =	150 pcf
Min. As %	=	0.0018
Cover @ Top = 21	n @l	Blm.= 3 in

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		Toe	Heel
Factored Pressure	=	2,807.15	0.0 psf
Mu' : Upward	=	0.0	0.0 ft-#
Mu': Downward	=	0.0	0.0 ft-#
Mu: Design	=	0	0 ft-#
Actual 1-Way Shear	=	*Beyond Toe	0.0 psi
Allow 1-Way Shear	=	43.018	43.818 psi
*Critical section for o	ne-w	ay shear falls beyor	nd the end of the toe.
Toe Reinforcing		None Spec'd	
Heel Reinforcing		None Spec'd	
Key Reinforcing	=	# 7 @ 12.00 in	
Other Acceptable SI	zes	& Spacings	
Toe: phiMn = phi'5'	lamt	da'sqrt(fc)'Sm	
Heel: phiMn = phi'5'	lamb	da'sqrt(fc)'Sm	
Key: No key define	d	and a second	

## Summary of Overturning & Resisting Forces & Moments

		0V	OVERTURNING			
ltem		Force Ibs	Distance ft	Moment ft-#		
Heel Aclive Pressure	=					
Surcharge Over Toe	E	0.0	0.0	0.0		
Adjacent Fooling Load	=	0.0	0.0	0.0		
Added Lateral Load	=	0.0	0.0	0.0		
Load @ Stem Above Soil	=	0.0	0.0	0.0		
Seismic Load	Ħ	908.61	4.20	3,816.16		
Seismic Stem Self Wt	=		0.0			
Total	Ħ	1,830.07	0.T.M.	5,966.24		
Resisting/Overturnin	g R	atlo	=	= 2.478		
Vertical Loads use	d fo	r Soil Press	ure =	5,150.65 lbs		

		RE		
		Force Ibs	Distance It	Moment ft-#
Soil Over Heel	=	0.0	5.333	0.0
Sloped Soil Over Hee	=	.0000130	5.333	.0000670
Surcharge Over Heel	=	0.0	0,0	0.0
Adjacent Footing Load	=	0.0	0.0	0.0
Axial Dead Load on Ste	m=	0.0	0.0	0.0
Soil Over Toe Surcharge Over Toe	=	0.0	0.0	0.0
Stem Weight	=	0.0	0.0	0,0
•	=	4,350.38	2.908	12,652.0
Earth above Sloping Ste	err <u>=</u>	0.270	5.333	1.440
Footing Weight	=	800.0	2.667	2,133.33
Key Weight	=	0.0	3.0	0.0
Vert. Component	=	0.0	0,0	0.0
To	tal =	5,150.65 I	bs R.M.≍	14,786.8

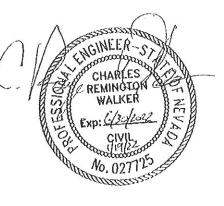
Vertical component of active pressure NOT used for soil pressure

### Tilt

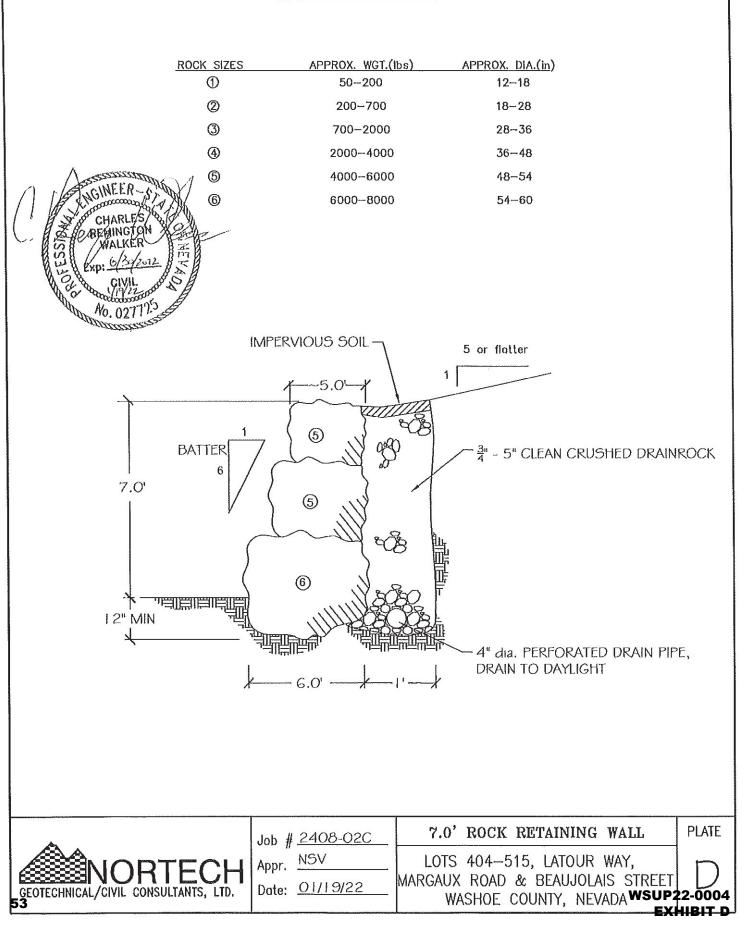
#### Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

