Community Services Department Planning and Development SPECIAL USE PERMIT FOR GRADING APPLICATION



Community Services Department Planning and Development 1001 E Ninth St., Bldg A. Reno, NV 89520

Telephone: 775.328.3600

Washoe County Development Application

Your entire application is a public record. If you have a concern about releasing personal information, please contact Planning and Development staff at 775.328.3600.

Project Information	s	Staff Assigned Case No.:						
Project Name:								
Project Description:								
Project Address:								
Project Area (acres or square fee	et):							
Project Location (with point of re	ference to major cross	streets AND area locator):						
Assessor's Parcel No.(s):	Parcel Acreage:	Assessor's Parcel No(s):	Parcel Acreage:					
Section(s)/Township/Range:								
Indicate any previous Washo Case No.(s).	e County approval	s associated with this applicat	ion:					
Applicant	Information (atta	ch additional sheets if necessary	/)					
Property Owner:		Professional Consultant:						
Name:		Name:						
Address:		Address:						
	Zip:	Zip:						
Phone:	Fax:	Phone:	Fax:					
Email:		Email:						
Cell:	Other:	Cell:	Other:					
Contact Person:		Contact Person:						
Applicant/Developer:		Other Persons to be Contacted:						
Name:		Name:						
Address:		Address:						
	Zip:		Zip:					
Phone:	Fax:	Phone:	Fax:					
Email:		Email:						
Cell:	Other:	Cell:	Other:					
Contact Person:		Contact Person:						
	For Office	Use Only						
Date Received:	Initial:	Planning Area:						
County Commission District:		Master Plan Designation(s):						
CAB(s):		Regulatory Zoning(s):						

Special Use Permit Application for Grading Supplemental Information

(All required information may be separately attached)

Chapter 110 of the Washoe County Code is commonly known as the Development Code. Specific references to special use permits may be found in Article 810, Special Use Permits. Article 438, Grading, and Article 418, Significant Hydrologic Resources, are the ordinances specifically involved in this request.

1.	What is the purpose of the grading?
2.	How many cubic yards of material are you proposing to excavate on site?
3.	How many square feet of surface of the property are you disturbing?
4.	How many cubic yards of material are you exporting or importing? If none, how are you managing to balance the work on-site?

5.	Is it possible to develop your property without surpassing the grading thresholds requiring a Special Use Permit? (Explain fully your answer.)
6.	Has any portion of the grading shown on the plan been done previously? (If yes, explain the circumstances and the year the work was done.)
7.	Have you shown all areas on your site plan that are proposed to be disturbed by grading? (If no explain fully your answer.)

	Can the disturoadways?	urbed area b	e seen from off-site?	If yes, fron	n which direc	ctions, and w	hich properties o
9.	Could neight	ooring prope a driveway, v	rties also be served vould it be used for a	by the prop	osed access litional neight	/grading requoting proper	uested (i.e. if youtles)?
10.			ntal:Vertical) of the c			I to be? Wha	at methods will be
11.	Are you plan	ning any ber	ms?				
	☐ Yes	□ No	If yes, how tall is th	e berm at its	highest?		

13. What are you proposing for visual mitigation of the work? 14. Will the grading proposed require removal of any trees? If so, what species, how many and of w size?	be ete,
14. Will the grading proposed require removal of any trees? If so, what species, how many and of w	
14. Will the grading proposed require removal of any trees? If so, what species, how many and of w	
14. Will the grading proposed require removal of any trees? If so, what species, how many and of w	
14. Will the grading proposed require removal of any trees? If so, what species, how many and of w	
	vhat

15. What intend	type of reve to broadca	egetatior st? Will	n seed mix a you use mu	re you plar lch and, if s	nning to us o, what typ	e and how be?	many pou	nds per ac	re do you
16. How a	re you prov	viding ter	nporary irrig	ation to the	disturbed	area?			
17. Have y	you reviewe corporated	ed the re their sug	vegetation p gestions?	lan with the	e Washoe	Storey Cor	nservation [District? If	yes, have
	ere any re it the reque		covenants, ding?	recorded	conditions,	or deed	restrictions	(CC&Rs)	that may
	res 🗆	No	If yes, plea	se attach a	сору.				

DRAINAGE REPORT

FOR

MUSTANG INDUSTRIAL DEVELOPMENT

Washoe County, Nevada

APN 084-370-02

Prepared for:

Scannell Properties 821 Meander Court, Suite 200 Medina, MN 55340

Prepared by:



10451 Double R Blvd. Reno, Nevada 89521

February 17, 2015 Job Number: 14217

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INTRODUCTION

LOCATION OF PROPERTY

The Mustang Industrial Development is a proposed development located on a vacant parcel of land off the Mustang Road Exist east of Sparks on Interstate 80. The parcel is bound by the UP Railroad to the north and the Truckee River to the south. Please see attached site plan for location. The site is approximately 117.76 acres with an APN of 084-370-02. The project is located in portions of Section 15 & 16, Township 19 North, Range 21 East, Mount Diablo Meridian in Washoe County, Nevada. See Exhibit 1 for a general Vicinity Map.

DESCRIPTION OF PROPERTY

The site is presently undeveloped land with the slope falling from the north side of the site to the river along the south side of the property. The undisturbed area of the site is sparsely populated with small weeds and sagebrush up to 2 feet in height.

PROJECT DESCRIPTION

Scannell Properties is proposing to develop a 117-acre parcel in the Truckee Canyon area of Washoe County, Nevada, near the intersection of Interstate 80 and Mustang Road. The site is bound by the Truckee River to the south and the Union Pacific Railroad to the north. The current zoning, Industrial, allows for the proposed use which includes two light industrial buildings that will be approximately 344,000 square feet and 517,000 square feet. Site development will be supported by infrastructure improvements including the construction of a new road from Mustang Road, a water main extension from the north, on-site sewer collection and treatment, and stormwater ponds to collect runoff. The project is expected to begin late-summer of 2015.

DRAINAGE BASIN DESCRIPTION

DRAINAGE DESCRIPTION

The entire site is being planned for development, as per Exhibit 2 attached, our site has been divided into five separate detention basin areas. All site drainage will be routed to each of these basins, each basin has been designed to meet the Washoe County LID standards for water quality and will treat the runoff before being allowed to be discharged back into the natural drainage way.

FLOODPLAIN INFORMATION

The project site lies in both Flood Zone AE and X. This information is based on the FEMA Flood Insurance Rate Map No. 32031C3069G and 32031C3088G, dated March 16, 2009 for Washoe County, Nevada. Flood Zone AE is defined as base floodplain where base flood elevations are provided. Flood Zone X is defined as "Areas determined to be outside the 500 year flood plain". Please see Exhibit 4 for the FEMA Map.

PROPOSED DRAINAGE FACILITIES

COMPLIANCE WITH REGULATIONS AND ADOPTED PLANS

The design criteria which has been used for this drainage report is in compliance with the Washoe County design guidelines, Article 438 Grading Standards.

HYDROLOGIC CRITERIA

The following design criteria assumptions were used for this analysis:

- Design for on-site facilities is based upon the 100 year storm event.
- Rainfall intensity/duration frequencies were obtained from the Washoe County, NV NOAA Atlas 14 Point Precipitation Frequency (Please see Appendix A)
- Runoff coefficients were obtained from Table 7-7 of the Rational Method QTR-55
 Software Program distributed by Hasted Methods.

METHODOLOGY

The rational method was used to determine the peak flows. The parameters for this method are:

- 1. The drainage area (A, acres)
- 2. Time of Concentration (T_c, minutes)
- 3. Runoff Coefficient (C)
- 4. Rainfall Intensity (i, inches per hour)

The time of concentration is calculated based on the equation:

 $T_c=10$ min or L/(Vx60), whichever is greater,

where

L=The travel distance in feet

V=Channel or overland velocity in feet per second

Due to the relatively small size of the site and sub areas and the high runoff potential within commercial developments, the minimum T_c of 10 minutes was used in this analysis.

Rainfall intensity/duration frequencies were obtained from the NOAA Atlas 14 Point Precipitation Frequency IDF Curve. For $T_c=10$ min., the rainfall intensities are $i_{25}=2.39$ in/hr and $i_{100}=3.57$ in/hr.

From the Public Works Design Manual (See Appendix A), the following runoff coefficients were used:

Developed C=0.90 Undeveloped C=0.45

The peak runoff is calculated using the following equation: Q=CiA

FACILITY DESIGN CALCULATIONS

ON-SITE DRAINAGE CALCULATIONS

Our proposed project will have an on-site storm drainage system consisting of four separate detention pond areas. These areas will have multiple sub basins within each basin but for summary purposes they will be lumped together. Table's 1 and 2 show the net increase in flow due to the development and the detention/retention/retention basin required sizing. All calculations can be found in Appendix B, C and D.

<u>Table 1 - Peak Basin Flow Summary</u> 25 & 100-Year Frequency

	Existing 25Yr(cfs)	Developed 25 Yr(cfs)	Net Increase (cfs)	Existing 100Yr(cfs)	Developed 100Yr(cfs)	Net Increase (cfs)
Basin						
Basin 1	10.04	20.20	10.16	14.96	30.18	15.22
Basin 2	7.81	18.01	10.20	11.63	26.89	15.26
Basin 3	46.16	95.35	49.19	68.78	142.42	73.64
Basin 4	14.10	26.47	12.37	21.00	39.53	18.53

<u>Table 2 - Basin Volume Summary</u> 25 & 100-Year Frequency

	100 yr	Volume
	Volume Required (cf)	Provided (cf)
Basin 1	9,674	10,500
Basin 2	9,927	10,500
Basin 3	47,023	47,500
Basin 4	11,633	12,000

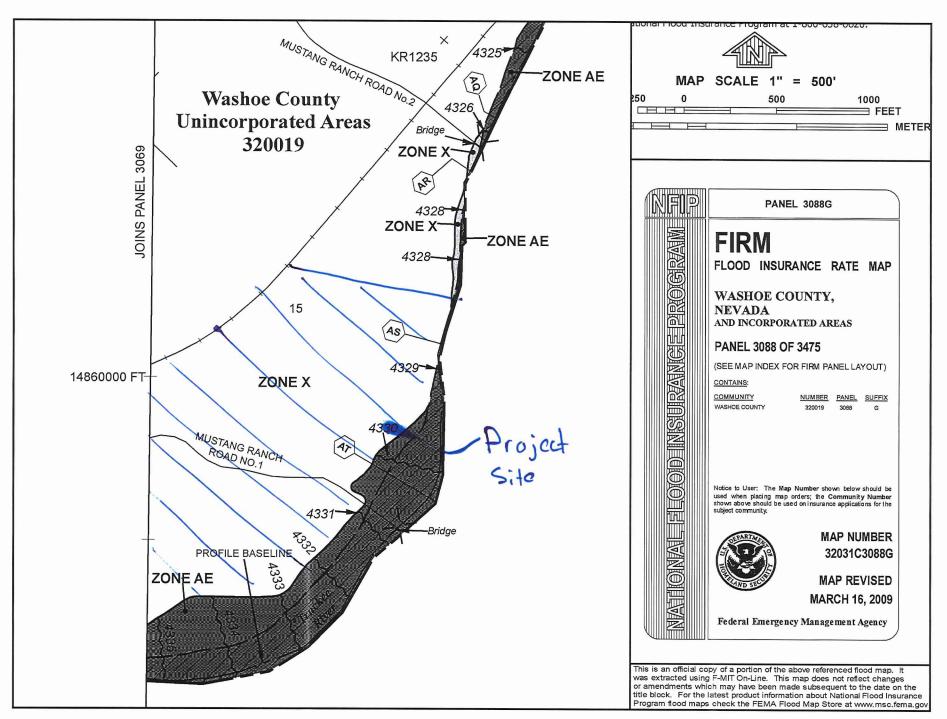
CONCLUSION

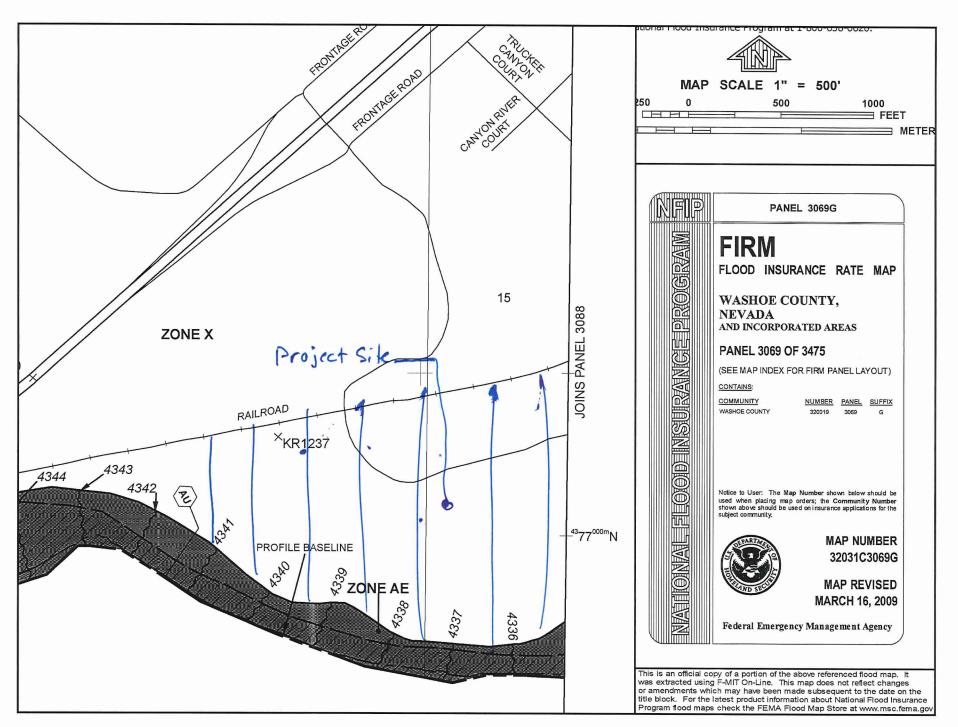
All designed storm drain and flood control facilities are effective in controlling storm runoff and have no impact on existing off-site facilities. Therefore, no mitigation of impacts is required. In addition, the storm drain and flood control facilities are in compliance with the following:

- FEMA requirements No buildings are proposed within the existing or proposed 100-year flood plain boundaries.
- Drainage Laws As designed, the drainage system shall promote and preserve the general health, welfare, and economic being of the region.

- The designed facilities are consistent with and integrated with the Washoe County Drainage Master Plan.
- All storm drain and flood control improvements have been designed to meet or exceed the design standards as set forth in the overall Washoe County Master Drainage Plan and in compliance with the Washoe County design guidelines, Article 438 Grading Standards.

