Washoe County Development Application

Your entire application is a public record. If you have a concern about releasing personal information, please contact Planning and Building staff at 775.328.6100.

Project Information	S	Staff Assigned Case No.:			
Project Name: 947 Tahoe Condominium					
Description	•	oment of 40 new residentia um on an approximately tw			
Project Address: 941 and 947	Tahoe Boulevard (SR 2	28)			
Project Area (acres or square f	eet): 2 acres				
Project Location (with point of	reference to major cross	streets AND area locator):			
Corner of Taho	e Blvd and	Southwood Blv	d		
Assessor's Parcel No.(s):	Parcel Acreage:	Assessor's Parcel No.(s):	Parcel Acreage:		
132-231-09	1.389				
132-231-10	0.598				
Indicate any previous Wash SPW2-7-96; WDCA22-0		s associated with this applica	ition: Case No.(s).		
Applicant Ir	nformation (attach	additional sheets if neces	sary)		
Property Owner:		Professional Consultant:			
Name: PALCAP FFIF TAHOE 1, LLP		Name: NCE			
Address: 940 Southwood Blvd		Address: PO Box 1760			
Incline Village, NV	Zip: 89451	Zephyr Cove, NV	Zip: 89448		
Phone: 469.233.2260	Fax:	Phone: 775-588-2505	Fax:		
Email: cbutler@palominocap.c	om	Email:mlefrancois@ncenet.com			
Cell: 214.269.3404	Other:	Cell: 530-386-2772	Other:		
Contact Person: Chuck Butler		Contact Person: Mike Lefrance	ois		
Applicant/Developer:		Other Persons to be Contacted:			
Name: Same as Owner		Name: Feldman Thiel, LLP			
Address:		Address: PO Box 1309			
	Zip:	Zephyr Cove, NV	Zip: 89448		
Phone:	Fax:	Phone: 775-580-7431	Fax:		
Email:		Email: kara@fmttahoe.com			
Cell:	Other:	Cell: 530-545-3522	Other:		
Contact Person:		Contact Person: Kara Thiel			
	For Office	e Use Only			
Date Received:	Initial:	Planning Area:			
County Commission District:		Master Plan Designation(s):			
CAB(s):		Regulatory Zoning(s):			

Tentative Subdivision Map Application Supplemental Information

(All required information may be separately attached)

1. What is the location (address or distance and direction from nearest intersection)?

941 AND 947 TAHOE BLVD

2. What is the subdivision name (proposed name must not duplicate the name of any existing subdivision)?

947 TAHOE CONDOMINIUM

3. Density and lot design:

a. Acreage of project site	1.99 Acres
b. Total number of lots	1 lot / 41 condominium units
c. Dwelling units per acre	20 units/acre
d. Minimum and maximum area of proposed lots	condominium unit size: 925 sf min 4,425 sf max
e. Minimum width of proposed lots	n/a
f. Average lot size	n/a

4. What utility company or organization will provide services to the development:

a. Sewer Service	IVGID
b. Electrical Service	NV ENERGY
c. Telephone Service	AT&T
d. LPG or Natural Gas Service	SOUTHWEST GAS
e. Solid Waste Disposal Service	IVGID
f. Cable Television Service	SPECTRUM
g. Water Service	IVGID

- 5. For common open space subdivisions (Article 408), please answer the following:
 - a. Acreage of common open space:



b. What development constraints are within the development and how many acres are designated slope, wetlands, faults, springs, and/or ridgelines:

NONE

c. Range of lot sizes (include minimum and maximum lot size):

n/a

d. Proposed yard setbacks if different from standard:

N/A

e. Justification for setback reduction or increase, if requested:

N/A

f. Identify all proposed non-residential uses:

N/A

g. Improvements proposed for the common open space:

lawn activity areas, spa, grills, and seating areas

h. Describe or show on the tentative map any public or private trail systems within common open space of the development:

N/A

i. Describe the connectivity of the proposed trail system with existing trails or open space adjacent to or near the property:

N/A

j. If there are ridgelines on the property, how are they protected from development?

N/A

k. Will fencing be allowed on lot lines or restricted? If so, how?

N/A

I. Identify the party responsible for maintenance of the common open space:

Homeowner's Association

6. Is the project adjacent to public lands or impacted by "Presumed Public Roads" as shown on the adopted April 27, 1999 Presumed Public Roads (see Washoe County Engineering website at <u>http://www.washoecounty.us/pubworks/engineering.htm</u>). If so, how is access to those features provided?



7. Is the parcel within the Truckee Meadows Service Area?

 8. Is the parcel within the Cooperative Planning Area as defined by the Regional Plan?

Yes No If yes, within what city? INCLINE VILLAGE

9. Has an archeological survey been reviewed and approved by SHPO on the property? If yes, what were the findings?

10. Indicate the type and quantity of water rights the application has or proposes to have available:

a. Permit #	-	acre-feet per year
b. Certificate #	-	acre-feet per year
¤ c. Surface Claim #	-	acre-feet per year
d. Other #	-	acre-feet per year

a. Title of those rights (as filed with the State Engineer in the Division of Water Resources of the Department of Conservation and Natural Resources):

Credit will be given for water rights associated with the previous restaurant and service station uses. The balance, if any, required to serve the project will be purchased from IVGID.

11. Describe the aspects of the tentative subdivision that contribute to energy conservation:

Triple paned glass in many windows, high efficiency radiant heating, electrical vehicle charging stations, bike room

12. Is the subject property in an area identified by Planning and Building as potentially containing rare or endangered plants and/or animals, critical breeding habitat, migration routes or winter range? If so, please list the species and describe what mitigation measures will be taken to prevent adverse impacts to the species:

No

13. If private roads are proposed, will the community be gated? If so, is a public trail system easement provided through the subdivision?

N/A

14. Are there any applicable policies of the adopted area plan in which the project is located that require compliance? If so, which policies and how does the project comply?

Policies T2-2 through T2-5: The project incorporates on-site bicycle storage and parking and the site is fronted by existing pedestrian and bike paths and is close to parks, schools, a golf course and other services. Policies T3-1 and -2: Access on 28 is for emergencies only. Policy T4-1: The site driveway intersections and SR 28/Village operate at acceptable LOS with the project. LU2-9: The development is a single-family dwelling airspace condominium and commercial space mixed-use project.

15. Are there any applicable area plan modifiers in the Development Code in which the project is located that require compliance? If so, which modifiers and how does the project comply?

Section 110.220.35, .145 and .150 apply to the Incline Village Commercial Regulatory Zone in which the project is located. The project complies with the applicable height, density, permissible use and land coverage standards.

16. Will the project be completed in one phase or is phasing planned? If so, please provide that phasing plan:

One phase

17. Is the project subject to Article 424, Hillside Development? If yes, please address all requirements of the Hillside Ordinance in a separate set of attachments and maps.

Yes	🖬 No	If yes, include a separate set of attachments and maps.

18. Is the project subject to Article 418, Significant Hydrologic Resources? If yes, please address Special Review Considerations within Section 110.418.30 in a separate attachment.

Yes	🖬 No	If yes, include separate attachments.
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Grading

Please complete the following additional questions if the project anticipates grading that involves: (1) Disturbed area exceeding twenty-five thousand (25,000) square feet not covered by streets, buildings and landscaping; (2) More than one thousand (1,000) cubic yards of earth to be imported and placed as fill in a special flood hazard area; (3) More than five thousand (5,000) cubic yards of earth to be imported and placed as fill; (4) More than one thousand (1,000) cubic yards to be excavated, whether or not the earth will be exported from the property; or (5) If a permanent earthen structure will be established over four and one-half (4.5) feet high:

19. How many cubic yards of material are you proposing to excavate on site?

19,098 CY excavation

20. How many cubic yards of material are you exporting or importing? If exporting of material is anticipated, where will the material be sent? If the disposal site is within unincorporated Washoe County, what measures will be taken for erosion control and revegetation at the site? If none, how are you balancing the work on-site?

18,325 export - out of Tahoe Basin

21. Can the disturbed area be seen from off-site? If yes, from which directions, and which properties or roadways? What measures will be taken to mitigate their impacts?

Visible from SR28. Disturbed areas to be landscaped or restored per TRPA.

22. What is the slope (Horizontal/Vertical) of the cut and fill areas proposed to be? What methods will be used to prevent erosion until the revegetation is established?

3:1 max slopes to be landscaped or restored per TRPA

23. Are you planning any berms and, if so, how tall is the berm at its highest? How will it be stabilized and/or revegetated?

No berms

24. Are retaining walls going to be required? If so, how high will the walls be, will there be multiple walls with intervening terracing, and what is the wall construction (i.e. rockery, concrete, timber, manufactured block)? How will the visual impacts be mitigated?

8.5' max high wall at driveway. Concrete proposed. Wall is below sight line from SR28.

25. Will the grading proposed require removal of any trees? If so, what species, how many, and of what size?

45 total trees to be removed. Summary on Sheet C2

26. What type of revegetation seed mix are you planning to use and how many pounds per acre do you intend to broadcast? Will you use mulch and, if so, what type?

Mulch of all disturbed areas as required of TRPA; Native pine needles or wood chips.

27. How are you providing temporary irrigation to the disturbed area?

irrigation in right-of-way areas not proposed

28. Have you reviewed the revegetation plan with the Washoe Storey Conservation District? If yes, have you incorporated their suggestions?

No

Tahoe Basin

Please complete the following questions if the project is within the Tahoe Basin:

29. Who is the Tahoe Regional Planning Agency (TRPA) project planner and what is his/her TRPA extension?

Bridget Cornell, bcornell@trpa.gov, 775.589.5218

30. Is the project within a Community Plan (CP) area? AREA PLAN:

□ Yes □ Nolf yes, which CP? INCLINE VILLAGE COMMERCIAL REG ZONE SPECIAL AREA 1

31. State how you are addressing the goals and policies of the Community Plan for each of the following sections:

a. Land Use:

Multiple-family dwellings are permissible as an allowed use in the IVCRZ SA 1 at a minimum and maximum density of 15 and 25 units/acre, respectively. For the two-acre site, the minimum and maximum densities are 30 units and 50 units, respectively. At 40 units, the project complies with the applicable density standards. The MFD-commercial mixed-use project can be subdivided into 40 airspace condos and a commercial condo since single-family dwelling condos are an allowed use in SA 1 when part of a mixed-use project.

b. Transportation:

The project incorporates on-site bicycle storage and parking and the site is fronted by existing pedestrian and bike paths. This will reduce reliance on the automobile.

c. Conservation:

The project is located in high capability land. Existing land coverage banked onsite will be used to support the project. Additional land coverage, in the form of existing coverage, will be transferred from elsewhere in the Region to the project, which is located in a Town Center. Air quality impacts will be mitigated through payment of the applicable fee. Scenic impacts will be mitigated through the use of earth tone colors, natural materials and landscape screening

d. Recreation:

The project incorporates on-site bicycle storage and parking and the site is fronted by existing pedestrian and bike paths and is close to parks, schools, a golf course and other services



e. Public Services:

Significant growth is not anticipated under this area plan. As a result, the plan envisions maintaining existing service levels. No major facility expansions or relocations are envisioned.