Soil Spring Reaction Modulus	p&50
Horizontal Defl @ Top of Wall (approximate only)	0.06266
The above calculation is not valid if the heel soil beari	ng pressure exceeds that of the toe,
because the wall would then tend to rotate into the rel	ained soil.



# RETAINING WALL DETAIL



# Gravity Retaining Wall LIC# : KW-06014449, Build:20.22.1.12

DESCRIPTION: 7 foot wall

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Criteria	Soil Data	[ · · · · · · · · · · · · · · · · · · ·
Retained Height = 7.0 (t	Allow Soil Bearing = 3,000.0 psf	1 CONSTRUCTION
Wall height above soil = ft Slope Behind Wal = 3	Coulomb Soil Presure calculation	· · · · · · · · · · · · · · · · · · ·
	Soil Friction Angle _ 32.0 deg	
Height of Soil over Toe = in Soll Density = 108.0 pcf	Active Pressure:Ka*Gamma⇒ 0.0 psf/(t Passive Pressure:Kp*Gamma 0.0 psf/(t	
Soll Density = 108.0 pcf	rassive riessule, the Gamina 0.0 psint	
	Footing  Soil Friction = 0.40	
	Soil height to ignore	
	for passive pressure = 12 in	
		L
		Thumbnail
Surcharge Loads	Lateral Load Applied to Stem	Adjacent Footing Load
Surcharge Over Heel = psf	Lateral Load = #//(t	Adjacent Footing Load = Ibs
>>>Used To Resist Sliding & Overturning Surcharge Over Toe = psf	Height to Top: = ft	Footing Width = ft
Surcharge Over Toe = psf Used for Sliding & Overturning	Height to Botton = It	Eccentricity = in Wall to Ftg CL Dist = ft
		Footing Type Line Load
		Base Above/Below Soil
	Wind on Exposed Stem = psf	al Back of Wall
		Poisson's Ratio = 0.3
Earth Pressure Seismic Load	Kae for seismic earth pressure = 0.6916	Added seismic base force 1,302.79 lbs
Design Kh = 0.2 g	Ka for static earth pressure = 0.3147	< Note1 These are horizontal components
Using Mononobe-Okabe / Seed-Whitman pro	Difference: Kae - Ka = 0.3770	
Design Summary	Rubble masonry, mortar bonded St	em Analysis Data (Unrolnforced material)
Total Bearing Load = 6,788.25 lbs	Wall Material Weight = 150.0 pcf	
resultant ecc. = 13.260 in		c : Max. Allow. Compression = 100 psi
Resultant Exceeds Ftg. Width1 Soil Pressure @ Toe = 2,287,48 psf N	F	c : Max. Allow. Tension = 10 psi
Soil Pressure @ Heel = 0.0 psf N		
Allowable = psf	Thickness @ Top of Stem = 60.0 in Back Batter Distance = in	
Soil Pressure Less Than Allowable ACI Factored @ Toe = 3,202.48 psf	@ Height	#1 @ Height #2 @ Height #3
	(U) reight	
ACI Factored @ Hee1 = 0.0 psf		
Footing Shear @ Toe = 0.0 psi C	K Height above Footing =	4 ft 2 ft 0.0 ft
Footing Shear @ Toe = 0.0 psi C Footing Shear @ Heel = 0.0 psi C	noight above rooting	
Footing Shear @ Toe = 0.0 psi C Footing Shear @ Heel = 0.0 psi C Allowable = 82.158 psi	K Wall Thick. @ Height = 66. Section Modulus = 8,712.	4 ft 2 ft 0.0 ft 0 ín 70.0 in 74.0 in
Footing Shear @ Toe       =       0.0 psi C         Footing Shear @ Heel       =       0.0 psi C         Allowable       =       82,158 psi         Sliding Stability Ratio       =       1.136 Ratio	VK     Wall Thick. @ Height     =     66.       < Section Modulus	4 ft 2 ft 0.0 ft 0 in 70.0 in 74.0 in 0 in^3 9,800.0 in^3 10,952.0 in^3 3 ft-# 5,923.06 ft-# 11,348.3 ft-#
Footing Shear @ Toe = 0.0 psi C Footing Shear @ Heel = 0.0 psi C Allowable = 82.158 psi Sliding Stability Ratio = 1.136 Ratio Sliding Calcs (Vertical Component NOT Used Lateral Sliding Force = lbs	VK Wall Thick. @ Height = 66. Section Modulus = 8,712.	4 ft 2 ft 0.0 ft 0 in 70.0 in 74.0 in 0 in^3 9,800.0 in^3 10,952.0 in^3 3 ft-# 5,923.06 ft-# 11,348.3 ft-#