EXHIBITS





APPENDIX A

REGIONAL DRAINAGE CRITERIA



NOAA Atlas 14, Volume 1, Version 5 Location name: Sparks, Nevada, US* Latitude: 39.5090°, Longitude: -119.6215° Elevation: 4462 ft* * source: Google Maps



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour) ¹											
Duration				Avera	age recurren	ce interval (years)				
Duration	1 2 5 10 25		50	50 100		500	1000				
5-min	1.15 (0.960–1.33)	1.43 (1.21–1.69)	1.92 (1.62–2.28)	2.38 (1.99-2.84)	3.14 (2.57-3.79)	3.85 (3.05-4.69)	4.69 (3.60-5.80)	5.71 (4.21–7.19)	7.37 (5.10-9.55)	8.88 (5.87-11.8)	
10-min	0.870 (0.732-1.01)	1.09 (0.918–1.28)	1.46 (1.24–1.73)	1.81 (1.52-2.17)	2.39 (1.96–2.89)	2.93 (2.32-3.57)	3.57 (2.74-4.40)	4.35 (3.20-5.47)	5.60 (3.89-7.27)	6.76 (4.46–8.95)	
15-min	0.720 (0.604-0.840)	0.900 (0.760-1.06)	1.21 (1.02–1.44)	1.50 (1.26–1.79)	1.98 (1.62-2.38)	2.42 (1.92–2.95)	2.95 (2.26-3.64)	3.59 (2.65-4.52)	4.63 (3.21-6.01)	5.58 (3.69-7.40)	
30-min	0.486 (0.408-0.566)	0.604 (0.512-0.714)	0.812 (0.686-0.966)	1.01 (0.846-1.20)	1.33 (1.09-1.60)	1.63 (1.29-1.99)	1.99 (1.52-2.45)	2.42 (1.78-3.04)	3.12 (2.16-4.05)	3.76 (2.48-4.98)	
60-min	0.301 (0.252-0.350)	0.374 (0.316-0.442)	0.503 (0.425-0.598)	0.623 (0.523-0.744)	0.824 (0.674-0.993)	1.01 (0.800-1.23)	1.23 (0.944-1.52)	1.50 (1.10-1.88)	1.93 (1.34-2.50)	2.33 (1.54-3.08)	
2-hr	0.198 (0.173-0.230)	0.246 (0.216-0.288)	0.318 (0.276-0.372)	0.380 (0.325-0.443)	0.474 (0.394-0.557)	0.558 (0.453-0.664)	0.656 (0.518-0.790)	0.777 (0.595-0.950)	0.993 (0.727-1.26)	1.19 (0.844-1.55)	
3-hr	0.157 (0.139-0.180)	0.196 (0.175-0.226)	0.248 (0.218-0.285)	0.289 (0.252-0.333)	0.348 (0.298-0.403)	0.399 (0.336-0.468)	0.461 (0.380-0.546)	0.541 (0.436-0.651)	0.680 (0.532-0.847)	0.809 (0.617-1.04)	
6-hr	0.110 (0.097–0.125)	0.138 (0.122-0.157)	0.172 (0.151–0.196)	0.198 (0.174-0.226)	0.233 (0.202-0.268)	0.260 (0.221-0.301)	0.287 (0.241-0.336)	0.321 (0.264-0.380)	0.376 (0.303-0.453)	0.433 (0.342-0.530)	
12-hr	0.072 (0.064-0.081)	0.090 (0.080-0.102)	0.115 (0.101-0.130)	0.134 (0.117-0.151)	0.159 (0.137-0.182)	0.178 (0.152-0.205)	0.198 (0.167-0.231)	0.218 (0.180-0.257)	0.244 (0.196-0.294)	0.267 (0.210-0.327)	
24-hr	0.045 (0.040-0.050)	0.056 (0.051-0.063)	0.072 (0.065-0.080)	0.084 (0.075-0.094)	0.101 (0.090-0.114)	0.115 (0.102-0.129)	0.130 (0.113-0.146)	0.144 (0.125-0.164)	0.165 (0.141-0.189)	0.182 (0.152-0.210)	
2-day	0.027 (0.024-0.030)	0.034 (0.030-0.038)	0.043 (0.038-0.049)	0.051 (0.045-0.057)	0.062 (0.054-0.070)	0.070 (0.061-0.080)	0.079 (0.068-0.091)	0.089 (0.076-0.103)	0.102 (0.085-0.120)	0.113 (0.093-0.134)	
3-day	0.019 (0.017-0.022)	0.025 (0.022-0.028)	0.032 (0.028-0.036)	0.038 (0.033-0.043)	0.046 (0.040-0.052)	0.053 (0.046-0.060)	0.060 (0.052-0.069)	0.068 (0.058-0.078)	0.079 (0.065-0.092)	0.087 (0.071-0.103)	
4-day	0.016 (0.014-0.018)	0.020 (0.018-0.023)	0.026 (0.023-0.030)	0.031 (0.028-0.035)	0.038 (0.034-0.044)	0.044 (0.038-0.050)	0.051 (0.043-0.058)	0.057 (0.049-0.066)	0.067 (0.055-0.077)	0.074 (0.061-0.087)	
7-day	0.011 (0.009-0.012)	0.014 (0.012-0.015)	0.018 (0.016-0.020)	0.021 (0.019-0.024)	0.026 (0.023-0.030)	0.030 (0.026-0.035)	0.034 (0.029-0.040)	0.039 (0.033-0.045)	0.045 (0.037-0.053)	0.050 (0.041-0.059)	
10-day	0.008 (0.007-0.010)	0.011 (0.009-0.012)	0.014 (0.012-0.016)	0.017 (0.015-0.019)	0.020 (0.018-0.023)	0.023 (0.020-0.027)	0.027 (0.023-0.031)	0.030 (0.025-0.035)	0.034 (0.029-0.040)	0.038 (0.031-0.045)	
20-day	0.005 (0.005-0.006)	0.007 (0.006-0.007)	0.009 (0.008-0.010)	0.010 (0.009-0.012)	0.012 (0.011-0.014)	0.014 (0.012-0.016)	0.016 (0.013-0.018)	0.017 (0.015-0.020)	0.020 (0.017-0.023)	0.022 (0.018-0.025)	
30-day	0.004 (0.003-0.004)	0.005 (0.004-0.006)	0.007 (0.006-0.008)	0.008 (0.007-0.009)	0.009 (0.008-0.011)	0.011 (0.009-0.012)	0.012 (0.010-0.014)	0.013 (0.011-0.015)	0.015 (0.013-0.017)	0.016 (0.014-0.019)	
45-day	0.003 (0.003-0.004)	0.004 (0.004-0.005)	0.005 (0.005-0.006)	0.006 (0.005-0.007)	0.007 (0.006-0.008)	0.008 (0.007-0.009)	0.009 (0.008-0.011)	0.010 (0.009-0.012)	0.011 (0.010-0.013)	0.012 (0.010-0.014)	
60-day	0.003 (0.002-0.003)	0.003 (0.003-0.004)	0.005 (0.004-0.005)	0.005 (0.005-0.006)	0.006 (0.005-0.007)	0.007 (0.006-0.008)	0.008 (0.007-0.009)	0.008 (0.007-0.010)	0.009 (0.008-0.011)	0.010 (0.008-0.011)	

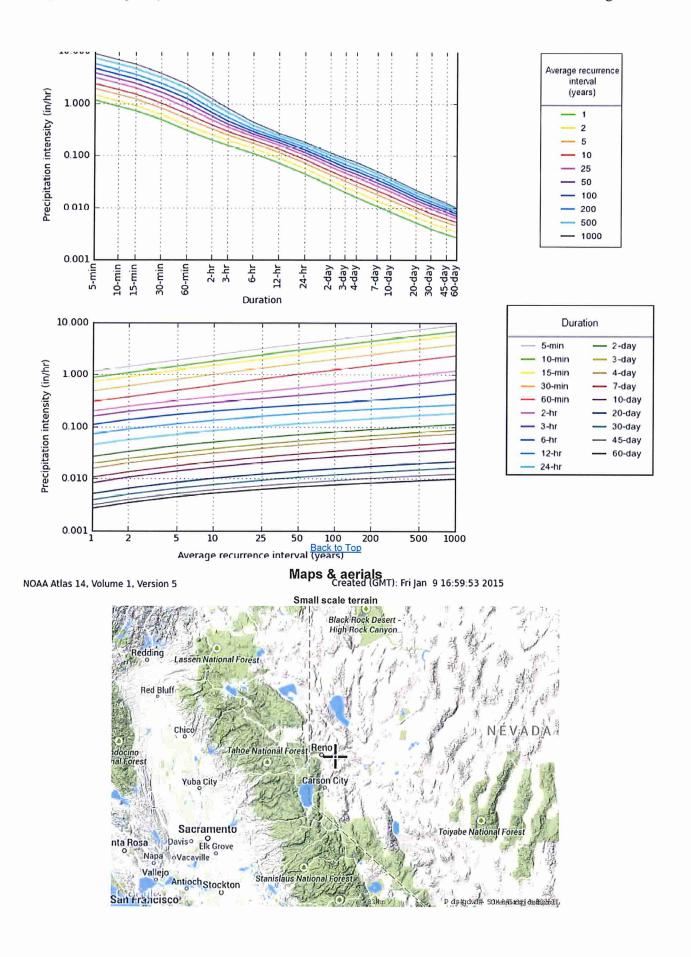
Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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PF graphical



APPENDIX B

EXISTING BASIN CALCULATIONS

Quick TR-55 Ver.5.46 S/N: Executed: 13:14:24 02-16-2015

MUSTANG INDUSTRIAL DEVELOPMENT EXISTING SITE OVERALL SUB BASIN 1

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * * *

Q = adj * C * I * A
Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres
adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 10 years `C' adjustment, k = 1 Adj. 'C' = Wtd.'C' \times 1

				===	=====		=======	======
Subarea Descr.	Runoff 'C'	Area Tc acres (min)	Wtd. 'C'		_	I in/hr	Total acres	Peak Q (cfs)
EXISTING	0.450	11.27		- -				
		15.00	0.450	- - 	0.450	1.500	11.27	7.61

Quick TR-55 Ver.5.46 S/N: Executed: 13:14:24 02-16-2015

MUSTANG INDUSTRIAL DEVELOPMENT EXISTING SITE OVERALL SUB BASIN 1

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

 $\label{eq:Q} Q = \text{adj * C * I * A} \\ \text{Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres}$ adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 25 years
'C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

					===	=====	=======		=======
Subarea	Runoff	Area	Tc	Wtd.	11	Adj.	I	Total	Peak Q
Descr.	'C'	acres	(min)	'C'	\Box	'C'	in/hr	acres	(cfs)
					-11-				
EXISTING	0.450	11.27			11				
					-11-				
		1	15.00	0.450	Ħ	0.450	1.980	11.27	10.04

Quick TR-55 Ver.5.46 S/N: Executed: 13:14:24 02-16-2015

MUSTANG INDUSTRIAL DEVELOPMENT EXISTING SITE OVERALL SUB BASIN 1

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

 $\label{eq:Q} Q = \text{adj * C * I * A} \\$ Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 100 years
`C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

					===				
Subarea	Runoff	Area	Tc				I	Total	Peak Q
Descr.	'C'	acres	(min)	'C'	11	'C'	in/hr	acres	(cfs)
					- -				
EXISTING	0.450	11.27	1		11			1	
					-11-				
			15.00	0.450	İİ	0.450	2.950	11.27	14.96

Quick TR-55 Ver.5.46 S/N: Executed: 13:14:55 02-16-2015

MUSTANG INDUSTRIAL DEVELOPMENT EXISTING SITE OVERALL SUB BASIN 2

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

 $\label{eq:Q} Q = \text{adj * C * I * A} \\ \text{Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres}$ adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 10 years
'C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

					2002 2002 2002	=====	======	=======	=======
Subarea Descr.	Runoff 'C'	Area acres	Tc (min)	Wtd. 'C'			I in/hr		Peak Q (cfs)
EXISTING	0.450	8.76			- -				
			15.00	0.450	- - 	0.450	1.500	8.76	5.91

Quick TR-55 Ver.5.46 S/N: Executed: 13:14:55 02-16-2015

MUSTANG INDUSTRIAL DEVELOPMENT EXISTING SITE OVERALL SUB BASIN 2

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

 $\label{eq:Q} Q = adj \ ^* \ C \ ^* \ I \ ^* A$ Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 25 years `C' adjustment, k = 1 Adj. 'C' = Wtd.'C' \times 1

					===			======	
Subarea	Runoff	Area	Tc	Wtd.	11	Adj.	I	Total	Peak Q
Descr.	'C'	acres	(min)	'C'	11	'C'	in/hr	acres	(cfs)
					-11-				
EXISTING	0.450	8.76 j			ii				i İ
					- -				
		i	15.00	0.450	11	0.450	1.980	8.76	7.81

Quick TR-55 Ver.5.46 S/N: Executed: 13:14:55 02-16-2015

MUSTANG INDUSTRIAL DEVELOPMENT EXISTING SITE OVERALL SUB BASIN 2

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

Q = adj * C * I * A
Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres
adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 100 years 'C' adjustment, k = 1 Adj. 'C' = Wtd.'C' x 1

				===	=====		=======	======
Subarea	Runoff	Area Tc			_		Total	. ~
Descr.	'C'	acres (mi	n) 'C'	 - -		in/hr	acres	(CIS)
EXISTING	0.450	8.76		ii				
				-11-		. 		
		15.	00 0.450	11	0.450	2.950	8.76	11.63

Quick TR-55 Ver.5.46 S/N: Executed: 13:15:31 02-16-2015

MUSTANG INDUSTRIAL DEVELOPMENT EXISTING SITE OVERALL SUB BASIN 3

Q = adj * C * I * A
Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres
adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 10 years
`C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

					====		=======	=======	=======
Subarea	Runoff	Area	Tc				I	Total	Peak Q
Descr.	'C'	acres	(min)	, C ,	П	'C'	in/hr	acres	(cfs)
					- -				-
EXISTING	0.450	51.81			\Box				1
					- -				
		i	15.00	0.450	11	0.450	1.500	51.81	34.97

Quick TR-55 Ver.5.46 S/N: Executed: 13:15:31 02-16-2015

MUSTANG INDUSTRIAL DEVELOPMENT EXISTING SITE OVERALL SUB BASIN 3

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

Q = adj * C * I * A

Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 25 years

`C' adjustment, k = 1 Adj. 'C' = Wtd.'C' x 1

 Quick TR-55 Ver.5.46 S/N: Executed: 13:15:31 02-16-2015

MUSTANG INDUSTRIAL DEVELOPMENT EXISTING SITE OVERALL SUB BASIN 3

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * * *

 $\label{eq:Q} Q = \text{adj * C * I * A} \\ \text{Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres}$ adj = 'C' adjustment factor for each return frequency