13

- 32. Identify where the development rights for the proposed project will come from:
- 33. Will this project remove or replace existing housing?

-		
Yes	🖬 No	If yes, how many units?

- 34. How many residential allocations will the developer request from Washoe County? No residential allocations will be requested. However, an allocation of 1,800 sf of CFA will be requested from the Area Plan's development rights pool for conversion to 6 RUUs.
- 35. Describe how the landscape plans conform to the Incline Village General Improvement District landscaping requirements:

Limited turf area per ordinance; native/adaptive species

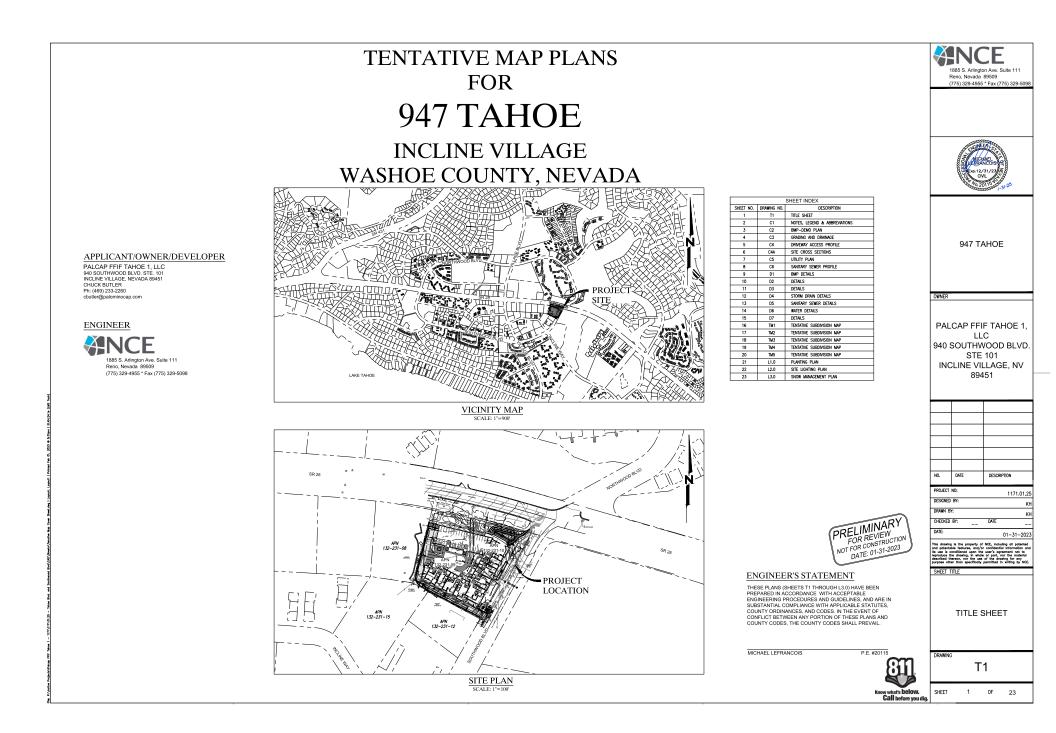
Request to Reserve New Street Name(s) The Applicant is responsible for all sign costs.							
		A	pplicant	Information			
Name:	ame: PALCAP FFIF TAHOE1, LLS						
Address:	940 Sol	ithwood Blvd					
	941 AND 947 TAHOE BLVD						
Phone :			I	-ax:			
	Priv	ate Citizen		Agency/Org	anization		
	(No more th			ne Requests	ch extra sheet if necessa	ary.)	
	NONE R	REQUESTED					
If final reco	rdation b	as not occurred	within on	a (1) vear it is	necessary to subm	nit a written	
					ation date of the c		
			Loc	ation			
Project Nan	ne: <u>947</u>	Tahoe Condomini	um				
	F	Reno	Spa	arks	Washoe Co	unty	
Parcel Num			_				
		Subdivision	Pai	rcelization	Private Stre	et	
	Ple	ase attach map	s, petition	s and suppler	nentary informatio	n.	
Approved:				Date:			
	Regional Street Naming Coordinator Except where noted						
Denied:		pi where noted			Date:		
Defiled.	Region	al Street Namin	g Coordina	ator	Dute		
	Wa	ashoe County Phone ⁻ (775	1001 E. N Reno, NV	hic Informatio linth Street 89512-2845 5 - Fax: (775)			

Nine 47 Tahoe Public Outreach

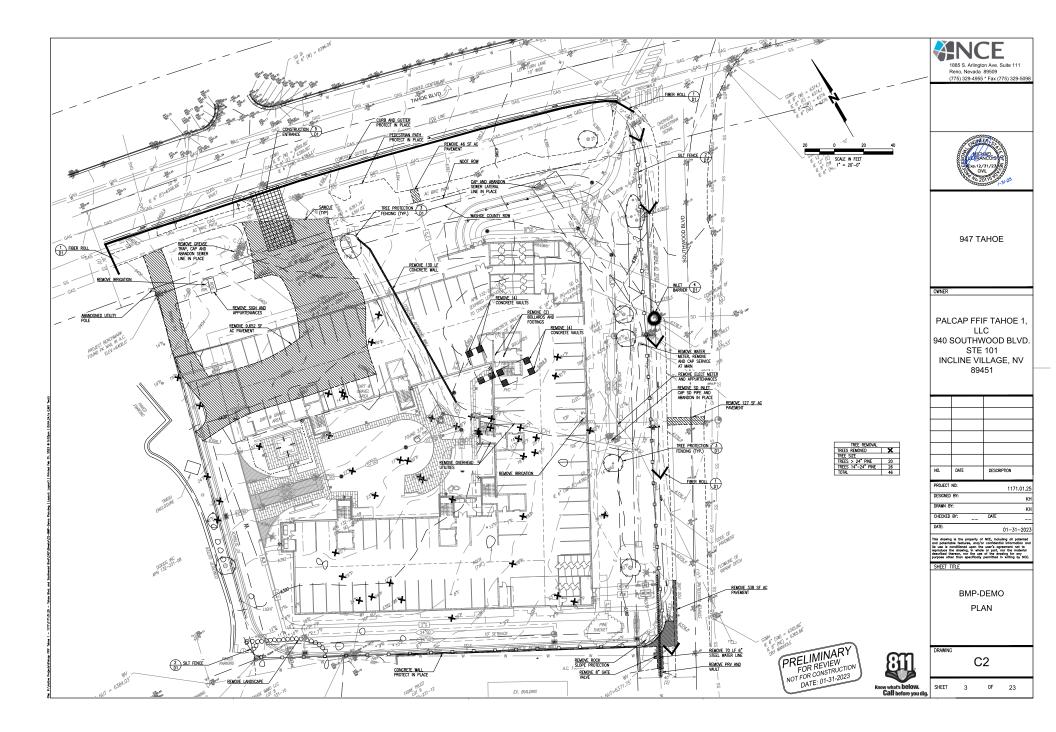
At least eight (8) public meetings have been held in the last year, three (3) more are scheduled in the next two months and the Planning Commission will hold a public hearing on the TSM in May 2023.

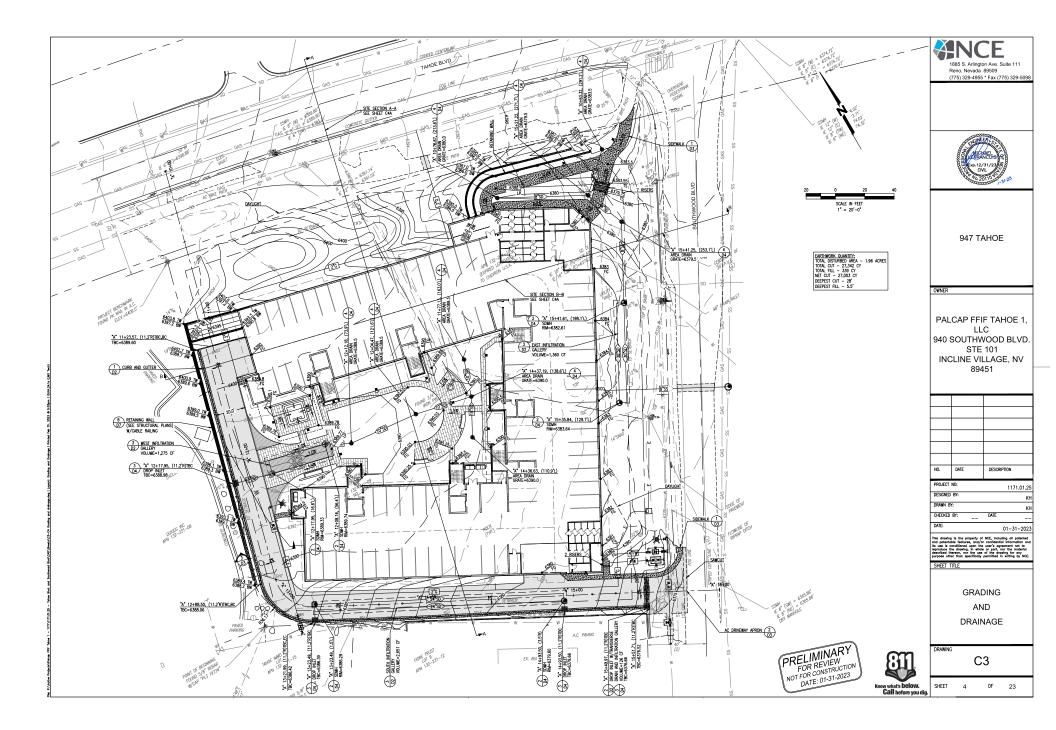
A neighborhood meeting was held on January 24, 2022, regarding the proposed Tentative Map. The TRPA Governing Board (GB) approved the Project on June 22, 2022, at a public meeting. Next, PAL CAP held a community workshop on August 22, 2022, on the Project and Amendment with more than 30 people in attendance. A public hearing on the Amendment was held at the Planning Commission (PC) on Nov. 1, 2022, and many of the comments received were on the Project. A public hearing was held at the Board of County Commissioners (BOCC) on December 13, 2022, for the first reading of the Amendment and, again, the Project was the subject of numerous public comments. TRPA made a presentation on the Amendment to the Incline Village / Crystal Bay CAB on January 3, 2023, with many people in attendance. A public hearing was held at the BOCC on January 17, 2023, for the second reading of the Amendment, which was unanimously approved. At the time of the BOCC's approval of the Amendment, more than 80 letters/emails had been submitted and dozens of people spoke during public comment about the Project. A public hearing was held on the Amendment at the February 22, 2023, TRPA Regional Plan Implementation Committee (RPIC) meeting with more than 70 public letters submitted, and several members of the public participated in the meeting. Finally, Randy Fleisher of PAL CAP has met individually with dozens of community members about the Project and reached out to Rotary Club members, business association members and non-profits groups.