Footing Shear @ Toe       =       0.0 psi       C         Footing Shear @ Heel       =       0.0 psi       C         Allowable       =       82,158 psi       S         Sliding Stability Ratio       =       1.136 Ratio         Sliding Calcs       (Vertical Component NOT Used Lateral Sliding Force       =       Ibs         less 100% Passive Force       -       0.0 lbs	VK       Wall Thick. @ Height       =       66.         < 1.t	4 ft         2 ft         0.0 ft           0 in         70.0 in         74.0 in           0 in^3         9,800.0 in^3         10,952.0 in^3           3 ft-#         5,923.06 ft-#         11,348.3 ft-#           0 lbs         4,062.50 lbs         5,862.50 lbs           1 psi         2.416 psi         5.832 psi
Footing Shear @ Toe = 0.0 psi C Footing Shear @ Heel = 0.0 psi C Allowable = 82.158 psi Sliding Stability Ratio = 1.136 Ratio Sliding Calcs (Vertical Component NOT Used Lateral Sliding Force = lbs	Wall Thick. @ Height = 66. K Wall Thick. @ Height = 0,712. Actual Load @ Height = 2,180.2 Vertical Load @ Height = 2,362.5 Actual Unit Tension = 0.0201 Actual Unit Compression = 5.98	4 ft         2 ft         0.0 ft           0 in         70.0 in         74.0 in           0 in^3         9,800.0 in^3         10,952.0 in^3           3 ft-#         5,923.06 ft-#         11,348.3 ft-#           0 lbs         4,062.50 lbs         5,862.50 lbs
Footing Shear @ Toe = 0.0 psi C Footing Shear @ Heel = 0.0 psi C Allowable = 82.158 psi Sliding Stability Ratio = 1.136 Ratio Sliding Calcs (Vertical Component NOT Used Lateral Sliding Force = lbs less 100% Passive Force = 0.0 lbs less 100% Friction Force = - 2,715.30 lbs	YK       Wall Thick. @ Height       =       66.         < 1.1	4 ft         2 ft         0.0 ft           0 in         70.0 in         74.0 in           0 in^3         9,800.0 in^3         10,952.0 in^3           3 ft-#         5,923.06 ft-#         11,348.3 ft-#           0 lbs         4,062.50 lbs         5,862.50 lbs           1 psi         2.416 psi         5.832 psi           6 psi         12.089 psi         19.036 psi           9 lbs         2,276.61 lbs         3,294.29 lbs
Footing Shear @ Toe =       0.0 psi C         Footing Shear @ Heel =       0.0 psi C         Allowable =       82.158 psi         Sliding Stability Ratio =       1.136 Ratio         Sliding Calcs (Vertical Component NOT Used Lateral Sliding Force =       0.0 lbs         less 100% Passive Force -       0.0 lbs         less 100% Friction Force =       2,715.30 lbs         Added Force Req'd =       0.0 lbs	YK       Wall Thick. @ Height       =       66.         < 1.1	4 ft         2 ft         0.0 ft           0 in         70.0 in         74.0 in           0 in^3         9,800.0 in^3         10,952.0 in^3           3 ft-#         5,923.06 ft-#         11,348.3 ft-#           0 lbs         4,062.50 lbs         5,862.50 lbs           1 psi         2.416 psi         5.832 psi           6 psi         12.089 psi         19.036 psi
Footing Shear @ Toe =       0.0 psi C         Footing Shear @ Heel =       0.0 psi C         Allowable =       82,158 psi         Sliding Stability Ratio =       1.136 Ratio         Sliding Calcs (Vertical Component NOT Used       1.136 Ratio         Lateral Sliding Force =       lbs         less 100% Passive Force -       0.0 lbs         less 100% Friction Force =       2,715.30 lbs         Added Force Req'd =       0.0 lbs C        for 1.5 Stability =       870.1 lbs N         Load Factors       Building Code	YK       Wall Thick. @ Height       =       66.         < 1.1	4 ft         2 ft         0.0 ft           0 in         70.0 in         74.0 in           0 in^3         9,800.0 in^3         10,952.0 in^3           3 ft-#         5,923.06 ft-#         11,348.3 ft-#           0 lbs         4,062.50 lbs         5,862.50 lbs           1 psi         2.416 psi         5.832 psi           6 psi         12.089 psi         19.036 psi           9 lbs         2,276.61 lbs         3,294.29 lbs