> RETURN FREQUENCY = 100 years
> `C' adjustment, k = 1 Adj. 'C' = Wtd.'C' x 1

					===	======	======	======	
Subarea Descr.	Runoff 'C'	Area acres	Tc (min)			_		Total acres	Peak Q (cfs)
EXISTING	0.450	51.81			- - 				
			15.00	0.450	- - 	0.450	2.950	51.81	68.78

Quick TR-55 Ver.5.46 S/N: Executed: 13:15:56 02-16-2015

MUSTANG INDUSTRIAL DEVELOPMENT EXISTING SITE OVERALL SUB BASIN 4

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

 $\label{eq:Q} Q = adj \ * \ C \ * \ I \ * \ A$ Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency

> RETURN FREQUENCY = 10 years C' adjustment, k = 1Adj. 'C' = Wtd.'C' x 1

					===	======	=======	=======	=======
Subarea Descr.	Runoff 'C'	Area acres	Tc (min)	Wtd. 'C'			I in/hr		Peak Q (cfs)
EXISTING	0.450	15.82	 		- - 				
			15.00	0.450	- - 	0.450	1.500	15.82	10.68

Quick TR-55 Ver.5.46 S/N: Executed: 13:15:56 02-16-2015

MUSTANG INDUSTRIAL DEVELOPMENT EXISTING SITE OVERALL SUB BASIN 4

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

 $\label{eq:Q} Q = \text{adj * C * I * A} \\ \text{Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres}$ adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 25 years `C' adjustment, k = 1 Adj. 'C' = Wtd.'C' \times 1

				===			======	======
Subarea Descr.	Runoff 'C'	Area To			_	I in/hr	Total acres	Peak Q (cfs)
EXISTING	0.450	15.82		- - 				
		15.	00 0.450	- - 	0.450	1.980	15.82	14.10

Quick TR-55 Ver.5.46 S/N: Executed: 13:15:56 02-16-2015

MUSTANG INDUSTRIAL DEVELOPMENT EXISTING SITE OVERALL SUB BASIN 4

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

Q = adj * C * I * A
Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres
adj = 'C' adjustment factor for each return frequency

						=====			=======
Subarea Descr.	Runoff 'C'	Area acres	TC (min)	Wtd. 'C'		_	I in/hr	Total acres	Peak Q (cfs)
EXISTING	0.450	15.82			-11-				
			15.00	0.450	- - 	0.450	2.950	15.82	21.00

Quick TR-55 Ver.5.46 S/N: Executed: 13:16:25 02-16-2015

MUSTANG INDUSTRIAL DEVELOPMENT EXISTING SITE OVERALL SUB BASIN 5

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

Q = adj * C * I * A
Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres
adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 10 years
`C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

					===	=====		.====== -	======
Subarea	Runoff	Area	TC			_	I	Total	Peak Q
Descr.	'C'	acres	(min)	'C'		'C'	in/hr	acres	(cfs)
					- -				
EXISTING	0.450	30.08	Ì		11			Ĺ	
					- -				
			15.00	0.450	H	0.450	1.500	30.08	20.30

Quick TR-55 Ver.5.46 S/N: Executed: 13:16:25 02-16-2015

MUSTANG INDUSTRIAL DEVELOPMENT EXISTING SITE OVERALL SUB BASIN 5

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

Q = adj * C * I * A
Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres
adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 25 years
'C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

				====			======	
Subarea Descr.	Runoff 'C'		Tc Wtd. min) 'C'		_		Total acres	Peak Q (cfs)
EXISTING	0.450	30.08						
		1!	5.00 0.450	0	.450	1.980	30.08	26.80

Quick TR-55 Ver.5.46 S/N: Executed: 13:16:25 02-16-2015

MUSTANG INDUSTRIAL DEVELOPMENT EXISTING SITE OVERALL SUB BASIN 5

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

 $\label{eq:Q} Q = adj \ * \ C \ * \ I \ * \ A$ Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency

> RETURN FREQUENCY = 100 years 'C' adjustment, k = 1 Adj. 'C' = Wtd.'C' x 1

					===		======	========	
Subarea	Runoff	Area	Tc	Wtd.	11	Adj.	I	Total	Peak O
Descr.	'C'	acres	(min)	'C'	11	'C'	in/hr	acres	(cfs)
					- -				
EXISTING	0.450	30.08			11				
					-11-				
			15.00	0.450	11	0.450	2.950	30.08	39.93

APPENDIX C

DEVELOPED BASIN CALCULATIONS

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 1

* * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

 $\label{eq:Q} Q = \text{adj * C * I * A} \\ \text{Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres}$ adj = 'C' adjustment factor for each return frequency

> RETURN FREQUENCY = 10 years `C' adjustment, k = 1
> Adj. 'C' = Wtd.'C' x 1

					===		=======		
Subarea Descr.	Runoff 'C'	Area acres	Tc (min)	Wtd. 'C'		-	I in/hr		Peak Q (cfs)
					- -				
DEVELPED	0.750	11.27	1		11			1	İ
					-11-				
			10.00	0.750	H	0.750	1.810	11.27	15.30

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 1

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

 $\label{eq:Q} Q = \text{adj * C * I * A} \\$ Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 25 years

'C' adjustment, k = 1 Adj. 'C' = Wtd.'C' x 1

					===		========	=======	
Subarea Descr.	Runoff 'C'	Area acres	Tc (min)	Wtd.		Adj. 'C'	I in/hr	Total acres	Peak Q (cfs)
DEVELPED	0.750	11.27	 		- - - -				
			10.00	0.750	ii	0.750	2.390	11.27	20.20

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 1

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

 $\label{eq:Q} Q = \text{adj * C * I * A} \\ \text{Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres}$ adj = 'C' adjustment factor for each return frequency

> RETURN FREQUENCY = 100 years 'C' adjustment, k = 1 Adj. $C' = Wtd.'C' \times 1$

					===			-=======	
Subarea	Runoff	Area	TC	Wtd.	11	Adj.	I	Total	Peak Q
Descr.	'C'	acres	(min)	'C'	11	'Cī	in/hr	acres	(cfs)
					-11-				
DEVELPED	0.750	11.27			Ϊİ			İ	
					- -				
			10.00	0.750	11	0.750	3.570	11.27	30.18

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 2

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

Q = adj * C * I * A
Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres
adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 10 years C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

					===		=======		
Subarea Descr.	Runoff 'C'	Area acres	Tc (min)	Wtd. 'C'			I in/hr		Peak Q (cfs)
DEVELPED	0.860	8.76			- <i>-</i>]	
			10.00	0.860	11	0.860	1.810	8.76	13.64

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 2

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

 $\label{eq:Q} Q = \text{adj * C * I * A} \\ \text{Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres}$ adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 25 years
`C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

					===			======	======
Subarea Descr.		Area acres	•			_		Total acres	_
DEVELPED	0.860	8.76						 	
			10.00	0.860	11	0.860	2.390	8.76	18.01

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 2

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

Q = adj * C * I * A
Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres
adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 100 years
'C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

						_			1
					===	=====	======		=======
Subarea Descr.	Runoff 'C'	Area acres	(min)	'C'	İÌ	'Cī	in/hr	Total acres	(cfs)
DEVELPED	0.860		,		1 1				
			10.00	0.860	- [] 	0.860	3.570	8.76	26.89

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 3

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

 $\label{eq:Q} Q = adj \ ^* \ C \ ^* \ I \ ^* A$ Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 10 years
'C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

					===				
Subarea	Runoff	Area	Tc	Wtd.	11	Adj.	I	Total	Peak Q
Descr.	'C'	acres	(min)	'C'	11	'C'	in/hr	acres	(cfs)
					-11-		. .		
DEVELPED	0.770	51.81			11				
					- -				
			10.00	0.770	11	0.770	1.810	51.81	72.21

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 3

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

Q = adj * C * I * A
Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres
adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 25 years 'C' adjustment, k = 1 Adj. 'C' = Wtd.'C' x 1

					===				=======
Subarea Descr.	Runoff 'C'	Area acres	Tc (min)				I in/hr	Total acres	-
DEVELPED	0.770	51.81	 						
			 10.00	0.770	- - 	0.770	2.390	51.81	95.35

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 3

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

Q = adj * C * I * A
Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres
adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 100 years `C' adjustment, k = 1

Adj. $'C' = Wtd.'C' \times 1$

					===	=====			=======
Subarea Descr.	Runoff 'C'	Area acres				Adj. 'C'	I in/hr		Peak Q (cfs)
DEVELPED	0.770	51.81			- - - -				
			10.00	0.770	11	0.770	3.570	51.81	142.42

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 4

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * * *

Q = adj * C * I * A

Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 10 years

`C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 4

* * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * * * * * \star

Q = adj * C * I * A
Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres
adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 25 years `C' adjustment, k = 1 Adj. 'C' = Wtd.'C' x 1

					===	=====	======		=======
Subarea Descr.	Runoff 'C'	Area acres					I in/hr		Peak Q (cfs)
					-11-				
DEVELPED	0.700	15.82			11				Ī
					- -				
]	10.00	0.700	\Box	0.700	2.390	15.82	26.47

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 4

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

 $\label{eq:Q} Q = \text{adj * C * I * A} \\ \text{Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres}$ adj = 'C' adjustment factor for each return frequency

> RETURN FREQUENCY = 100 years
> `C' adjustment, k = 1 Adj. $C' = Wtd.'C' \times 1$

					===				
Subarea	Runoff	Area	Tc	Wtd.	11	Adj.	I	Total	Peak Q
Descr.	'C'	acres	(min)	'C'	11	'C'	in/hr	acres	(cfs)
					- -				
DEVELPED	0.700	15.82			11			1	
					-11-				
		į	10.00	0.700	H	0.700	3.570	15.82	39.53

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 5

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

Q = adj * C * I * A

Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 10 years
`C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 5

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

 $\label{eq:Q} Q = \text{adj * C * I * A} \\ \text{Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres}$ adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 25 years
`C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

					===	=====		========	
Subarea Descr.	Runoff 'C'	Area acres	Tc (min)	Wtd.		_	I in/hr	•	Peak Q (cfs)
DEVELPED	0.450	30.08			- -				
			15.00	0.450	- - 	0.450	1.980	30.08	26.80

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 5

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

 $\label{eq:Q} Q = \text{adj * C * I * A} \\ \text{Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres}$ adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 100 years
`C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

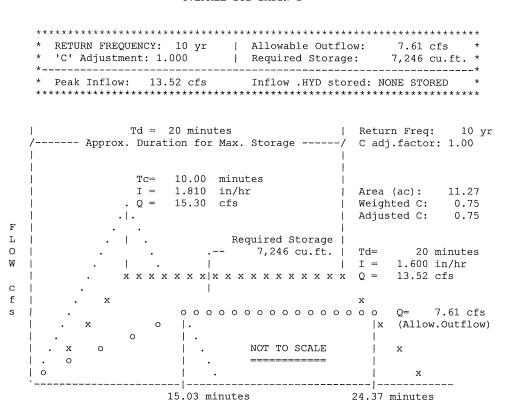
					===	=====			=======
Subarea	Runoff	Area	Tc	Wtd.	11	Adj.	I	Total	Peak Q
Descr.	'C'	acres	(min)	'C'		'C'	in/hr	acres	(cfs)
					-11-				
DEVELPED	0.450	30.08			11				
					- -				
		ĺ	15.00	0.450	H	0.450	2.950	30.08	39.93

APPENDIX D

DETENTION BASIN CALCULATIONS

MODIFIED RATIONAL METHOD ---- Graphical Summary for Maximum Required Storage ----

First peak outflow point assumed to occur at Tc hydrograph recession leg.



MODIFIED RATIONAL METHOD ---- Graphical Summary for Maximum Required Storage ----

First peak outflow point assumed to occur at Tc hydrograph recession leg.

* RETURN FREQUENCY: 25 yr Allowal * 'C' Adjustment: 1.000 Require	
* Peak Inflow: 15.64 cfs Inflow ************************************	
Td = 20 minutes / Approx. Duration for Max. Storage	Return Freq: 25 y
Tc= 10.00 minutes I = 2.390 in/hr Q = 20.20 cfs	Area (ac): 11.27 Weighted C: 0.75 Adjusted C: 0.75
Required S	cu.ft. Td= 20 minutes I = 1.850 in/hr
. x	:
.	-==== x

MODIFIED RATIONAL METHOD ---- Graphical Summary for Maximum Required Storage ----

First peak outflow point assumed to occur at Tc hydrograph recession leg.