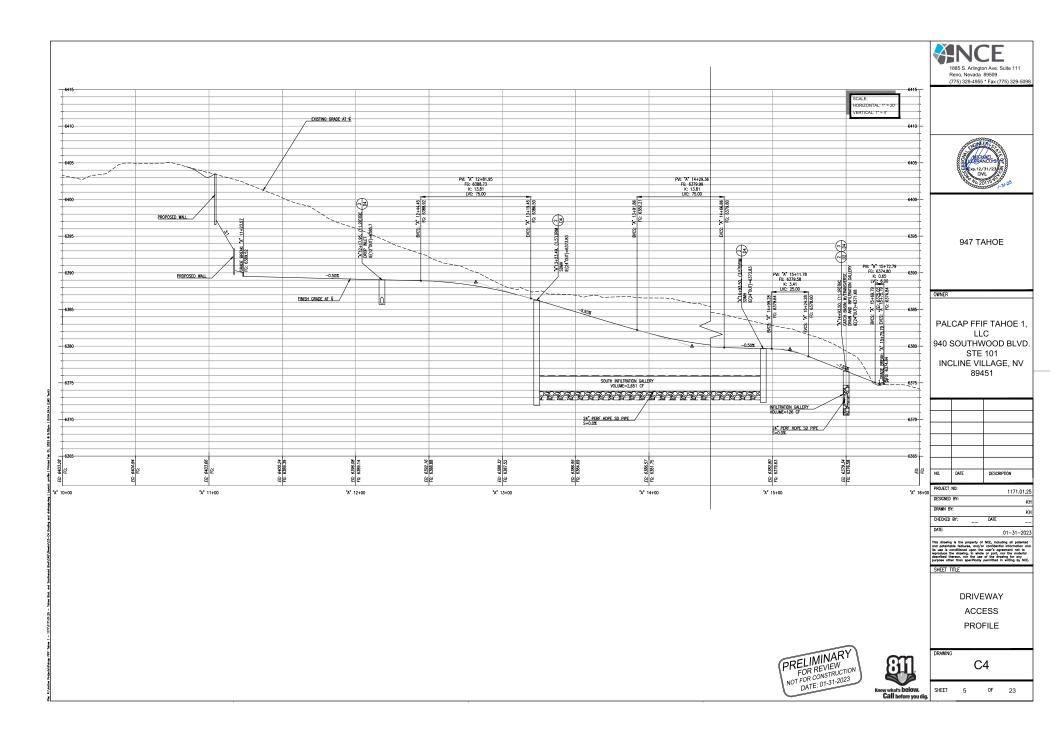
Future public hearings on the Amendment, which will undoubtedly garner public comments on the Project, will be held March 8, 2023, at the TRPA Advisory Planning Commission meeting, March 22, 2023, RPIC meeting and April 26, 2023, at the TRPA GB meeting. Finally, the public will have another opportunity to comment on the Project during the PC meeting on the Project's Tentative Subdivision Map.

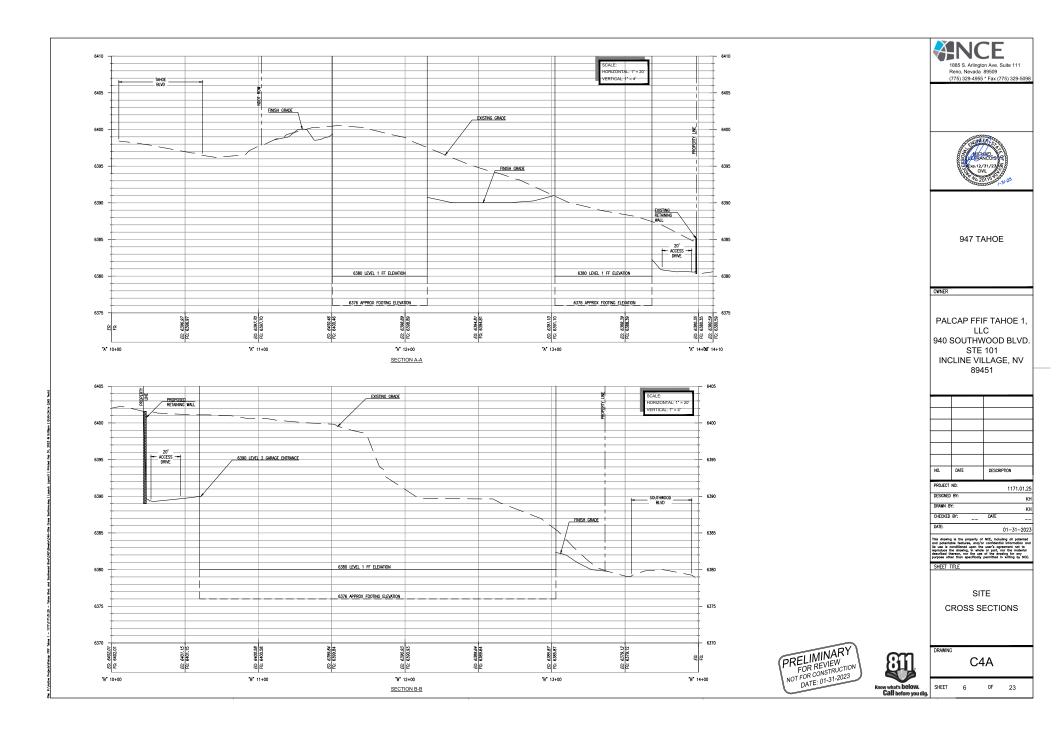


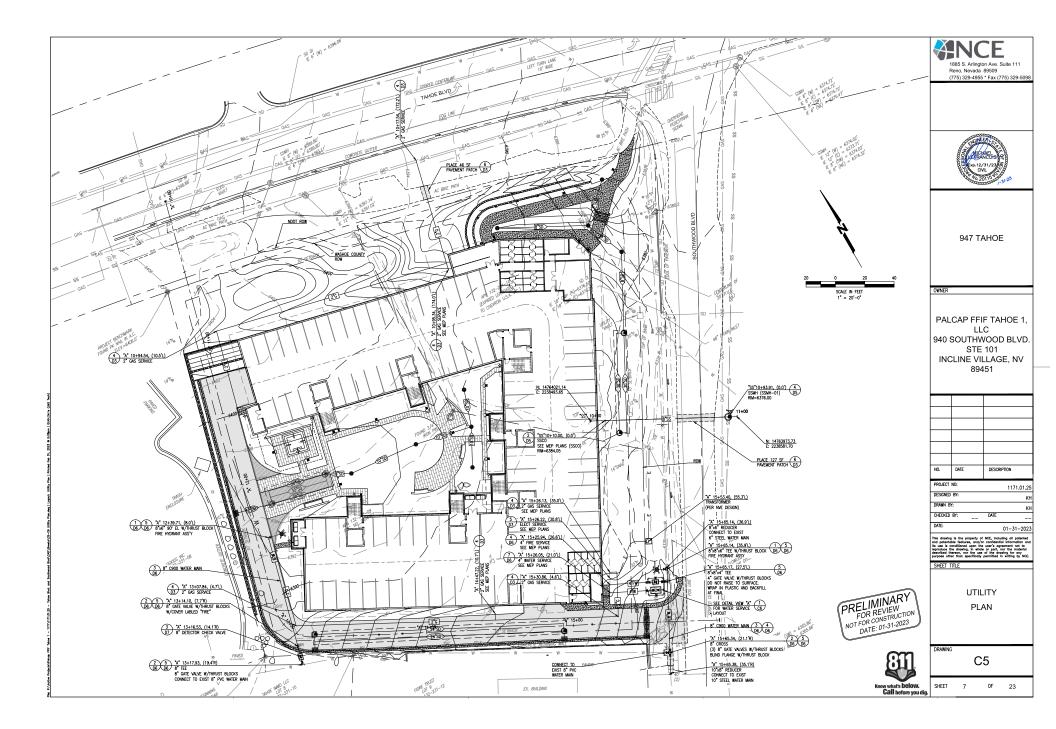
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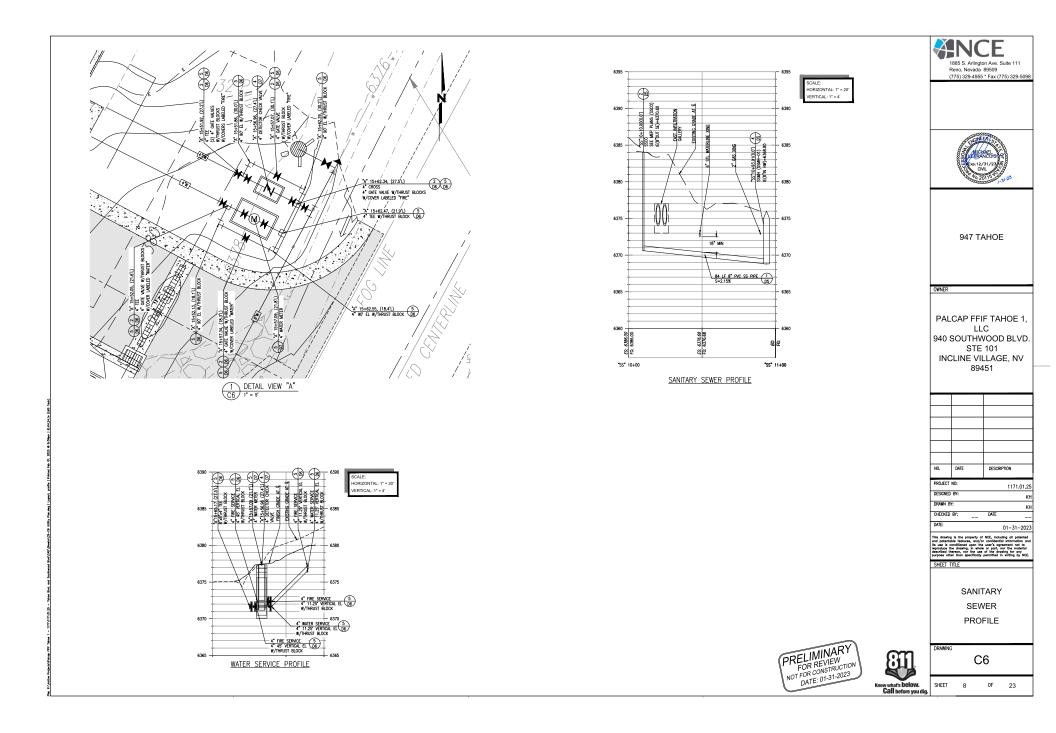