Footing Shear @ Toe =       0.0 psi C         Footing Shear @ Heel =       0.0 psi C         Allowable =       82.158 psi         Sliding Stability Ratio =       1.136 Ratio         Sliding Calcs (Vertical Component NOT Used       Lateral Sliding Force =         Lateral Sliding Force =       lbs         less 100% Passive Force =       0.0 lbs         less 100% Friction Force =       2,715.30 lbs         Added Force Req'd =       0.0 lbs C        for 1.5 Stability =       870.1 lbs N         Load Factors	YK       Wall Thick. @ Height       =       66.         < 1.1	4 ft         2 ft         0.0 ft           0 in         70.0 in         74.0 in           0 in^3         9,800.0 in^3         10,952.0 in^3           3 ft-#         5,923.06 ft-#         11,348.3 ft-#           0 lbs         4,062.50 lbs         5,862.50 lbs           1 psi         2.416 psi         5.832 psi           6 psi         12.089 psi         19.036 psi           9 lbs         2,276.61 lbs         3,294.29 lbs
Footing Shear @ Toe =       0.0 psi C         Footing Shear @ Heel =       0.0 psi C         Allowable =       82,158 psi         Sliding Stability Ratio =       1,136 Ratio         Sliding Calcs (Vertical Component NOT Used       1.136 Ratio         Lateral Sliding Force =       lbs         less 100% Passive Force -       0.0 lbs         less 100% Friction Force =       2,715.30 lbs         Added Force Req'd =       0.0 lbs C        for 1.5 Stability =       870.1 lbs N         Load Factors       Building Code	YK       Wall Thick. @ Height       =       66.         < 1.1	4 ft         2 ft         0.0 ft           0 in         70.0 in         74.0 in           0 in^3         9,800.0 in^3         10,952.0 in^3           3 ft-#         5,923.06 ft-#         11,348.3 ft-#           0 lbs         4,062.50 lbs         5,862.50 lbs           1 psi         2.416 psi         5.832 psi           6 psi         12.089 psi         19.036 psi           9 lbs         2,276.61 lbs         3,294.29 lbs
Footing Shear @ Toe =       0.0 psi C         Footing Shear @ Heel =       0.0 psi C         Allowable =       82,158 psi         Sliding Stability Ratio =       1.136 Ratio         Sliding Calcs (Vertical Component NOT Used       1.136 Ratio         Sliding Calcs (Vertical Component NOT Used       1.136 Ratio         Lateral Sliding Force =       lbs         less 100% Passive Force -       0.0 lbs         less 100% Friction Force =       2,715.30 lbs         Added Force Req'd =       0.0 lbs        for 1.5 Stability =       870.1 lbs         Load Factors	YK       Wall Thick. @ Height       =       66.         < 1.1	4 ft         2 ft         0.0 ft           0 in         70.0 in         74.0 in           0 in^3         9,800.0 in^3         10,952.0 in^3           3 ft-#         5,923.06 ft-#         11,348.3 ft-#           0 lbs         4,062.50 lbs         5,862.50 lbs           1 psi         2.416 psi         5.832 psi           6 psi         12.089 psi         19.036 psi           9 lbs         2,276.61 lbs         3,294.29 lbs