*		REQUENCY: 1						14.96 ct 9,674 ct	
*		low: 27.(
 /	Аррі	Td = 1	13 minute ion for I			/ 		n Freq: .factor:	
		I =	10.00 r 3.570 r 30.18 d	in/hr		 	Weigh	(ac): ted C: ted C:	0.75
	· ·	. . . x x x x	 x x x x	- 19,	ed Stora 674 cu.f	t. i	I =		n/hr
	. x	0			OOOO	Ε	x o o x 	-	
1 .	0		.			-		х	

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 1

**** Modified Rational Hydrograph ***** Weighted C = 0.750 Area= 11.270 acres Tc = 10.00 minutes

Adjusted C = 0.750 Td= 20.00 min. I= 1.60 in/hr Qp= 13.52 cfs

RETURN FREQUENCY: 10 year storm Adj.factor = 1.00 Output file: NONE STORED

HYDROGRAPH FOR MAXIMUM STORAGE For the 10 Year Storm

Time Minutes	Time		Time increme represents				row.
0.00	0.00	1.35	2.70	4.06	5.41	6.76	8.11
7.00	9.47	10.82	12.17	13.52	13.52	13.52	13.52
14.00	13.52	13.52	13.52	13.52	13.52	13.52	13.52
21.00	12.17	10.82	9.47	8.11	6.76	5.41	4.06
28.00	2.70	1.35	0.00				

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 1

**** Modified Rational Hydrograph ***** Weighted C = 0.750 Area= 11.270 acres Tc = 10.00 minutes

Adjusted C = 0.750 Td= 20.00 min. I= 1.85 in/hr Qp= 15.64 cfs

RETURN FREQUENCY: 25 year storm Adj.factor = 1.00 Output file: NONE STORED

HYDROGRAPH FOR MAXIMUM STORAGE For the 25 Year Storm

Time			7	Time increme	ent = 1 .	00 Minute	es	
Minutes	-	Time	on left	represents	time for	first Q	in each	row.
0.00		0.00	1.56	3.13	4.69	6.25	7.82	9.38
7.00	1	10.95	12.51	14.07	15.64	15.64	15.64	15.64
14.00	}	15.64	15.64	15.64	15.64	15.64	15.64	15.64
21.00	1	14.07	12.51	10.95	9.38	7.82	6.25	4.69
28.00		3.13	1.56	0.00				

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 1

**** Modified Rational Hydrograph ***** Weighted C = 0.750 Area= 11.270 acres Tc = 10.00 minutes

Adjusted C = 0.750 Td= 13.00 min. I= 3.20 in/hr Qp= 27.03 cfs

RETURN FREQUENCY: 100 year storm Adj.factor = 1.00 Output file: NONE STORED

HYDROGRAPH FOR MAXIMUM STORAGE For the 100 Year Storm

Time		ŋ	Time increme	ent = $1.$	00 Minute	es	
Minutes	Time	on left	represents	time for	first Q	in each	row.
0.00	0.00	2.70	5.41	8.11	10.81	13.52	16.22
7.00	18.92	21.62	24.33	27.03	27.03	27.03	27.03
14.00	24.33	21.62	18.92	16.22	13.52	10.81	8.11
21.00	5.41	2.70	0.00				

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 1

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

Q = adj * C * I * A
Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres
adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 10 years
`C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

					===			=======	======
Subarea	Runoff	Area	Tc			_	I	Total	Peak Q
Descr.	'C'	acres	(min)	'C'	11	'C'	in/hr	acres	(cfs)
					- -				
DEVELPED	0.750	11.27	1		11			1	
					- -				
			10.00	0.750	İÌ	0.750	1.810	11.27	15.30

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 1

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

 $\label{eq:Q} Q = \text{adj * C * I * A} \\ \text{Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres}$ adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 25 years
'C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

					====	.=====			======
Subarea Descr.	Runoff 'C'	Area acres	Tc (min)			Adj. 'C'	I in/hr	Total acres	Peak Q (cfs)
DEVELPED	0.750	11.27			- - - -				
			10.00	0.750		0.750	2.390	11.27	20.20

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 1

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

Q = adj * C * I * A

Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 100 years `C' adjustment, k = 1 Adj. 'C' = Wtd.'C' \times 1

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* MODIFIED RATIONAL METHOD	*
* Grand Summary For All Storm Frequencies	*
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First peak outflow point assumed to occur at Tc hydrograph recession leg.

	A		11.27 ac	res		To	= 10.	00 minutes
::::::::	:::::::::		:::::::	::::::	:::::::::	:::	VO:	::::::: LUMES
Frequency (years)	Adjusted 'C'	Duration minutes	Intens. in/hr	Qpeak cfs	Allowable cfs		Inflow (cu.ft.	Storage) (cu.ft.)
10 25 100	0.750 0.750 0.750	20 20 13	1.600 1.850 3.198	13.52 15.64 27.03	7.61 10.04 14.96		16,229 18,765 21,084	7,246 7,153 9,674

MODIFIED RATIONAL METHOD ---- Summary for Single Storm Frequency ----

First peak outflow point assumed to occur at Tc hydrograph recession leg.

RETURN F	REQUENCY:	10 yr	'C' Adjust	ment =	1.000 All	owable Q =	7.61 cfs
Hydrogra	ph file: NC	NE STOREI)		::::::::::	Tc = 10.00	minutes
						AOLA	MES
Weighted `C'	'c'	minutes	in/hr	Areas acres	cfs	Inflow (cu.ft.)	(cu.ft.)
0.750 0.750			1.810 1.500		,	9,179	
*****	*****	*****	*****	*****	*****	**** Storage	e Maximum
0.750	0.750	20	1.600	11.27	13.52		7,246
0.750 0.750	0.750 0.750	30 40	1.139 0.859	11.27 11.27	9.63 7.26	17,328 Qpeak <	•

MODIFIED RATIONAL METHOD ---- Summary for Single Storm Frequency ----

First peak outflow point assumed to occur at Tc hydrograph recession leg.

RETURN FR	REQUENCY:	25 yr `(C' Adjust	ment = 1	1.000 Allo	wable Q =	10.04 cfs
Hydrograp	h file: NC	NE STORED			T	c = 10.00	minutes
Weighted `C'	Adjusted 'C'	Duration minutes	Intens. in/hr	Areas acres	Qpeak cfs	VOLUI Inflow (cu.ft.)	Storage
0.750 0.750	0.750 0.750	10 15	2.390 1.980		20.20 16.74	12,121 15,062	
0.750	0.750	20	1.850	11.27	15.64	**** Storage	7,153
0.750 0.750 0.750	0.750 0.750 0.750	30 40 50	1.450 1.200 1.100	11.27 11.27 11.27	12.26 10.14 9.30	22,061 24,343 Qpeak <	4,959 1,732

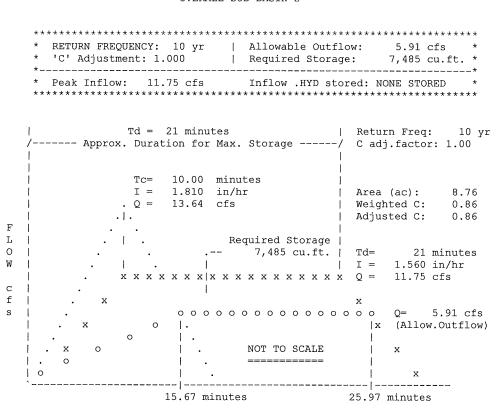
MODIFIED RATIONAL METHOD ---- Summary for Single Storm Frequency ----

First peak outflow point assumed to occur at Tc hydrograph recession leg.

RETURN FR	REQUENCY: 1	.00 yr `	C' Adjust	ment = 3	L.000 Allo	wable Q =	14.96 cfs
Hydrograp	oh file: NC	NE STORED	:::::::		T	c = 10.00	::::::::
Weighted `C'	Adjusted 'C'	minutes	in/hr		Qpeak cfs	<pre>Inflow (cu.ft.)</pre>	Storage (cu.ft.)
0.750	0.750	10	3.570			18,105	
******	*****	*****	******	******	******	**** Storage	e Maximum
					27.03		- /
0.750 0.750 0.750	0.750 0.750 0.750	15 20 30	2.950 2.500 1.733	11.27 11.27 11.27	24.93 21.13 14.65	22,441 25,358 Qpeak <	8,358

MODIFIED RATIONAL METHOD ---- Graphical Summary for Maximum Required Storage ----

First peak outflow point assumed to occur at Tc hydrograph recession leg.



F L O W

MODIFIED RATIONAL METHOD ---- Graphical Summary for Maximum Required Storage ----

First peak outflow point assumed to occur at Tc hydrograph recession leg.

* RETURN FREQUENCY: 25 yr Allowable Outfl * 'C' Adjustment: 1.000 Required Storag	
* Peak Inflow: 13.94 cfs Inflow .HYD sto	
Td = 20 minutes Approx. Duration for Max. Storage/	Return Freq: 25 C adj.factor: 1.00
Tc= 10.00 minutes	Area (ac): 8.76 Weighted C: 0.86 Adjusted C: 0.86
· · · · · · · · · · · · · · · · · · ·	Td= 20 minutes $I=$ 1.850 in/hr
. x	x 0 0 0 Q= 7.81 cf
. 0	

MODIFIED RATIONAL METHOD ---- Graphical Summary for Maximum Required Storage ----

First peak outflow point assumed to occur at Tc hydrograph recession leg.

*	RETURN FREQUENCY: 100 yr Allowable Outflo 'C' Adjustment: 1.000 Required Storage		11.63 cfs * 9,927 cu.ft. *
*	Peak Inflow: 23.16 cfs Inflow .HYD stor		
 /	Td = 14 minutes Approx. Duration for Max. Storage/		rn Freq: 100 y: j.factor: 1.00
	Tc= 10.00 minutes I = 3.570 in/hr Q = 26.89 cfs	Weig	(ac): 8.76 hted C: 0.86 sted C: 0.86
 	Required Storage 9,927 cu.ft. . . . x x x x x x x x x x x x x x x x x x x	Td= I = Q =	
[. x	x x	~

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 2

**** Modified Rational Hydrograph **** Weighted C = 0.860 Area= 8.760 acres Tc = 10.00 minutes

Adjusted C = 0.860 Td= 21.00 min. I= 1.56 in/hr Qp= 11.75 cfs

RETURN FREQUENCY: 10 year storm Adj.factor = 1.00

Output file: NONE STORED

HYDROGRAPH FOR MAXIMUM STORAGE For the 10 Year Storm

Time		Time increment = 1.00 Minutes								
Minutes	Time	on left	represents	time for	first Q	in each	row.			
0.00	0.00	1.18	2.35	3.53	4.70	5.88	7.05			
7.00	8.23	9.40	10.58	11.75	11.75	11.75	11.75			
14.00	11.75	11.75	11.75	11.75	11.75	11.75	11.75			
21.00	11.75	10.58	9.40	8.23	7.05	5.88	4.70			
28.00	3.53	2.35	1.18	0.00						

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 2

**** Modified Rational Hydrograph ***** Weighted C = 0.860 Area= 8.760 acres Tc = 10.00 minutes

Adjusted C = 0.860 Td= 20.00 min. I= 1.85 in/hr Qp= 13.94 cfs

RETURN FREQUENCY: 25 year storm Adj.factor = 1.00 Output file: NONE STORED

HYDROGRAPH FOR MAXIMUM STORAGE For the 25 Year Storm

Time		Time increment = 1.00 Minutes Time on left represents time for first Q in each row.							
Minutes	Time	on left	represents	time for	first Q	in each	row.		
0.00	0.00	1.39	2.79	4.18	5.57	6.97	8.36		
7.00	9.76	11.15	12.54	13.94	13.94	13.94	13.94		
14.00	13.94	13.94	13.94	13.94	13.94	13.94	13.94		
21.00	12.54	11.15	9.76	8.36	6.97	5.57	4.18		
28.00	2.79	1.39	0.00						

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 2

**** Modified Rational Hydrograph **** Weighted C = 0.860 Area= 8.760 acres Tc = 10.00 minutes

Adjusted C = 0.860 Td= 14.00 min. I= 3.07 in/hr Qp= 23.16 cfs

RETURN FREQUENCY: 100 year storm Adj.factor = 1.00

Output file: NONE STORED

HYDROGRAPH FOR MAXIMUM STORAGE For the 100 Year Storm

Time Minutes	Time increment = 1.00 Minutes Time on left represents time for first Q in each row.						
0.00 i	0.00	2.32	4.63	6.95	9.26	11.58	13.89
7.00	16.21	18.53	20.84	23.16	23.16	23.16	23.16
14.00	23.16	20.84	18.53	16.21	13.89	11.58	9.26
21.00	6.95	4.63	2.32	0.00			

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 2

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

 $\label{eq:Q} Q = \text{adj * C * I * A} \\$ Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency

> RETURN FREQUENCY = 10 years `C' adjustment, k = 1Adj. $C' = Wtd.C' \times 1$

					===	=====	======	======	=======
Subarea	Runoff		TC					Total	~
Descr.	'C'	acres (min)	'C'		'C'	in/hr	acres	(cfs)
					- -				
DEVELPED	0.860	8.76							
					-11-				
		1 1	0.00	0.860	11	0.860	1.810	8.76	13.64

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 2

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

Q = adj * C * I * A
Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres
adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 25 years
`C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

					===	======			
Subarea Descr.	Runoff 'C'	Area acres	Tc (min)	Wtd. 'C'		Adj. 'C'	I in/hr	Total acres	Peak Q (cfs)
					-				
DEVELPED	0.860	8.76	***************************************					1	
			I		-11-				
			10.00	0.860	ii	0.860	2.390	8.76	18.01

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 2

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

Q = adj * C * I * A

Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 100 years

`C' adjustment, k = 1 Adj. 'C' = Wtd.'C' x 1

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* MODIFIED RATIONAL METHOD	*
* Grand Summary For All Storm Frequencies	*
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First peak outflow point assumed to occur at Tc hydrograph recession leg.

	A	rea =	8.76 ac	res		Тc	= 10.00	minutes
::::::::	:::::::::	::::::::	:::::::	::::::	:::::::::::	:::	:::::::::	::::::::
							VOLUI	MES
Frequency	Adjusted	Duration	Intens.	Qpeak	Allowable	ŀ	Inflow	Storage
(years)	'C'	minutes	in/hr	cfs	cfs	1	(cu.ft.)	(cu.ft.)
						·		
10	0.860	21	1.560	11.75	5.91		14,808	7,485
25	0.860	20	1.850	13.94	7.81		16,725	7,649
100	0.860	14	3.074	23.16	11.63	1	19,453	9,927

MODIFIED RATIONAL METHOD ---- Summary for Single Storm Frequency ----

First peak outflow point assumed to occur at Tc hydrograph recession leg.

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 2

RETURN FR	EQUENCY:	10 yr ``	C' Adjust	ment = 1	.000 Allo	wable Q =	5.91 cfs			
Hydrograph file: NONE STORED Tc = 10.00 minutes										
Weighted `C'	Adjusted 'C'	Duration minutes	Intens. in/hr	Areas acres	Qpeak cfs	VOLU Inflow (cu.ft.)	Storage			
0.860 0.860 0.860	0.860 0.860 0.860	10 15 20	1.810 1.500 1.600	8.76 8.76 8.76	13.64 11.30 12.05	8,181 10,170 14,465	4,635 5,010 7,473			
0.860	0.860	21	1.560	8.76	********* 11.75 ******	14,808	7,485			
0.860 0.860 0.860	0.860 0.860 0.860	30 40 50 60	1.139 0.859 0.900 0.800	8.76 8.76 8.76 8.76	8.58 6.47 6.78 6.03	15,444 15,533 20,341 21,697	1,391			
0.860	0.860	120	0.520	8.76	3.92	Qpeak <	QattoM.			

MODIFIED RATIONAL METHOD ---- Summary for Single Storm Frequency ----

First peak outflow point assumed to occur at Tc hydrograph recession leg.