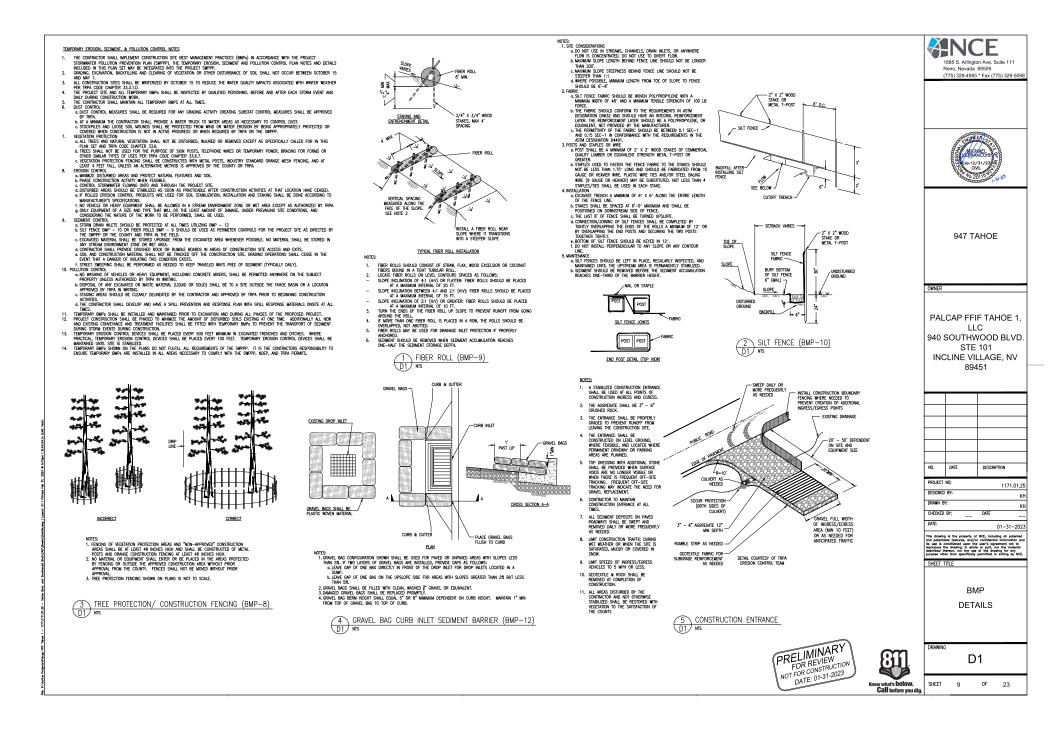


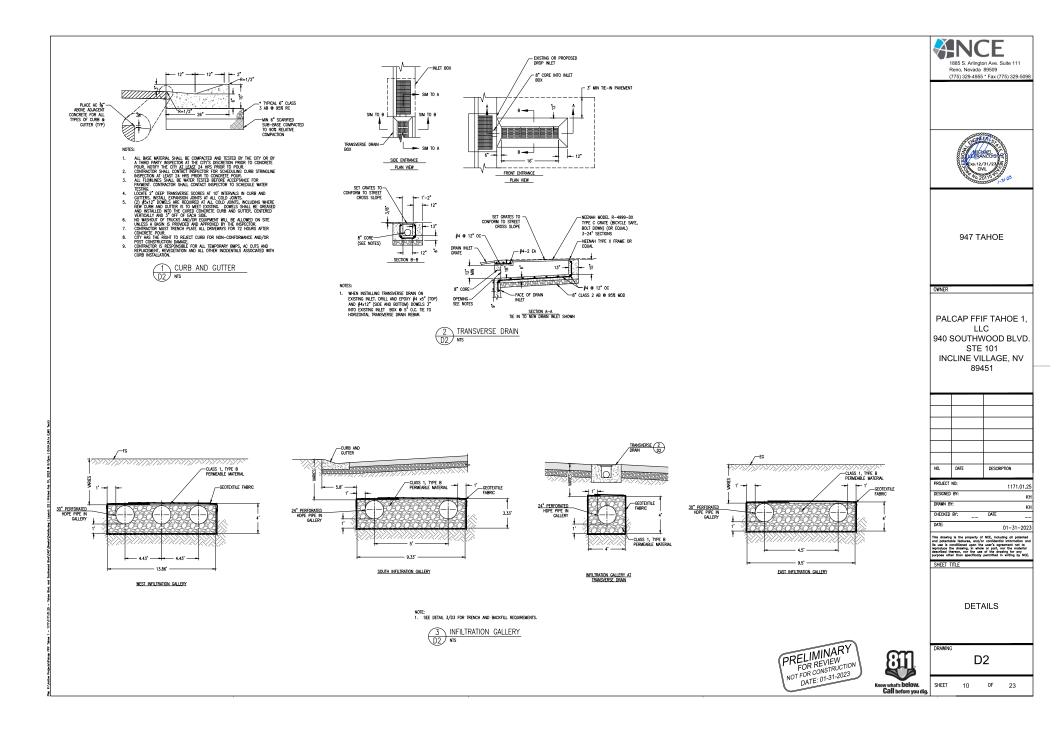


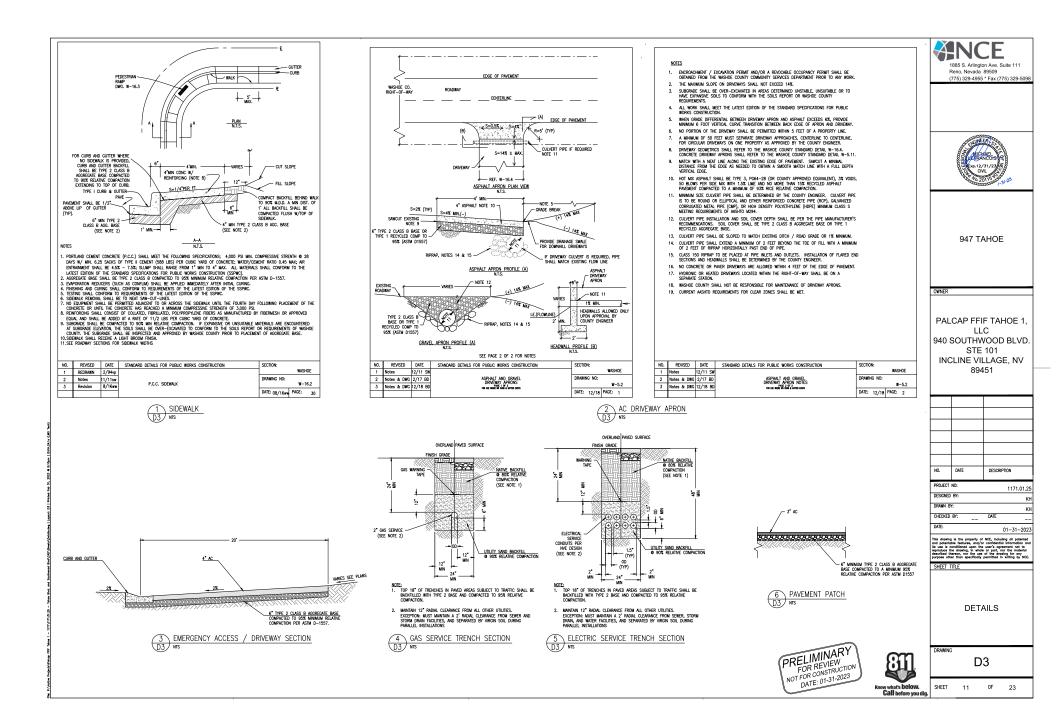


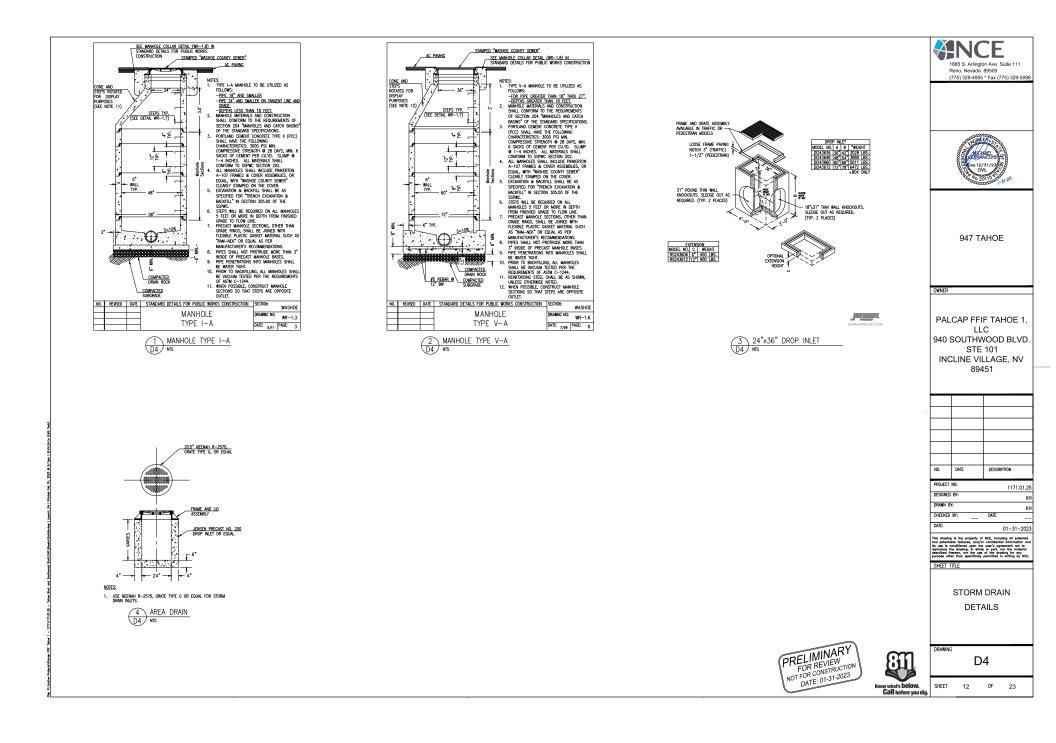


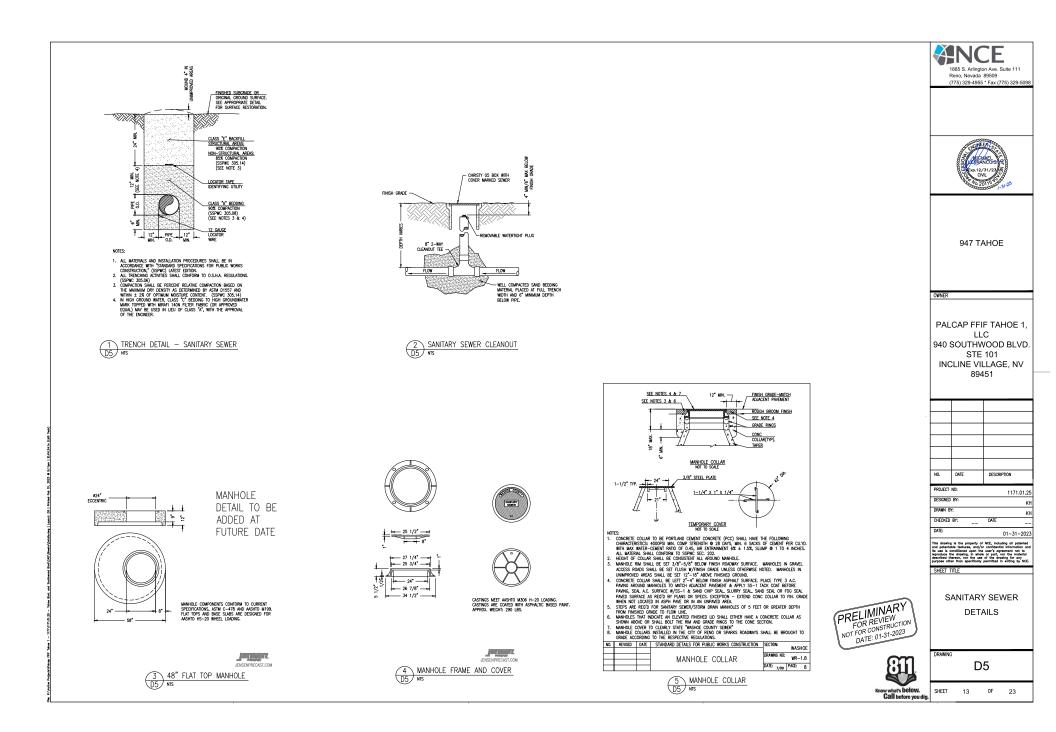


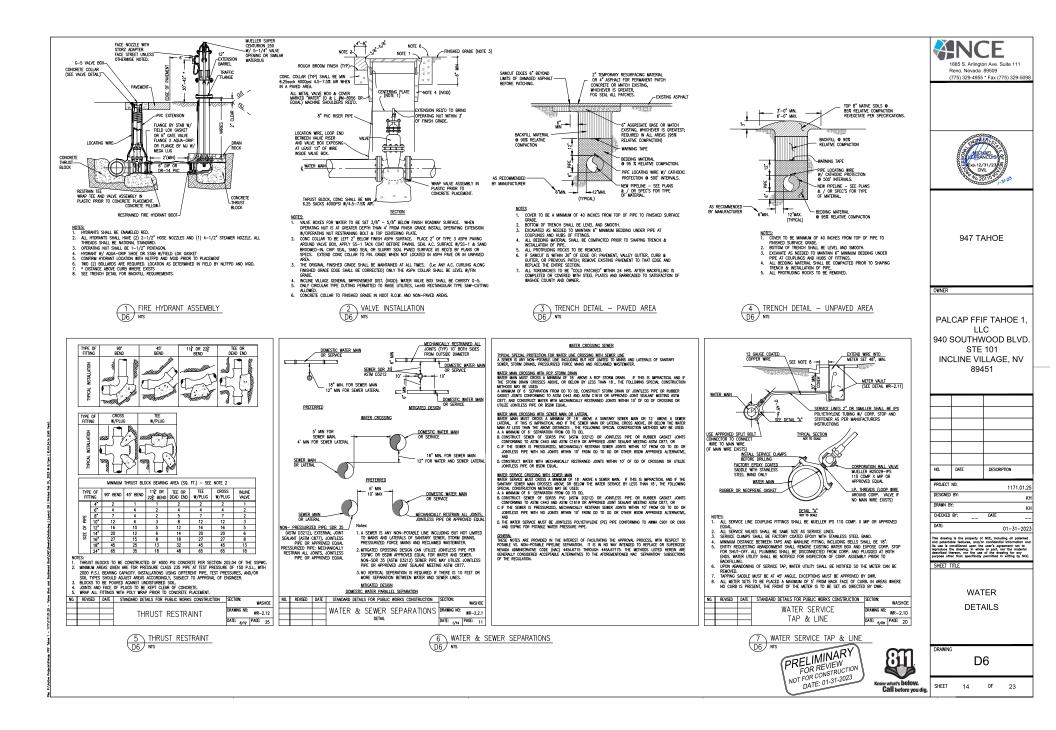


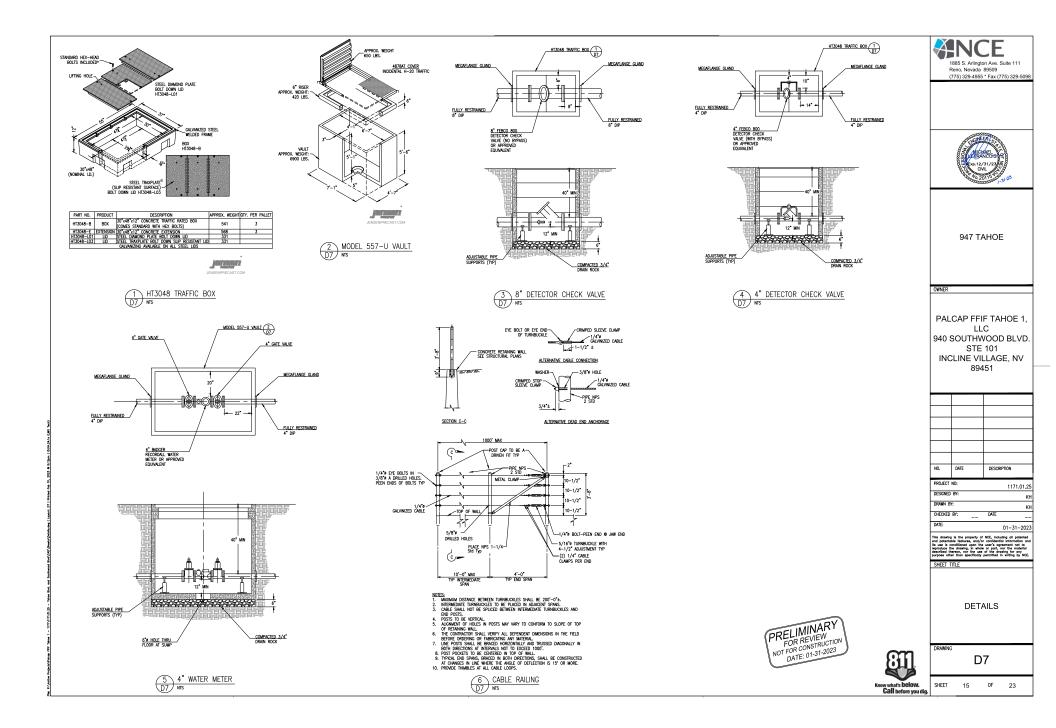


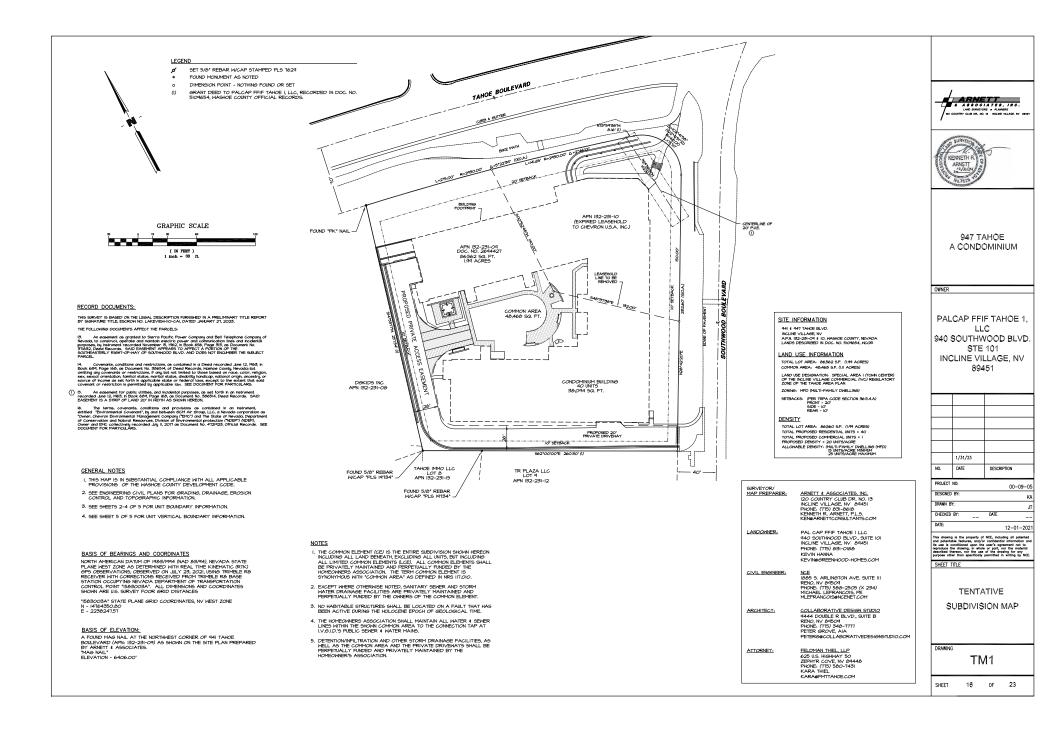


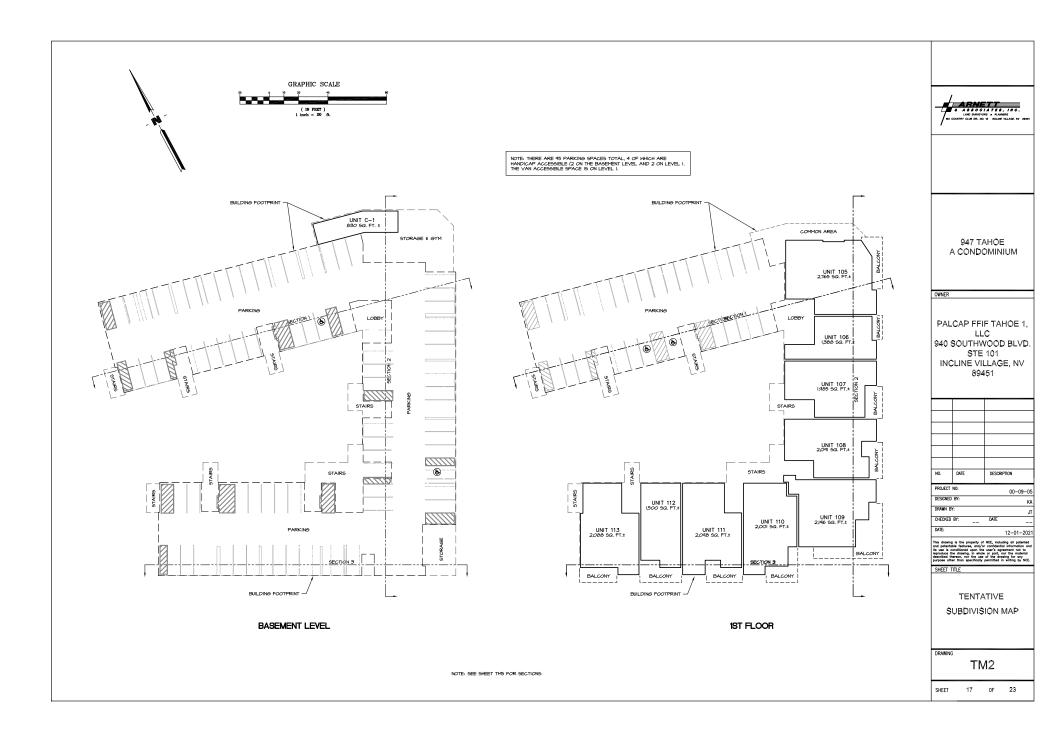


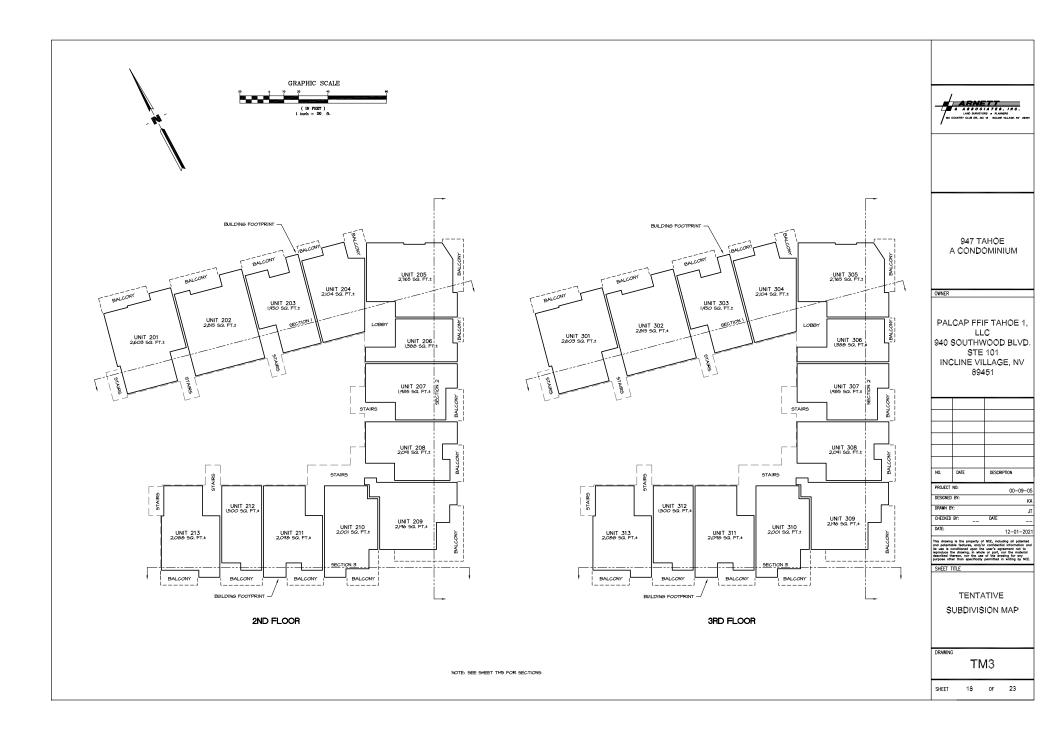


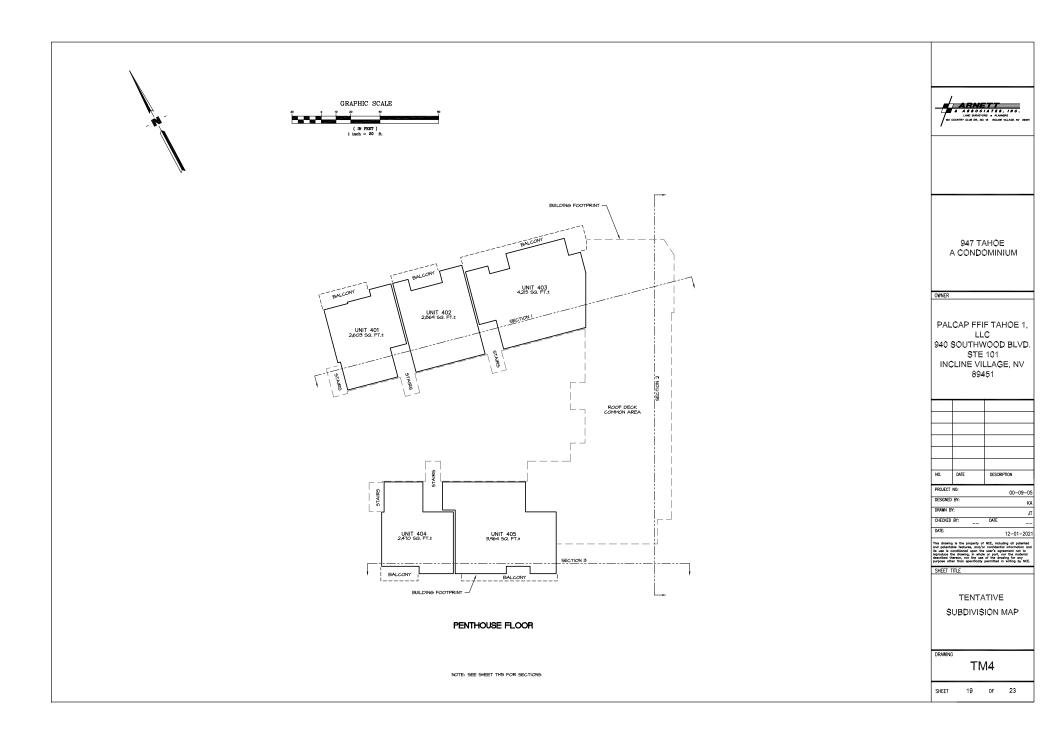




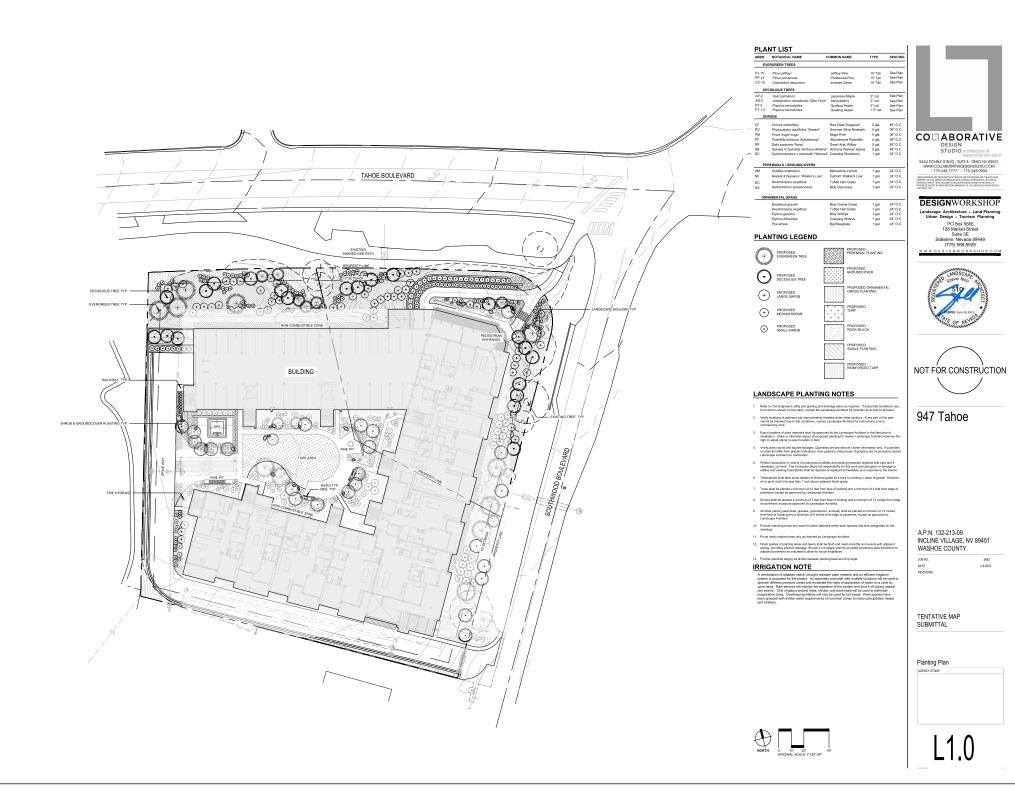


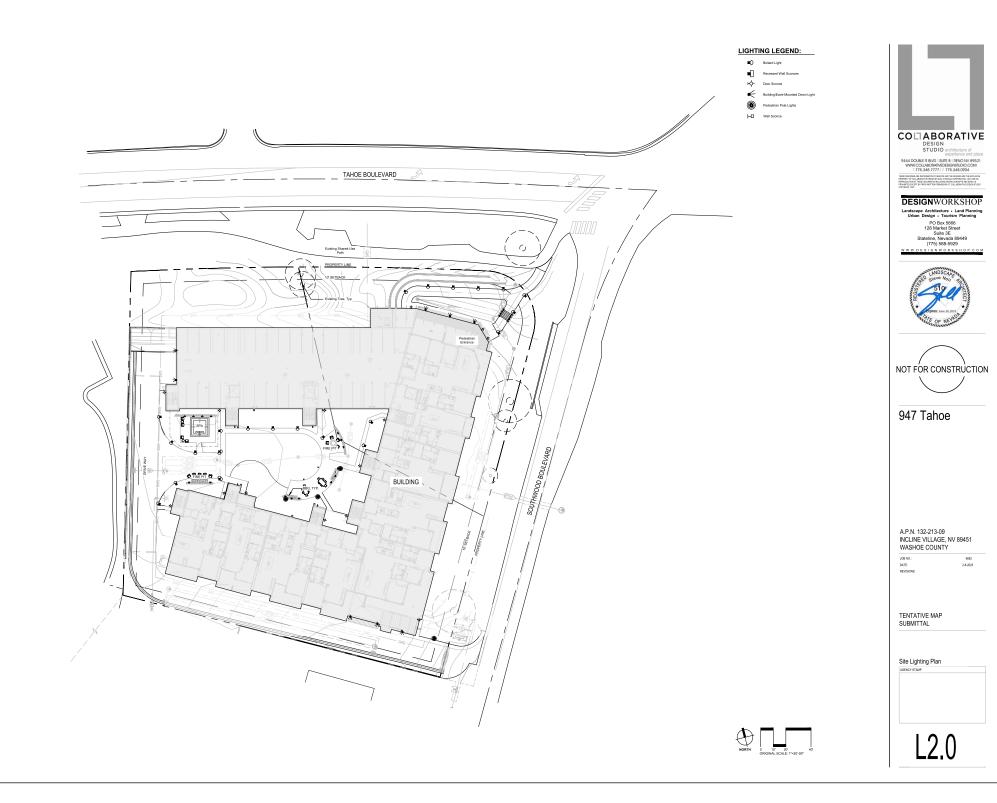




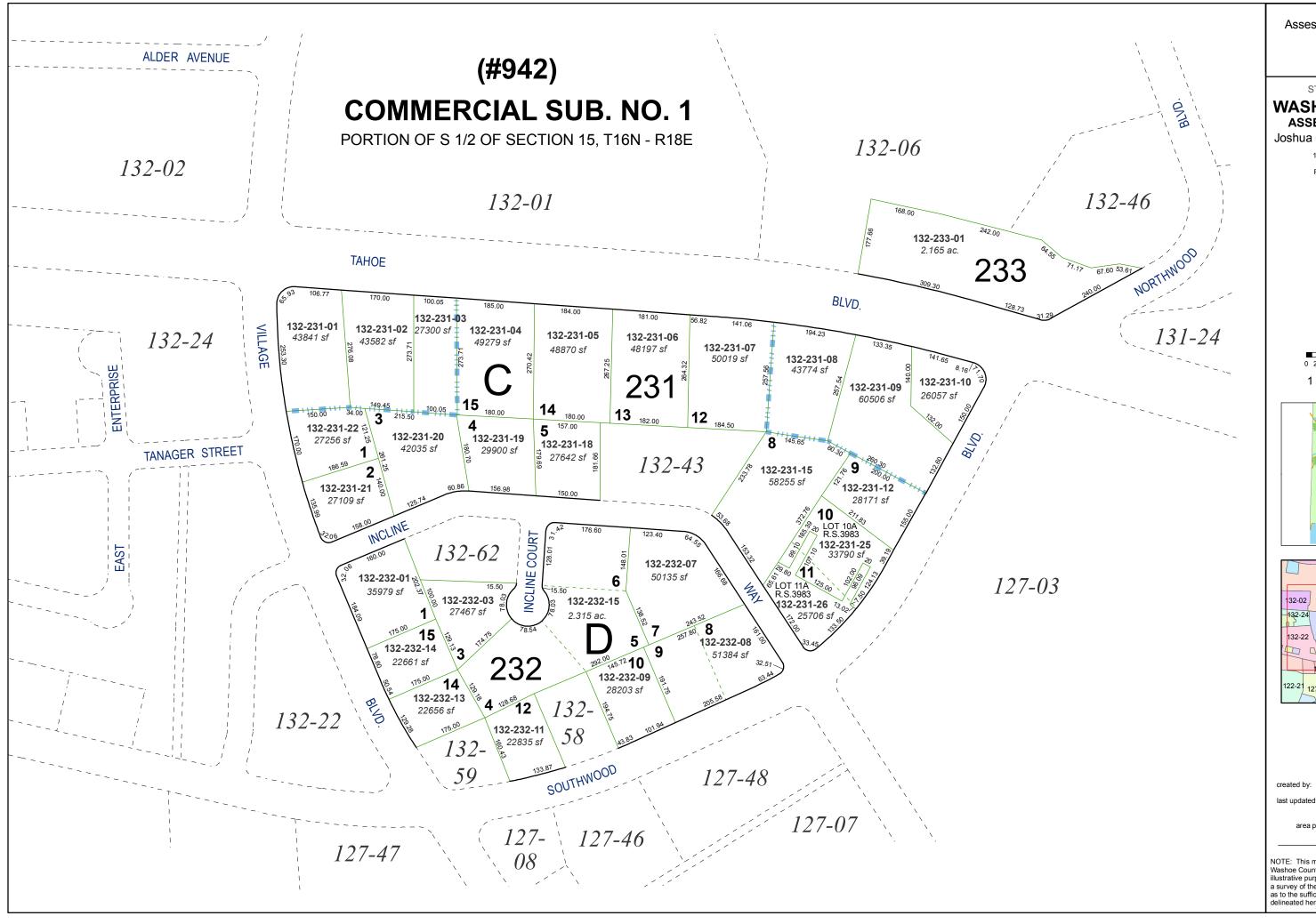












Assessor's Map Number

132-23

STATE OF NEVADA

WASHOE COUNTY **ASSESSOR'S OFFICE** Joshua G. Wilson, Assessor 1001 East Ninth Street Building D Reno, Nevada 89512 (775) 328-2231 100 150 0 25 50 200 1 inch = 200 feet \Box 132-23 DD 127-03 127-47 127-07 122-21 127-30 KSB 4/13/2009 last updated: CFB 07/30/2010 area previously shown on map(s)

NOTE: This map was prepared for the use of the Washoe County Assessor for assessment and illustrative purposes only. It does not represent a survey of the premises. No liability is assumed as to the sufficiency or accuracy of the data delineated hereon.

Consulting Civil Engineers P.O. Box 18449 Reno, Nevada 89511 PH (775) 853-9100 FAX (775) 853-9199

July 1, 2021 Project No. 21073.001

Mr. Kevin Hanna PAL CAP FIFF Tahoe I, LLC 940 Southwood Boulevard, Suite 101 Incline Village, Nevada 89451 Email: kevin@greenwood-homes.com

Subject: Geotechnical Assessment Southwood Condominiums 941 and 947 Tahoe Boulevard Incline Village, Washoe County, Nevada 89451 APN's: 132-231-09 and 132-231-10

Dear Mr. Hanna:

This report presents the results of Reno Tahoe Geo Associates' (RTGA's) geotechnical assessment for a proposed 5-story condominium building to be located on two adjoining parcels at 941 Tahoe Boulevard and 947 Tahoe Boulevard in Incline Village, Washoe County, Nevada (APN's: 132-231-09 and 132-231-10). This report provides the information required by Washoe County. The project location is shown on Plate 1.

A limited subsurface field investigation was included in this geotechnical assessment. Therefore, it is important that RTGA be involved during grading and construction to confirm that the site conditions are as anticipated and to make any necessary revisions to our recommendations.

PROJECT DESCRIPTION

The proposed project site is composed of two adjoining irregularly shaped parcels totaling 1.987 acres located at 941 Tahoe Boulevard and 947 Tahoe Boulevard (corner parcel), Incline Village, Washoe County, Nevada. The parcels are bounded to the north by Tahoe Boulevard, to the east by Southwood Boulevard, and to the south and west by developed privately owned parcels. Access is by existing paved and gravel private driveways from Tahoe Boulevard and Southwood Boulevard. A site plan