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# Gravity Retaining Wall LIC# : KW-06014449, Buikd:20.22.1.12

**DESCRIPTION:** 7 foot wall

Footing Strengths & Dimensions						
Toe Width	Ξ	ft				
Heel Width	= ĵ	66666666				
Total Ecoling Midth	-	6 467				

Total Fooling Widtr	=	6.167
Footing Thickness	=	12.0 in
Key Width	=	24 in
Key Depth	=	in
Key Distance from Toe	13	2 ft
Footing Concrete Densit	-	60000 psi 150 pcf
Min. As %	Ħ	0.0018
Cover@Top = 2i	n @ Btr	m.≕ 3 in

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Footing Design	Res	sults	
		Toe	Heel
Factored Pressure		3,202.48	0.0 psf
Mu' : Upward	=	0.0	0.0 ft-#
Mu': Downward	÷	0.0	0.0 ft-#
Mu: Design	12	0	0 11-#
Actual 1-Way Shear	=	*Beyond Toe	0.0 psi
Allow 1-Way Shear	=	43.818	43.818 psi
*Critical section for o			nd the end of the toe.
Toe Reinforcing Heel Reinforcing Key Reinforcing	=	None Spec'd None Spec'd # 7 @ 12.00 in	
Othor Acceptable SI Toe: phiMn = phi'5' Heel: phiMn = phi'5'	lamb	da'sqrt(fc)'Sm	
Key: No key define			

### Summary of Overturning & Resisting Forces & Moments

	OVERTURNING			
Item		Force lbs	Distance	
Rem	3	105	ft	ft-#
Heel Active Pressure	Ħ			
Surcharge Over Toe	-	0.0	0.0	0.0
Adjacent Footing Load	=	0.0	0.0	0.0
Added Lateral Load	=	0.0	0.0	0.0
Load @ Stem Above Soil	=	0.0	0.0	0.0
Seismic Load	=	1,302.79	4.80	6,253.37
Seismic Stem Self Wt	÷		0.0	
Total	=	2,390.30	0.T.M.	9,153.40
				=
Resisting/Overturnin	g R	atio	=	2.467
Vertical Loads used for Soil Pressure				6,788.25 lbs

Vertical component of active pressure NOT used for soil pressure

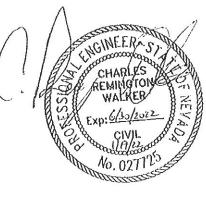
		RESISTING		
_		Force Ibs	Distance ft	Moment ft-#
Soll Over Heel Sloped Soil Over Heel Surcharge Over Heel Adjacent Footing Load	Ξ	0.0	6,167	0.0
	n	.0000130	6.166	.0000770
	=	0.0	0.0	0,0
	=	0.0	0.0	0.0
Axial Dead Load on Stem =		0.0	0.0	0.0
Soil Over Toe Surcharge Over Toe Stem Welght Earth above Stoping Ste Footing Weight Key Welght	=	0.0	0.0	0.0
	=	0.0	0.0	0.0
		5,862.94	3.365	19,729.1
	9m ==	0.3150	6.167	1.943
	=	925,0	3.083	2,852.08
	Ħ	0.0	3.0	0.0
Vert. Component	₽	0.0	0.0	0.0
Tol	tal =	6,788.25	os R.M.≂	22,503.1

Tilt

#### Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

Soil Spring Reaction Modulus	pØ50		
Horizontal Defl @ Top of Wall (approximate only)	0.07213	/	
The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe,			
because the wall would then tend to rotate into the retain	ained soil.		



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