RETURN FREQUENCY:	25 yr	`C' Adjustment = 1.000	Allowable Q =	7.81 cfs

Hydrograp	h file: NC	NE STORED	:::::::	:::::::	Tc	c = 10.00	::::::::
Weighted `C'	Adjusted 'C'	Duration minutes	Intens. in/hr	Areas acres	Qpeak cfs 	Inflow (cu.ft.)	Storage (cu.ft.)
0.860 0.860	0.860 0.860	10 15	2.390 1.980		18.01 14.92	10,803 13,425	6,117 6,606
******	*****	*****	*****	******	*****	*** Storage	e Maximum
0.860	0.860	20	1.850	8.76	13.94 ******	16,725	7,649
0.860 0.860 0.860 0.860	0.860 0.860 0.860 0.860	30 40 50 60	1.450 1.200 1.100 0.930	8.76 8.76 8.76 8.76	10.92 9.04 8.29 7.01	19,663 21,697 24,861 Qpeak <	•

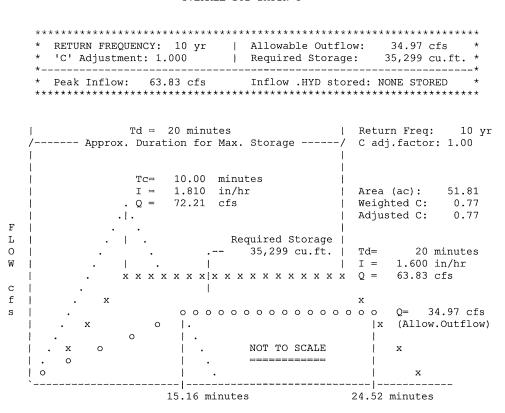
MODIFIED RATIONAL METHOD ---- Summary for Single Storm Frequency ----

First peak outflow point assumed to occur at Tc hydrograph recession leg.

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 2

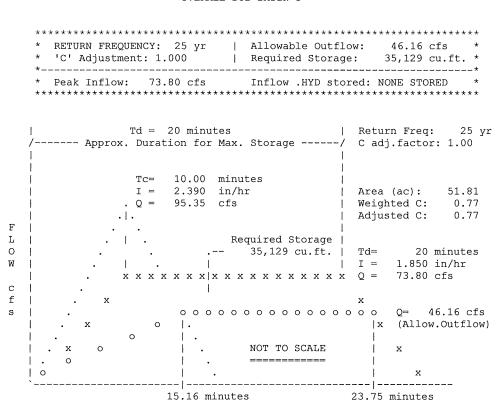
MODIFIED RATIONAL METHOD ---- Graphical Summary for Maximum Required Storage ----

First peak outflow point assumed to occur at Tc hydrograph recession leg.



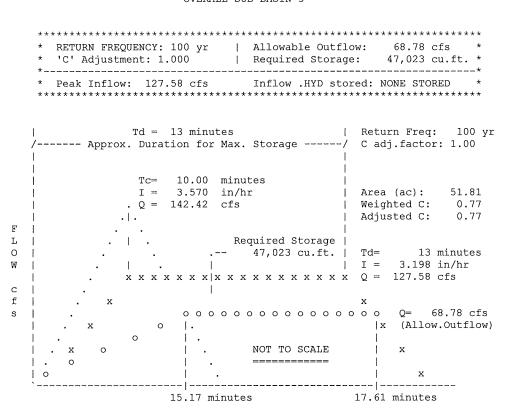
MODIFIED RATIONAL METHOD ---- Graphical Summary for Maximum Required Storage ----

First peak outflow point assumed to occur at Tc hydrograph recession leg.



MODIFIED RATIONAL METHOD ---- Graphical Summary for Maximum Required Storage ----

First peak outflow point assumed to occur at Tc hydrograph recession leg.



MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 3

**** Modified Rational Hydrograph **** Weighted C = 0.770 Area 51.810 acres Tc = 10.00 minutes

Adjusted C = 0.770 Td= 20.00 min. I = 1.60 in/hr Qp= 63.83 cfs

RETURN FREQUENCY: 10 year storm Adj.factor = 1.00 Output file: NONE STORED

HYDROGRAPH FOR MAXIMUM STORAGE For the 10 Year Storm

Time		_	Time increme				
Minutes	Time	on left	represents	time for	first Q	in each	row.
0.00	0.00	6.38	12.77	19.15	25.53	31.91	38.30
7.00	44.68	51.06	57.45	63.83	63.83	63.83	63.83
14.00	63.83	63.83	63.83	63.83	63.83	63.83	63.83
21.00	57.45	51.06	44.68	38.30	31.91	25.53	19.15
28.00	12.77	6.38	0.00				

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 3

**** Modified Rational Hydrograph **** Weighted C = 0.770 Area= 51.810 acres Tc = 10.00 minutes

Adjusted C = 0.770 Td= 20.00 min. I= 1.85 in/hr Qp= 73.80 cfs

RETURN FREQUENCY: 25 year storm Adj.factor = 1.00

Output file: NONE STORED

HYDROGRAPH FOR MAXIMUM STORAGE For the 25 Year Storm

Time		Time increment = 1.00 Minutes								
Minutes	Time	on left	represents	time for	first Q	in each	row.			
0.00	0.00	7.38	14.76	22.14	29.52	36.90	44.28			
7.00	51.66	59.04	66.42	73.80	73.80	73.80	73.80			
14.00	73.80	73.80	73.80	73.80	73.80	73.80	73.80			
21.00	66.42	59.04	51.66	44.28	36.90	29.52	22.14			
28.00	14.76	7.38	0.00							

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 3

**** Modified Rational Hydrograph ***** Weighted C = 0.770 Area= 51.810 acres Tc = 10.00 minutes

Adjusted C = 0.770 Td= $13.00 \, \text{min}$. I= $3.20 \, \text{in/hr}$ Qp= $127.58 \, \text{cfs}$

RETURN FREQUENCY: 100 year storm Adj.factor = 1.00

Output file: NONE STORED

HYDROGRAPH FOR MAXIMUM STORAGE For the 100 Year Storm

Time		7	Time increme	ent = $1.$	00 Minute	es	
Minutes	Time	on left	represents	time for	first Q	in each	row.
0.00	0.00	12.76	25.52	38.27	51.03	63.79	76.55
7.00	89.31	102.06	114.82	127.58	127.58	127.58	127.58
14.00	114.82	102.06	89.31	76.55	63.79	51.03	38.27
21.00	25.52	12.76	0.00				

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 3

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

 $\label{eq:Q} Q = \text{adj * C * I * A} \\ \text{Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres}$ adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 10 years
'C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

						_			
					===		=======		
Subarea Descr.	Runoff 'C'	Area acres				_		Total acres	Peak Q (cfs)
					- -				
DEVELPED	0.770	51.81			11				l
					-11-				
			10.00	0.770	11	0.770	1.810	51.81	72.21

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 3

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

 $\label{eq:Q} Q = \text{adj * C * I * A} \\$ Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 25 years
`C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

				=====	========		=======
Subarea Descr.	Runoff 'C'	Area To			Adj. I C' in/hr		Peak Q (cfs)
DEVELPED	0.770	51.81		- 			
		10.	00 0.770	0.	770 2.390	51.81	95.35

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 3

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

Q = adj * C * I * A
Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres
adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 100 years
'C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

						Auj.	C - WLC	1. C A I	
						=====			=======
Subarea	Runoff	Area	TC	Wtd.	11	Adj.	I	Total	Peak Q
Descr.	'C'	acres	(min)	'C'	1	'C'	in/hr	acres	(cfs)
					- -				
DEVELPED	0.770	51.81	1		Ħ				
					- -				
			10.00	0.770	H	0.770	3.570	51.81	142.42

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* MODIFIED RATIONAL METHOD	*
* Grand Summary For All Storm Frequencies	*
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First peak outflow point assumed to occur at Tc hydrograph recession leg.

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 3

VOLUMES

Frequency (years)	Adjusted 'C'	Duration minutes	Intens. in/hr	Qpeak cfs	Allowable cfs		Inflow (cu.ft.)	Storage (cu.ft.)
10	0.770	20	1.600	63.83	34.97		76,596	35,299
25	0.770	20	1.850	73.80	46.16		88,564	35,129
100	0.770	13	3.198	127.58	68.78		99,512	47,023

MODIFIED RATIONAL METHOD ---- Summary for Single Storm Frequency ----

First peak outflow point assumed to occur at Tc hydrograph recession leg.

RETURN FR	EQUENCY:	10 yr `C	' Adjust	ment =	1.000 All	owable Q =	34.97 cfs
						m = 10 00	
нуdrograp	h file: NO	NE STORED				Tc = 10.00	minutes
::::::::	:::::::::	:::::::::	:::::::	::::::		VOLU	MES
Weighted	,	Duration	Intens.	Areas		Inflow	_
`C'	'C'	minutes		acres	•	(cu.ft.)	
			1.810		•		•
0.770	0.770	15	1.500	51.81	59.84	53,856	23,434
*****	*****	*****	*****	*****	*****	**** Storag	e Maximum
					63.83	_	
*****						*****	****
0.770	0.770	30	1.139	51.81	45.43	81,782	21,830
0.770	0.770	40	0.859	51.81	34.27	Qpeak <	Qallow

MODIFIED RATIONAL METHOD ---- Summary for Single Storm Frequency ----

First peak outflow point assumed to occur at Tc hydrograph recession leg.

RETURN FR	EQUENCY:	25 yr ``	C' Adjust	ment =	1.000 All	lowable Q = 4	16.16 cfs			
Hydrograph file: NONE STORED Tc = 10.00 minutes										
						VOLUM				
Weighted `C'	Adjusted 'C'	minutes	in/hr	Areas acres	Qpeak cfs	•	Storage (cu.ft.)			
0.770 0.770	0.770 0.770	10 15		51.81 51.81			29,512 30,935			
******	******	*****	*****	*****	*****	***** Storage	Maximum			
0.770	0.770					88,564 ******	35,129			

0.770 0.770 0.770	0.770 0.770 0.770	30 40 50	1.450 1.200 1.100	51.81 51.81 51.81	57.85 47.87 43.88		10,758			

MODIFIED RATIONAL METHOD ---- Summary for Single Storm Frequency ----

First peak outflow point assumed to occur at Tc hydrograph recession leg.

RETURN FR	REQUENCY: 1	.00 yr ``	C' Adjust	ment = 1	1.000 Allo	owable Q =	68.78 cfs			
Hydrograph file: NONE STORED Tc = 10.00 minutes										
`č'	Adjusted	minutes	in/hr	Areas acres	cfs	VOLU Inflow (cu.ft.)	Storage (cu.ft.)			
0.770	0.770	10		51.81		85 , 452				
0.770	0.770	13	3.198	51.81	127.58	**** Storag 99,512 ******	47,023			
0.770 0.770 0.770 0.770	0.770 0.770 0.770 0.770	15 20 30 40	2.950 2.500 1.733 1.262	51.81 51.81 51.81 51.81	117.69 99.73 69.15 50.34	105,918 119,681 124,468 Qpeak <	•			

MODIFIED RATIONAL METHOD ---- Graphical Summary for Maximum Required Storage ----

First peak outflow point assumed to occur at Tc hydrograph recession leg.

		10 yr Allowab 000 Require		
		72 cfs Inflow **********		
 /		20 minutes ion for Max. Storage		ırn Freq: 10 dj.factor: 1.00
	I =	10.00 minutes 1.810 in/hr 20.04 cfs	Weig	a (ac): 15.8 ghted C: 0.7 usted C: 0.7
[[Required S 8,670 x x x x x x x x x x	cu.ft. Td=	20 minute 1.600 in/hr 17.72 cfs
		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SCALE	Q= 10.68 c (Allow.Outfl

MODIFIED RATIONAL METHOD ---- Graphical Summary for Maximum Required Storage ----

First peak outflow point assumed to occur at Tc hydrograph recession leg.

*				Allowable Outf Required Stora		
				Inflow .HYD st		
 /	Appr		20 minutes ion for Ma	x. Storage		rn Freq: 25
		I =	10.00 min 2.390 in 26.47 cf	/hr	Weigh	(ac): 15.82 ated C: 0.70 sted C: 0.70
			· I	Required Storage 8,322 cu.ft. xxxxxxxx	Td=	1.850 in/hr
	. x . x . x o	0	0000	OOOOOOOOO		Q= 14.10 cf (Allow.Outflo
1 .	0					x

MODIFIED RATIONAL METHOD ---- Graphical Summary for Maximum Required Storage ----

First peak outflow point assumed to occur at Tc hydrograph recession leg.

* RETURN FREQUENCY: 1 * 'C' Adjustment: 1.0	00 yr Allowable Outf 000 Required Stora	low: 21.00 cfs * ge: 11,633 cu.ft. *
	ll cfs Inflow .HYD st	
	.3 minutes on for Max. Storage	Return Freq: 100 y / C adj.factor: 1.00
I =	10.00 minutes 3.570 in/hr 39.53 cfs	Area (ac): 15.82 Weighted C: 0.70 Adjusted C: 0.70
	Required Storage 11,633 cu.ft. x x x x x x x x x x x x x	Td= 13 minutes I = 3.198 in/hr
. x o	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	x 0 0 0 0 Q= 21.00 cfs x (Allow.Outflow
. x o	NOT TO SCALE	X X

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 4

**** Modified Rational Hydrograph *****

Weighted C = 0.700 Area 15.820 acres Tc = 10.00 minutes

Adjusted C = 0.700 Td= 20.00 min. I= 1.60 in/hr Qp= 17.72 cfs

RETURN FREQUENCY: 10 year storm Adj.factor = 1.00 Output file: NONE STORED

HYDROGRAPH FOR MAXIMUM STORAGE For the 10 Year Storm

Time		Time increment = 1.00 Minutes								
Minutes	Time	on left	represents	time for	first Q	in each	row.			
					-					
0.00	0.00	1.77	3.54	5.32	7.09	8.86	10.63			
7.00	12.40	14.17	15.95	17.72	17.72	17.72	17.72			
14.00	17.72	17.72	17.72	17.72	17.72	17.72	17.72			
21.00	15.95	14.17	12.40	10.63	8.86	7.09	5.32			
28.00	3.54	1.77	0.00							

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 4

Adjusted C = 0.700 Td= 20.00 min. I= 1.85 in/hr Qp= 20.49 cfs

RETURN FREQUENCY: 25 year storm Adj.factor = 1.00 Output file: NONE STORED

HYDROGRAPH FOR MAXIMUM STORAGE For the 25 Year Storm

Time		7	Time increme	ent = 1.	00 Minute	es	
Minutes	Time	on left	represents	time for	first Q	in each	row.
0.00	0.00	2.05	4.10	6.15	8.19	10.24	12.29
7.00	14.34	16.39	18.44	20.49	20.49	20.49	20.49
14.00	20.49	20.49	20.49	20.49	20.49	20.49	20.49
21.00	18.44	16.39	14.34	12.29	10.24	8.19	6.15
28.00	4.10	2.05	0.00				