941 and 947 Tahoe Boulevard - Geotechnical Assessment July 1, 2021 Project No. 21073.001 Page 2 of 13

including the existing property lines and the proposed condominium building footprint is presented on Plate 1.

The two parcels are currently undeveloped, unoccupied, and without above ground structures. The corner lot, 947 Tahoe Boulevard, was formerly occupied by a Chevron gas station. 941 Tahoe Boulevard is located on the south and west sides of 947 Tahoe Boulevard and formerly had a building used as a restaurant located in the north-central portion of the parcel near Tahoe Boulevard. The southern portion of this parcel does not appear to have undergone any historic development. An approximately 4-foot high retaining wall located on the west edge of the corner lot along its north-south property line. The formerly developed portions of each parcel are approximately level and the levelled portion of 947 Tahoe Boulevard is approximately 8 feet lower than the levelled portion of the western parcel. From Tahoe Boulevard, the combined parcels slope from approximately 6,406 feet at the northwest corner to 6,379 feet at the southeast corner where they meet Southwood Boulevard, resulting in an overall site slope of approximately 7 percent to the southeast.

We understand that a new, 5-story condominium complex with covered parking will be constructed with anticipated cuts of up to 20 feet and fills on the order of 8 feet or less. E-mail correspondence indicates the complex will be supported on concrete slab with a concrete and steel structure. Structural loads were not available at the time of this report and were assumed for the purposes of this proposal. Estimated vertical structural loads are not expected to exceed 50 kips at isolated columns and 2 kips to 4 kips per linear foot along continuous wall foundations for long-term loading conditions. Once plans are made available, we may need to modify our recommendations if the actual construction scope differs.

REFERENCES

The following information was provided to RTGA in the course of this investigation and serves as the basis of our understanding of the project type and scope.

• Topographic Survey, Arnett & Associates, Inc., 941 & 7 947 Tahoe Boulevard, Washoe County, Nevada, October 30, 2020.

 ALTA/NSPS Land Title Survey, 941 & 7 947 Tahoe Boulevard, Washoe County, Nevada, October 30, 2020.

The following published and unpublished references were also reviewed during preparation of this report.

- ASCE, 2019, ASCE 7 Hazard Tool, accessed June 2021;