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 4

**** Modified Rational Hydrograph ***** Weighted C = 0.700 Area= 15.820 acres Tc = 10.00 minutes

Adjusted C = 0.700 Td= 13.00 min. I= 3.20 in/hr Qp= 35.41 cfs

RETURN FREQUENCY: 100 year storm Adj.factor = 1.00

Output file: NONE STORED

HYDROGRAPH FOR MAXIMUM STORAGE For the 100 Year Storm

Time		7	Time increme	ent = 1	.00 Minute	es	
Minutes	Time	on left	represents	time for	r first Q	in each	row.
		-					
0.00	0.00	3.54	7.08	10.62	14.17	17.71	21.25
7.00	24.79	28.33	31.87	35.41	35.41	35.41	35.41
14.00	31.87	28.33	24.79	21.25	17.71	14.17	10.62
21.00	7.08	3.54	0.00				

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 4

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

 $\label{eq:Q} Q = \text{adj * C * I * A} \\ \text{Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres}$ adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 10 years `C' adjustment, k = 1 Adj. 'C' = Wtd.'C' x 1

					===			=======	
Subarea Descr.	Runoff 'C'	Area acres	Tc (min)	Wtd.			I in/hr	Total acres	Peak Q (cfs)
DEVELPED	0.700	15.82						Ī	
			10.00	0.700	-11- 11	0.700	1.810	15.82	20.04

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 4

* * * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

Q = adj * C * I * A
Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres
adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 25 years
'C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

					===				
Subarea Descr.	Runoff 'C'	Area	•			_		Total acres	Peak Q (cfs)
DEVELPED	0.700	15.82	 						
			10.00	0.700		0.700	2.390	15.82	26.47

MUSTANG INDUSTRIAL DEVELOPMENT DEVELOPED SITE OVERALL SUB BASIN 4

* * * * * SUMMARY OF RATIONAL METHOD PEAK DISCHARGES * * * * * *

 $\label{eq:Q} Q = \text{adj * C * I * A} \\ \text{Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres}$ adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 100 years

`C' adjustment, k = 1 Adj. 'C' = Wtd.'C' x 1

Descr.	'C'	acres	(min)	Wtd. 'C'	'C'	in/hr	acres	(cfs)
DEVELPED	0.700	15.82	İ	11			1	
			10.00	0.700	0.700	3.570	15.82	39.53

*******************	**
***************	**
*	*
*	*
* MODIFIED RATIONAL METHOD	*
* Grand Summary For All Storm Frequencies	*
*	*
*	*
*****************	* *
*****************	* *

First peak outflow point assumed to occur at Tc hydrograph recession leg.

		rea = 3	15.82 acı	res		Tc	= 10.0	0 minutes
							VOL	UMES
Frequency	Adjusted	Duration			Allowable	1	Inflow	Storage
(years)	'C'	minutes	in/hr	cfs	cfs		(cu.ft.)	(cu.ft.)
10	0.700	20	1.600	17.72	10.68		21,262	8,670
25	0.700	20	1.850	20.49	14.10	1	24,584	8,322
100	0.700	13	3.198	35.41	21.00		27,623	11,633

MODIFIED RATIONAL METHOD ---- Summary for Single Storm Frequency ----

First peak outflow point assumed to occur at Tc hydrograph recession leg.

						owable Q =	
	ph file: NC				,	Tc = 10.00	minutes
		,				AOTA	MES
`č'	-	minutes	in/hr	Areas	cfs	Inflow (cu.ft.)	(cu.ft.)
0.700	0.700		1.810			12,026	5,618
						**** Storag	
						21,262 ******	
	0.700 0.700	30 40	1.139 0.859	15.82 15.82	12.61 9.51	22,702 Qpeak <	•

MODIFIED RATIONAL METHOD ---- Summary for Single Storm Frequency ----

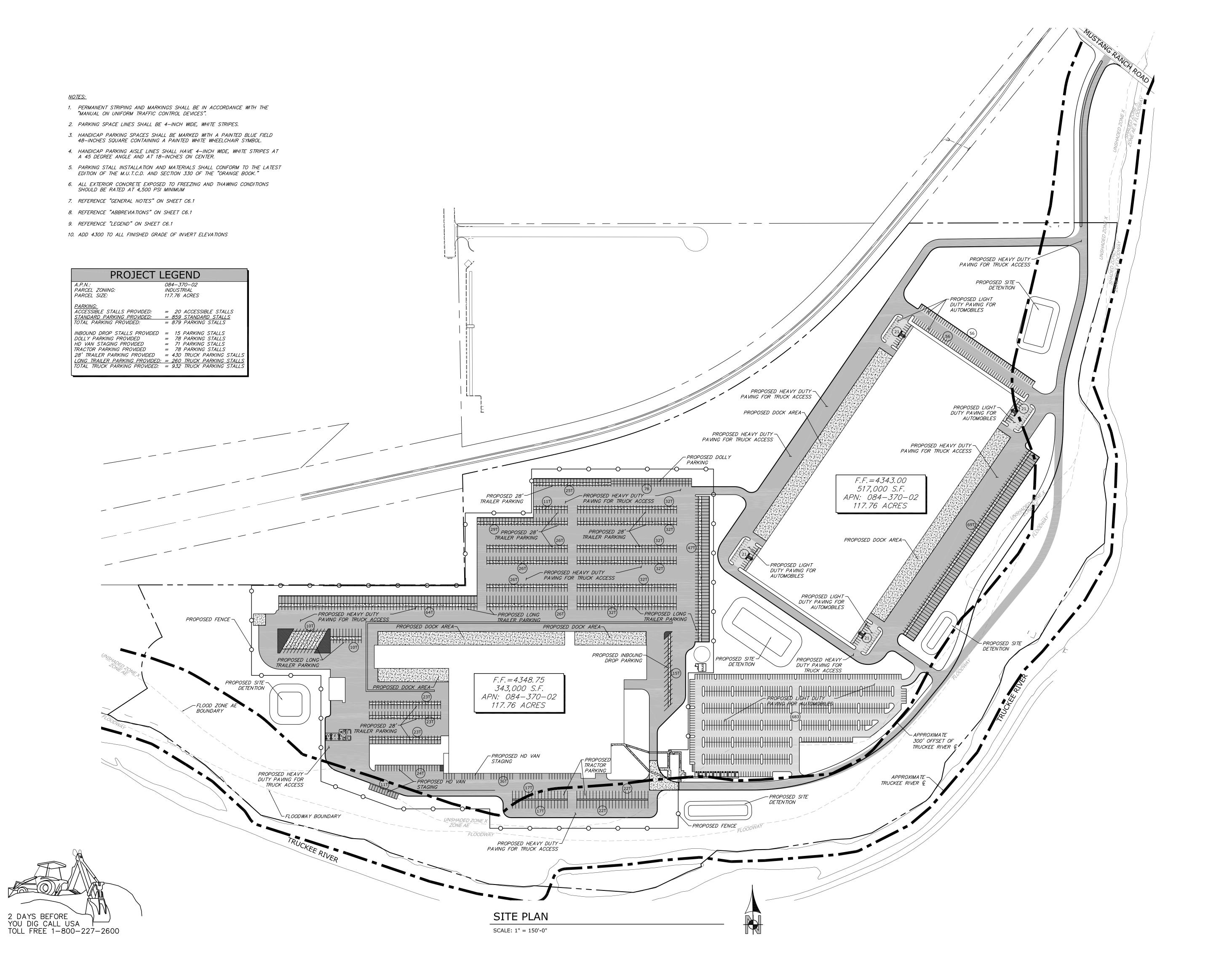
First peak outflow point assumed to occur at Tc hydrograph recession leg.

RETURN	FREQUENCY:	25 yr `C	C' Adjust	ment = :	1.000 All	owable Q =	14.10 cfs
Hydrogr	aph file: NO	NE STORED				Tc = 10.00	minutes
::::::	:::::::::	:::::::::	:::::::	::::::	:::::::::	VOLU	:::::: MES
Weighte	d Adjusted	Duration	Intens.	Areas		Inflow	-
`C'	'C'	minutes		acres		(cu.ft.)	
0.700	0.700	10	2.390		 26.47	15,880	
0.700	0.700	15	1.980	15.82	21.93		7,511
0.700	0.700	13	1.500	10.02	21.55 1	13,731	,,011
*****	*****	******	*****	****	*****	***** Storag	e Maximum
0.700	0.700	20	1.850	15.82	20.49	24,584	8,322
*****	******	******	******	*****	******	*****	*****
0.700	0.700		1.450		16.06	•	•
0.700	0.700	40	1.200	15.82	13.29	Qpeak <	Qallow

MODIFIED RATIONAL METHOD ---- Summary for Single Storm Frequency ----

First peak outflow point assumed to occur at $\ensuremath{\text{Tc}}$ hydrograph recession leg.

RETURN FR	EQUENCY: 1	00 yr `(C' Adjust	ment =	1.000 All	lowable Q	= 21.00 cfs
Hydrograp:	h file: NO	NE STORED				Tc = 10	.00 minutes
::::::::	:::::::::	:::::::::		::::::	:::::::::		OLUMES
`č'	Adjusted 'C'	minutes	in/hr		cfs		Storage .) (cu.ft.)
0.700	0.700	10				,	
*****	*****	*****	******	*****	*****	***** Sto	rage Maximum
					35.41		
******	*****	******	*****	*****	******	******	*****
0.700	0.700	15	2.950	15.82	32.67	29,401	11,205
0.700	0.700	20	2.500	15.82	27.68	33,222	9,454
0.700	0.700	30	1.733	15.82	19.19	Qpea	k < Qallow



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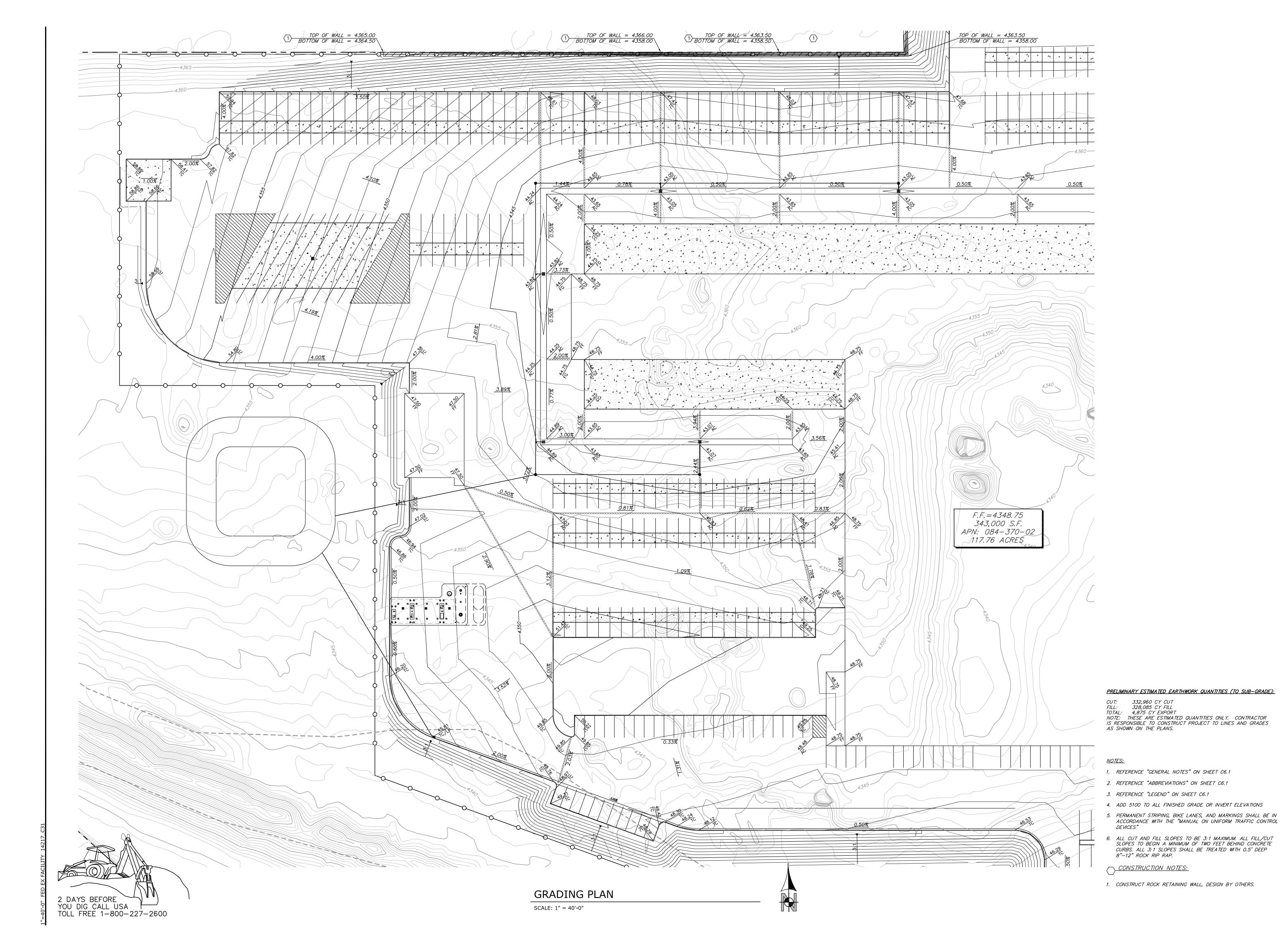
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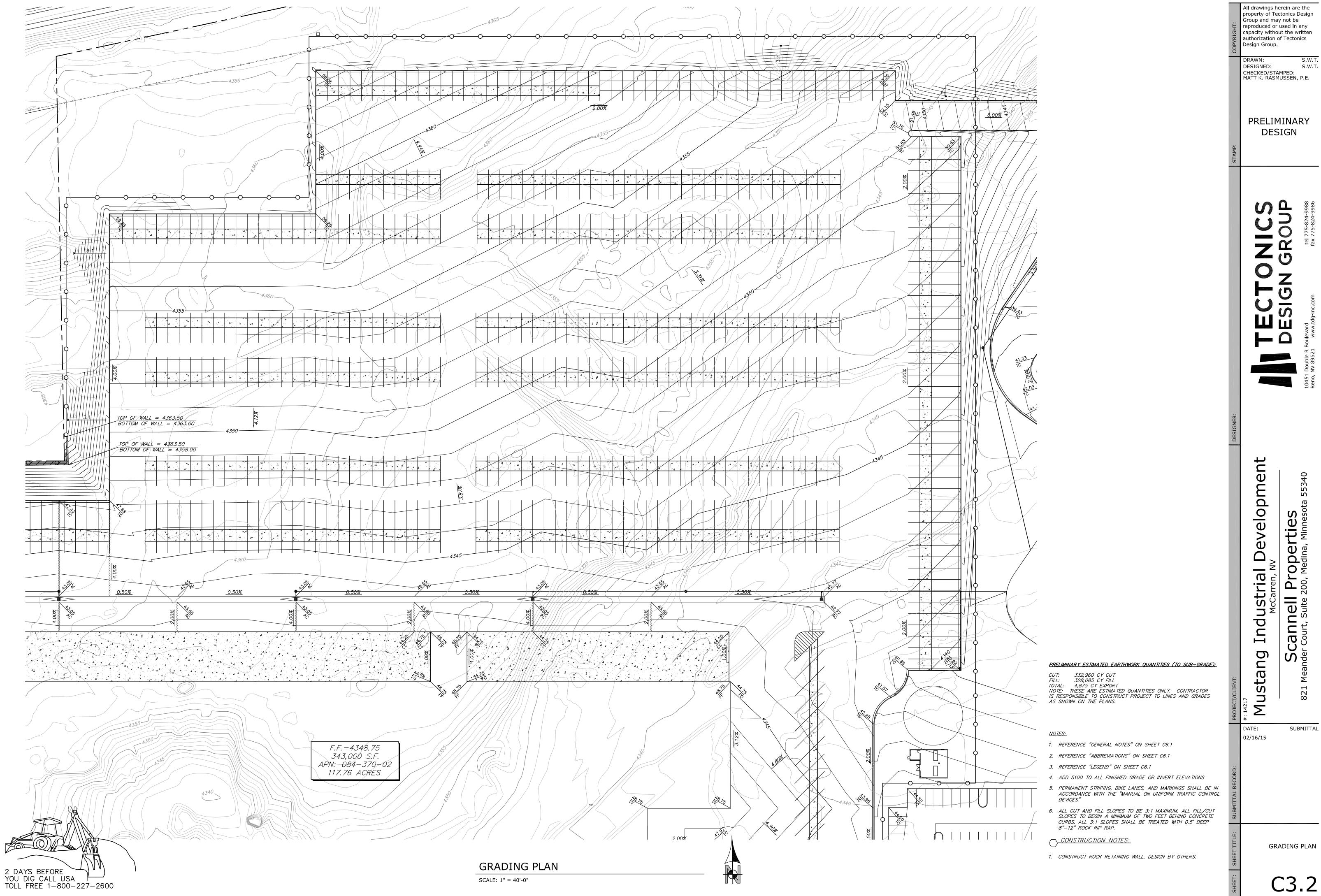
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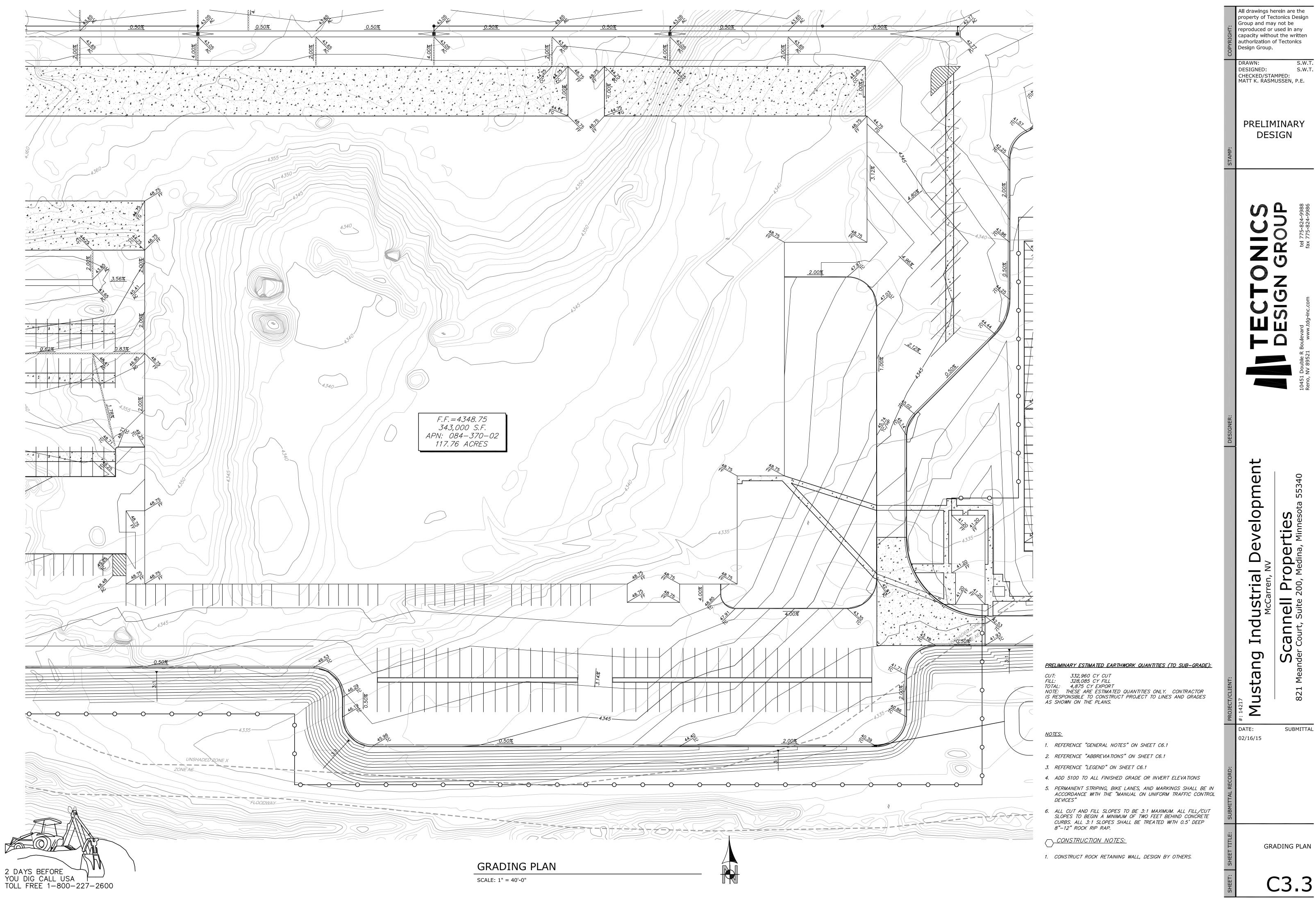
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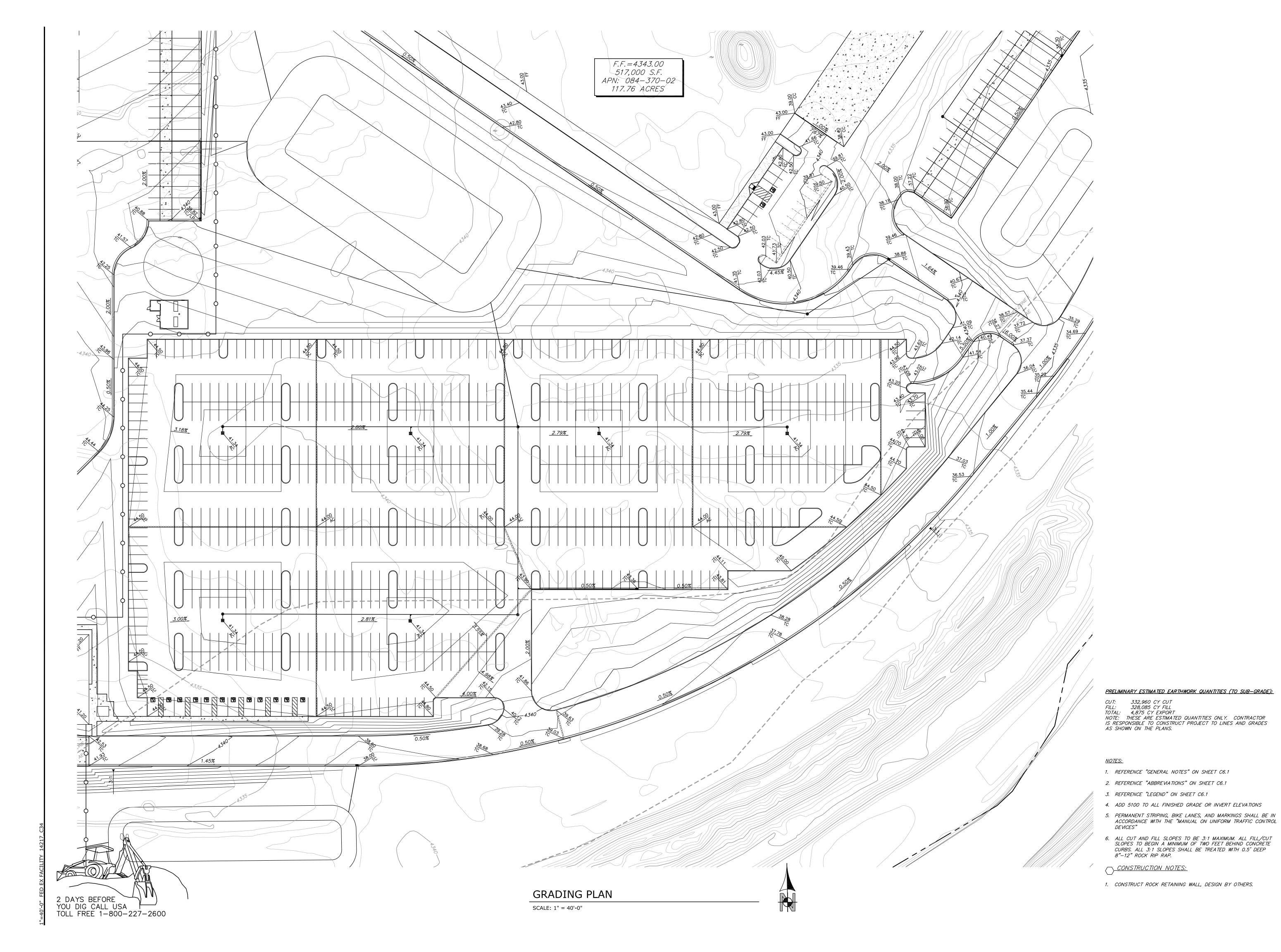
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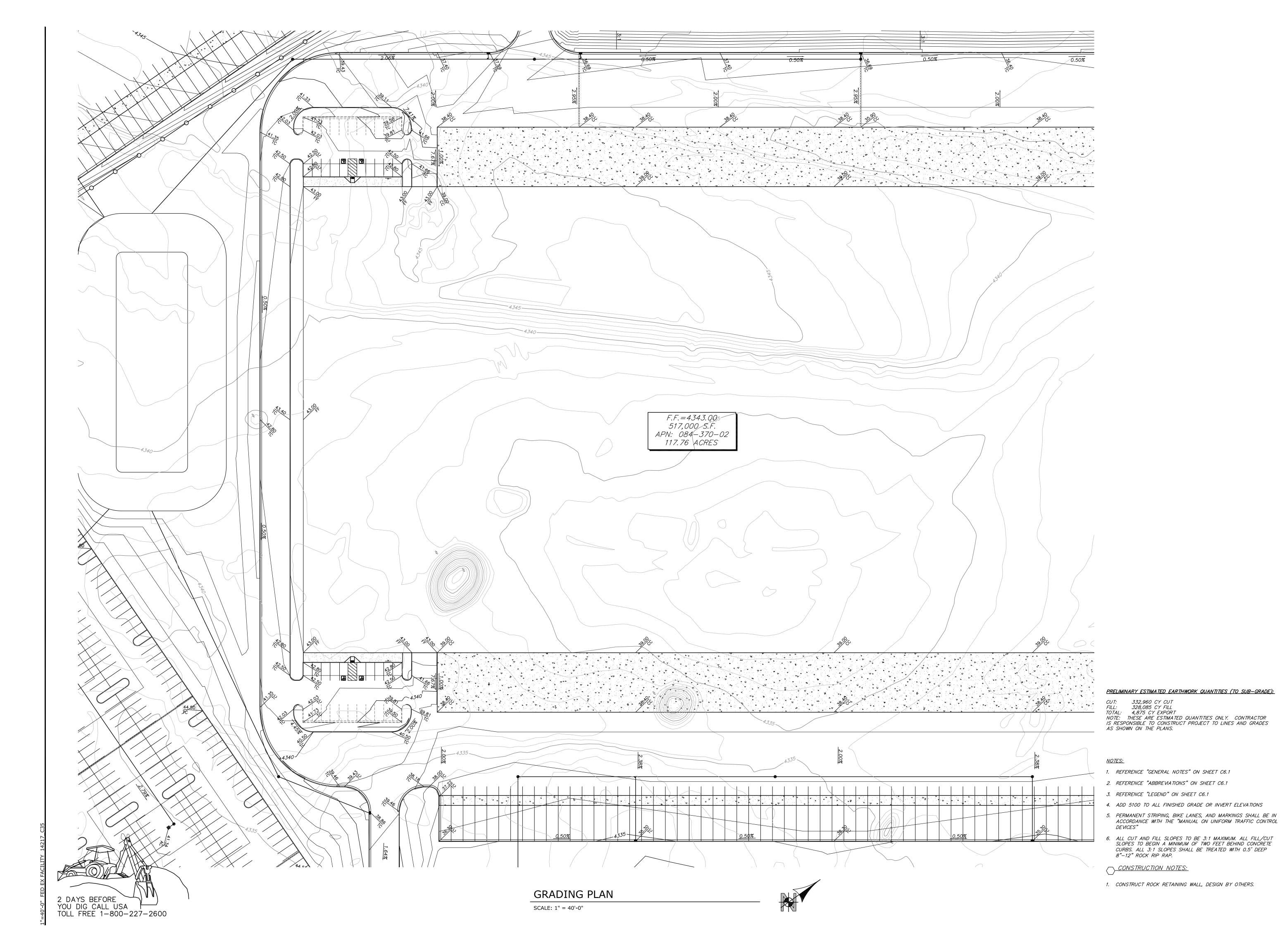