- Natural Resources Conservation Service (NRCS) *Web Soil Survey in Google Earth*, accessed June, 2021;
- Washoe County Real Property Assessment Data, Washoe County website accessed June 2021;
- Saucedo, George J. 2005, *Geologic Map of the Lake Tahoe Basin, California and Nevada*, California Geological Survey;
- United State Geologic Survey (USGS), Quaternary Fault and Fold Database of the United States, (<u>http://earthquake.usgs.gov/hazards/qfaults/)</u>, accessed August 2020.

We also reviewed nearby projects and our previous experience in the project area in developing these recommendations.

FIELD EXPLORATION

Our selection of field exploration locations was based on the anticipated project layout and site access. The subsurface exploration consisted of three test pits and a shear-wave velocity survey, which were located in the field by visual sighting and/or measuring from existing features at the site. The exploration locations shown on Plate 1 should be considered accurate only to the degree implied by the methods used.

Refraction Microtremor Survey (ReMi)

A Refraction Microtremor (ReMi) geophysical array was utilized to obtain shear-wave velocity measurements to determine the Seismic Design Category and estimate the depth to competent bedrock. ReMi provides a means to obtain a basic subsurface profile in an essentially continuous profile without physical investigations across the explored location. The results of the ReMi survey are presented both as a one-dimensional vertical profile and a two-dimensional transect on Plate 2.

941 and 947 Tahoe Boulevard - Geotechnical Assessment July 1, 2021 Project No. 21073.001 Page 4 of 13

Test Pit Excavation

Three test pits were excavated using a Link-Belt 145 X 2 excavator. Our engineer visually classified soils encountered in the test pit according to the Unified Soil Classification System (USCS) and obtained bulk samples for further identification and laboratory testing. Soil conditions encountered are presented on the test pit logs on Plates 3 through 5. A description of the USCS used to identify the site soils and a test pit log legend are presented on Plate 6.

After the test pits were completed, they were backfilled with excavated soil using the equipment on site. Backfill was loosely placed and <u>not</u> compacted to the requirements typically specified for engineered fill. Structures, slabs supported on grade, or pavements located over these areas may experience excessive settlement. Removal and re-compaction of test pit backfill may be required prior to construction of improvements over this area.

LABORATORY TESTING