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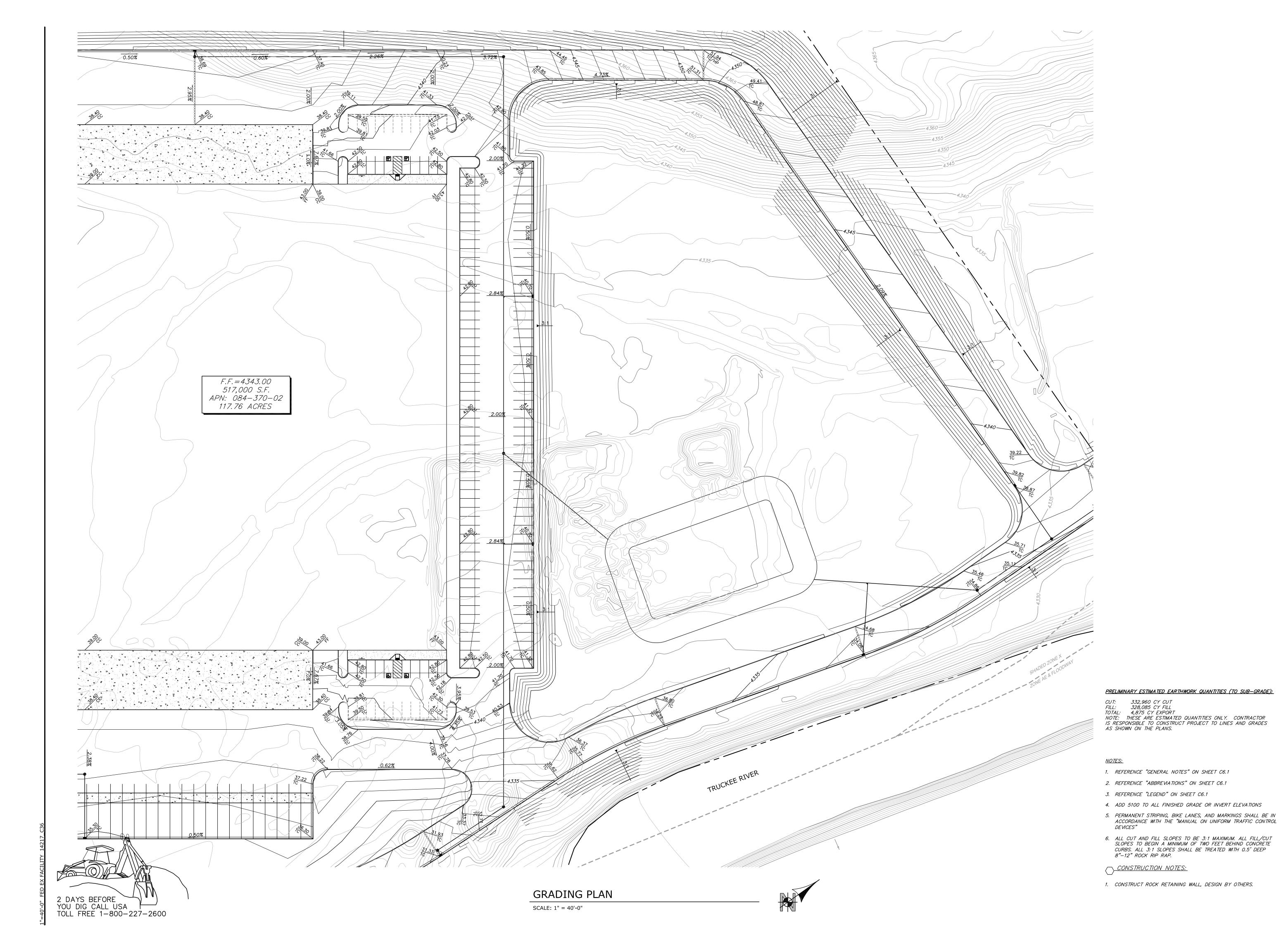
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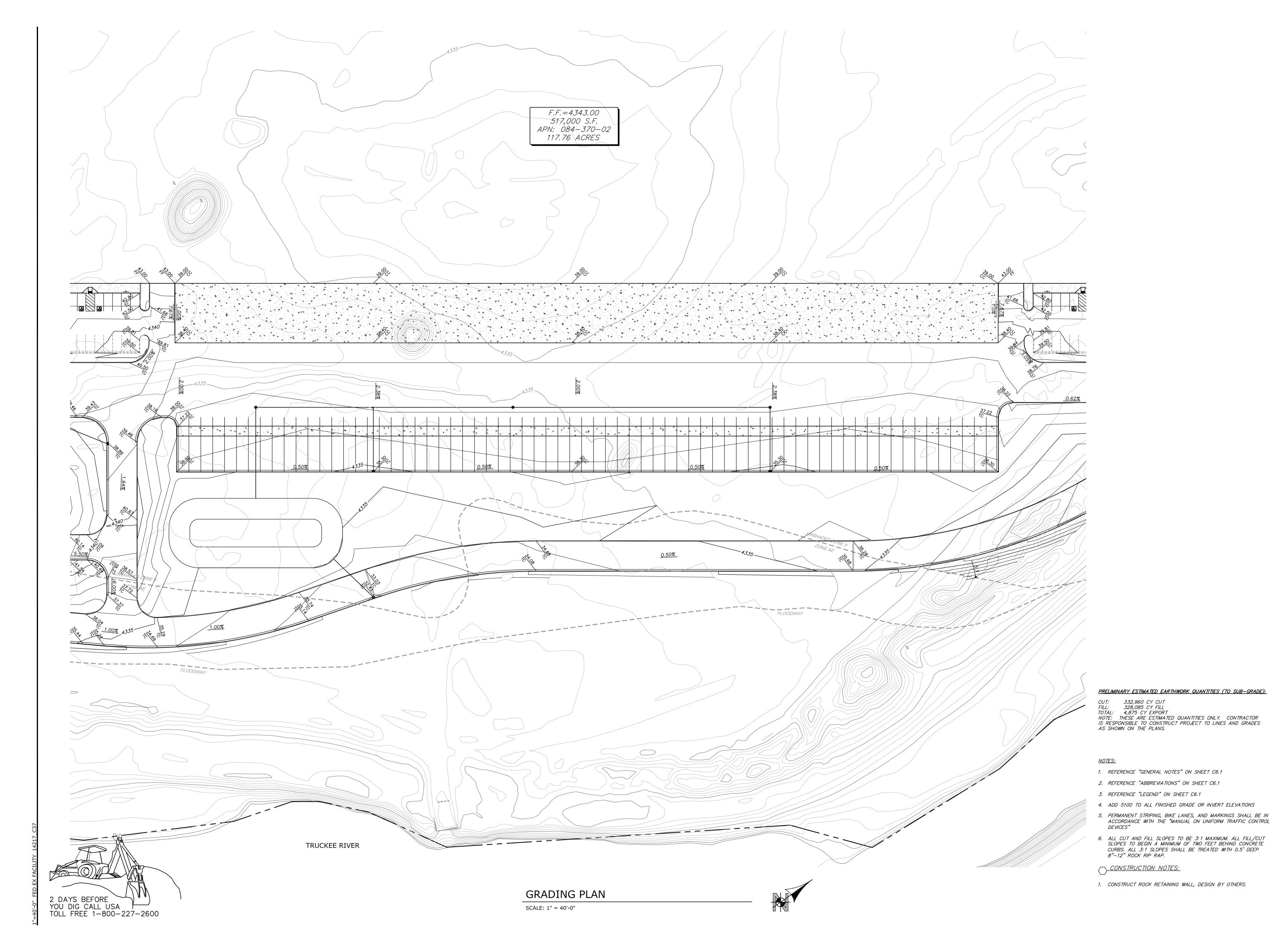
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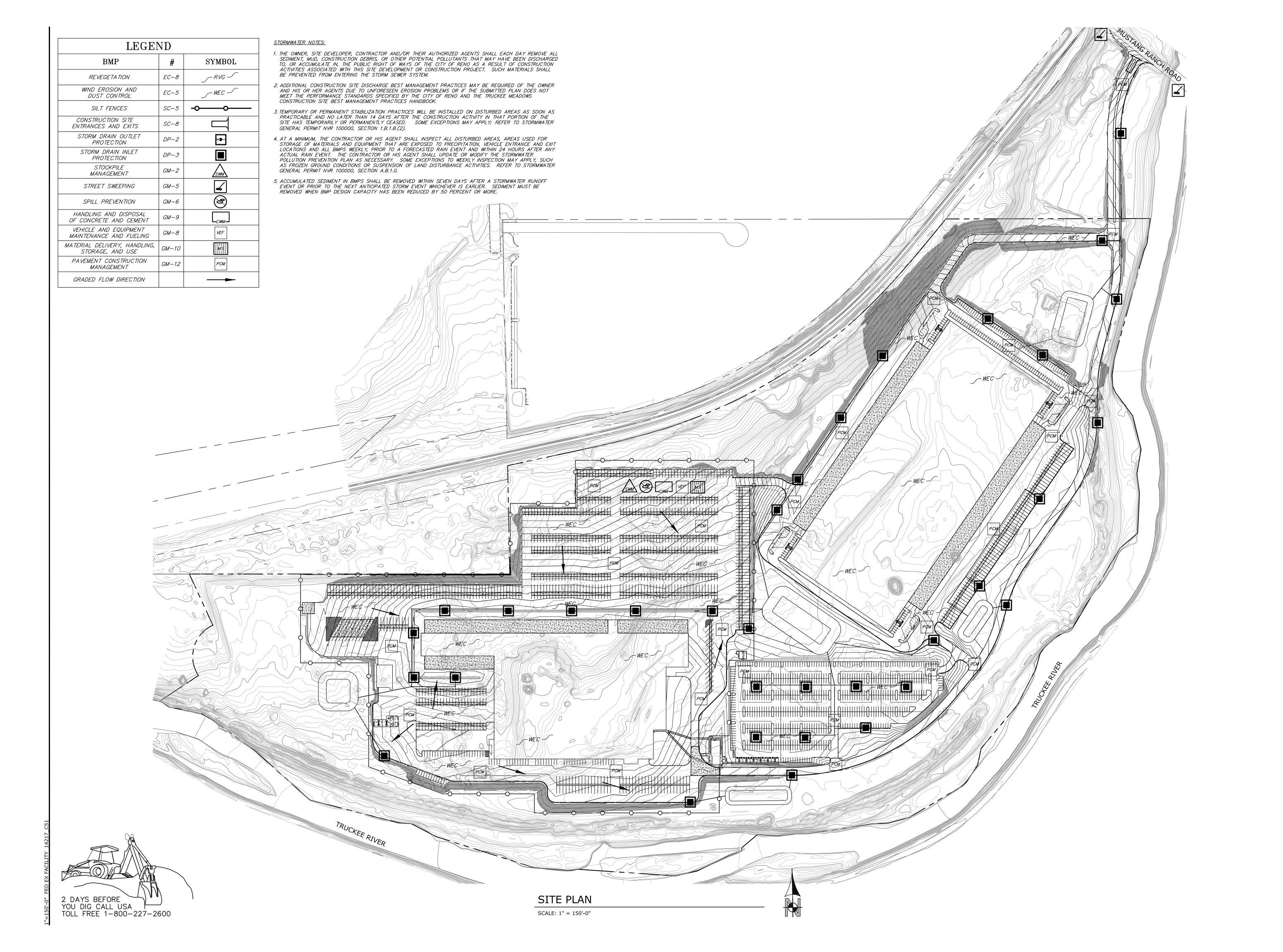
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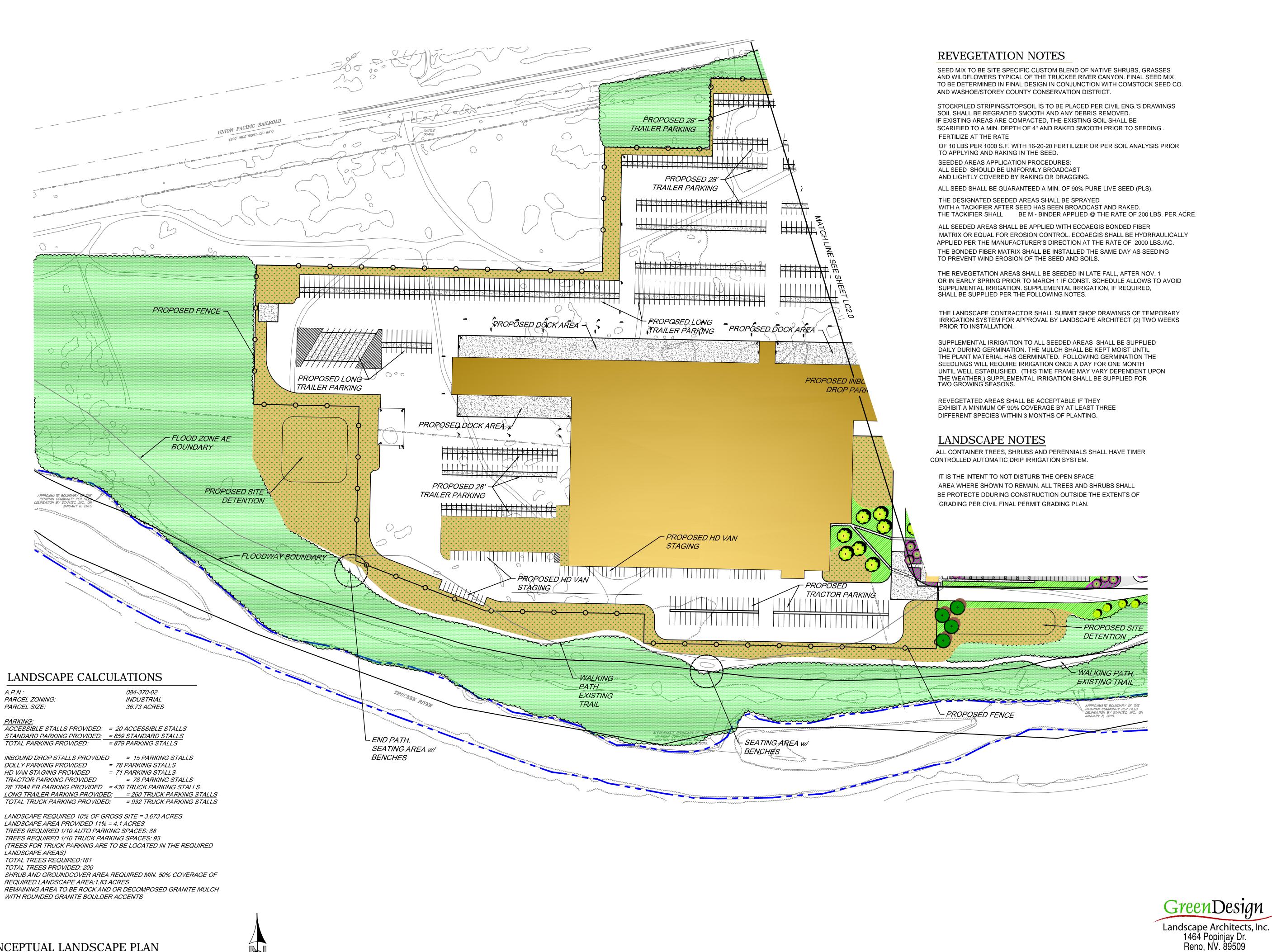
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CONCEPTUAL LANDSCAPE PLAN

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