Laboratory tests were performed on selected samples to aid in soil classification and to evaluate physical properties of the soils, which may affect the geotechnical aspects of project design and construction. Gradation analysis and plasticity index (Atterberg Limits) was performed for a sample of site soils. Laboratory test results can be found on the test pit logs (Plates 3 through 5) and on Plates 7 and 8 at the end of this report. In addition, one soil sample of sandy lean clay collected from 12 feet depth in TP-01 was submitted for soil corrosivity analysis. Results of laboratory testing for this sample will be reported under separate cover when they are received.

SOIL AND GEOLOGIC CONDITIONS

According to Saucedo et al. (2005), the site is underlain by unnamed gravels, sand, and alluvium of Pliocene and/or Pleistocene age. Based on published information by NRCS and site observation, the native soils have been categorized as Inville gravelly coarse sandy loam, 2 to 9 percent slopes, stony, and within the hydrologic soil group A. The soil is well drained, with a saturated permeability of 2 to 6 inches per hour. According to Saucedo et al. (2005), the site is underlain by undivided glacial outwash deposits of Holocene or Pleistocene age.

Based on test pit excavations, laboratory analysis of soil samples, and the seismic survey conducted at the site, the subsurface conditions consist of greater than 15 feet thickness of silty gravel with sand,

Reno Tahoe Geo Associates, Inc.

941 and 947 Tahoe Boulevard - Geotechnical Assessment July 1, 2021 Project No. 21073.001 Page 5 of 13

cobbles, and boulders, over highly-weathered bedrock. Sandy lean clay was logged between 11 and 13 feet depth in test pit TP-1. Clayey sand with gravel was encountered below 13 feet in test pit TP-1.

The upper portion of bedrock, if encountered, may consist of intermixed weathered and permeable zones with harder boulder or zones where jointing is widely spaced. The bedrock typically transmits infiltrated water vertically to joint systems to sills or geologic contacts at depth, and rarely have springs or surface runoff. Boulders and bedrock may exhibit variations in density and hardness within the planned excavation.

The weighted average soil shear-wave velocity measured in the upper 100 feet of the soil horizon is 1,385 feet per second (fps) based on the ReMi measurement. Based on the shear-wave velocity profile, the soil at the ground surface is dense (material shear-wave velocities of about 800 fps to 1,000 fps). The ReMi data suggests that soft to hard rock (material greater than 1,200 fps to 2,800 fps shear-wave velocity) is present at approximately 16 to 26 feet in depth. Very hard excavation conditions may be present at shallow depths. The contractor should anticipate shallow large boulders and possibly bedrock in excavations.

No groundwater was observed in the test pits.

Seismicity and Faulting

Lake Tahoe lies within an area with moderate to high potential for strong ground shaking from large earthquakes (moment magnitude 7 or larger) in northern Nevada and California. Ground shaking can result in secondary seismic hazards such as liquefaction, seismic settlement, differential compaction, seismically induced slope instability, and rock falls. None of these hazards are present in this site due to dense soils, moderate slopes, and absence of tall rock outcrops or surface boulders. Due to the high potential for strong ground shaking from earthquakes, all structures should be designed for seismic loads in accordance with the most recently adopted International Building Code/International Residential Code.

Reno Tahoe Geo Associates, Inc.

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941 and 947 Tahoe Boulevard - Geotechnical Assessment July 1, 2021 Project No. 21073.001 Page 6 of 13

Saucedo et al. (2005) and the USGS Fault and Fold Database indicate the nearest fault is the Incline Village Fault approximately 7,400 feet west, (Saucedo, 2005). This fault zone is assigned as a Class A Fault of undifferentiated Quaternary Age. Based on review of the above-referenced published sources, no evidence was found that would indicate the presence of active faults trending through the subject property. No portion of any active Holocene age faulting is known to cross the site at this time, nor has any direct evidence of on-site faulting been observed in the field during the subsurface exploration of this project. No additional fault studies or fault setback requirements are needed for the subject parcel.

RECOMMENDATIONS AND DISCUSSION

From a geotechnical engineering standpoint, the site may be developed as a condominium structure as planned. Based upon our review of the above-referenced material, we have developed the following conclusions. These conclusions may change if additional information becomes available or the design is changed. *Please note, it is recommended that the soil and rock conditions presented in this report be verified during construction by the project geotechnical engineer.*

- The presence of shallow boulders is expected to be a significant constraint which will result in additional costs and difficulties during construction. No other soil or groundwater constraints were observed which will preclude the development as planned.
- Soils are a loose to medium dense silty sand with varying gravel, cobble, and boulder content. Boulders greater than 6 feet diameter were encountered in test pit TP-1 and smaller boulders were found to be common in the subsurface across the site. The contractor should anticipate boulders during excavation of the planned subgrade parking area, footings, and trenches.
- In most cases, native soils, if screened to <6 inches, are suitable for reuse as structural fill under structural areas or floor slabs. This excludes clayey soils such as those found below 11 feet depth in TP-1. Native soil is suitable for subgrade below footings or slabs if in a relatively undisturbed state. The Contractor may choose to use onsite material in structural areas but should be made aware that these soils may prove difficult to moisture condition and compact. It will be far easier to backfill narrow excavations, such as between building walls and excavations, with drain rock, aggregate base, or other readily specified compactable materials.

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- Imported structural fill, if required, should consist of granular material nearly free of organic debris, with a liquid limit of less than 35, a plasticity index less than 12, 100 percent passing the 4-inch sieve, and less than 30 percent passing the No. 200 sieve. All imported fill materials should be approved by the project Soils Engineer prior to being transported to the site.
- Fill should be uniformly moisture conditioned to within 2 percent of optimum moisture content and placed in layers of 8 inches or less in loose thickness. Each lift should then be compacted with appropriate compaction equipment to achieve at least 90 percent relative compaction^{*}, unless specified otherwise. No fill material should be placed, spread, or rolled while it is frozen, thawing, or during unfavorable weather conditions.
- Fills with more than 30 percent of particles greater than ³/₄-inch diameter and composed of durable stone or rock fragments, including drain rock and, likely, native materials, are not applicable to conventional compaction testing and is considered "rock fill". These materials should be uniformly moisture conditioned to above optimum moisture content and placed in thin layers not exceeding one foot in loose thickness. They should be compacted with a minimum of five passes with a large sheepsfoot compactor, such as Caterpillar 825, a large excavator with a compaction wheel, or a minimum of five passes with hand held compaction equipment in trenches or other small excavations. Compaction shall continue until no further densification or change in volume is noted. Any fill material within this category should be placed only under continuous observation and approval of the soil engineer. It is also noted that other types and sizes of compaction equipment may require thinner lifts of material.
- The 2018 International Building Code or International Residential Code should be implemented for the project seismic design. A Site Class C, per the IBC, is applicable for site soils due to the proximity of bedrock to the surface. For design purposes, the seismic criteria in the following table should be implemented.

^{*} Wherever referenced in this report, relative compaction should be determined by comparing to the maximum density and optimum moisture content determination in accordance with ASTM D1557 Test Method for compaction curves.

SEISMIC DESIGN CRITERIA USING ASCE 7-16 Southwood Condominium Project, Incline Village, Nevada	1
Approximate Latitude of Site	39.24874
Approximate Longitude of Site	-119.947296
Spectral Response Acceleration at Short Period (0.2 second), S _s	1.805 g
Spectral Response Acceleration at 1-Second Period, S ₁	0.618 g
Site Class Selected for this Site	С
Site Coefficient, F _a	1.2
Site Coefficient, F _v	1.4
Site Spectral Response Acceleration at Short Period, S _{MS}	2.166 g
Site Spectral Response Acceleration at Long Period, S _{M1}	0.866 g
Design Spectral Acceleration Parameters, S _{DS}	1.44
Design Response Spectrum, S _{D1}	0.58
Peak Ground Acceleration (PGA)	0.77 g

- We recommend that all foundations be bottomed at a minimum depth of 24 inches below the existing ground surface. This depth will provide adequate foundation support and protect against shallow ground loosening due to frost heave.
- Foundations bottomed at least 2 feet below the final ground surface may be designed for an allowable bearing pressure of 3,000 psf, assuming a minimum footing width of 12 inches. Bearing capacity can be increased by 500 psf for each foot of increase in thickness up to 4,500 psf. Footings at greater than 10 feet depth can be designed for an allowable bearing pressure of 6,000 psf where they are on bedrock.
- The allowable bearing pressure may be increased by one-third for total loading conditions, including wind and seismic forces. For balanced backfill, the allowable bearing pressure is a net value; therefore, the weight of the foundation which extends below grade and the overlying backfill may be neglected when computing dead loads.
- Total settlement of an individual foundation will vary depending on the plan dimensions of the foundation and the actual load supported. Based upon anticipated foundation dimensions and loads, we estimate that total post-construction settlement of footings designed and

constructed in accordance with the recommendations of this report will be ¹/₂-inch. Differential settlement between similarly loaded, adjacent footings is expected to be ¹/₄-inch, provided footings are founded on similar materials (e.g., all on native soil). Settlement of all foundations is expected to occur rapidly, generally during the construction time frame for the building. Improvements supported on non-structural fill may experience larger settlements.

- <u>All footing excavations should be observed by the project Soils Engineer</u> prior to placing reinforcing steel for concrete to verify the underlying soil conditions and recommendations contained herein are implemented during construction.
- Excavations from the surface to 15 or more feet below surface are likely to encounter boulders with intervening soil filled voids. Soil and altered rock temporary excavations may potentially be in the range of 1H:1V to 1.5H:1V. Slopes to 1H:3V feet may be generally stable below this depth, provided chain link netting is used to prevent loosening of boulders. However, RTGA should closely observe excavations below the bedrock surface to verify that loose or over-steepened zones are not present which could allow rock wedges or boulders to slide into the excavation. Steeper excavations can be implemented if required, but will generally require either soil-nail and shotcrete facing in soil and weathered bedrock, or spot nailing of bedrock blocks and wedges in intact bedrock (without shotcrete)
- If required, rock anchors or soil nails may be needed to stabilize unstable areas within the excavation wall. Rock anchors or soil nails commonly used in the area are hollow bars with 1½-inch outer diameter fitted with a drill bit of 3 to 3½-inches diameter. Soil nails are typically drilled 5 feet or more into the bedrock surface. Neat cement grout is pumped through the hollow center of the bar and create a 3½-inch-diameter annulus of grout around the bar back to the surface. For design of soil nails the ultimate grout to soil/bedrock interface is expected to be approximately 30 psi in soil to 60 psi for depths greater than 5 feet into the bedrock surface (FHA, 2005).
- Soil nail walls in theory could be used for permanent support of the uphill side of the excavation, however practically the excavation will not be neat and the excavation line will likely vary widely outside of the building line due to uneven rock joints and fractures. Careful consideration would be required for drainage and removal of groundwater seepage behind the shotcrete face so that it does not affect interior building components.

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• If required, subterranean structures and retaining walls, including foundations, should be designed to resist the lateral earth pressure exerted by the retained, compacted backfill plus any additional lateral force that will be applied to the wall due to surface loads placed at or near the wall. The table below presents a list of soil design parameters for these structures.

TABLE 2 - LATERA	L EARTH PRESSURES
<u>Earth Pressure</u>	<u>Equivalent Fluid Density (pcf)</u>
Active Pressure	
Retained Slope = Level to 4H:1V	30
Retained Slope = $4H:1V$ to $2H:1V$	40
At-Rest Pressure	
Rigidly Restrained	60
Seismic Active	
Retained Slope = Level to 4H:1V	60
Retained Slope = $4H:1V$ to $2H:1V$	80
Allowable Passive Pressure	
Retained Slope = Level	350
Allowable Coefficient of Friction	0.45

- Surcharge loads behind walls are not factored into the recommended equivalent fluid pressures. Any anticipated surcharge load should be factored into the design in addition to the above-mentioned pressures.
- The active pressure can be used for flexible walls with a potential to dislocate. At-rest pressure should be used for building walls or restrained walls. The seismic active pressure is applicable for the earthquake condition for both at-rest and active walls.
- The values do not include hydrostatic pressures that might be caused by collected runoff water trapped behind the structure. Accordingly, wall backfill should be free draining and provisions should be made to collect and dispose of excess water that may accumulate behind earth retaining structures.
- Adequate drainage of backfill in the form of subdrains should be provided at the base of exterior walls (preferably below the joint between wall and footing) to collect and dispose of

excess water which can accumulate behind the retaining structures. The subdrain should be placed in the drain rock and be enveloped in filter fabric as shown on Plate 9. Drain rock should be densified to a non-yielding condition by placing in lifts and compacting in a manner which does not damage the waterproofing material or structurally damage the wall. Dripline trenches or surface drains should not be connected to the exterior foundation drain.

- Heavy compaction equipment or other loads which may result in lateral pressures higher than those recommended above should not be allowed within proximity to the wall, unless planned for in the structural design.
- Where retaining walls will enclose useable interior space or floors below grade, the wall should be waterproofed. Waterproofing material should consist of rubberized asphalt, polymer-modified asphalt, butyl rubber, or other approved materials capable of bridging nonstructural cracks. Joints in the membrane should be lapped and sealed in accordance with the manufacturer's recommendations. Extra attention should be paid to concrete cold joints between the wall and footing. A manufactured water-stop or key should be placed at all cold joints.
- The drain system should discharge into a properly designed infiltration trench, storm drain system, or other approved exterior location. Filter fabric (Mirafi 140N or approved alternate) should separate the drain rock from overlying fill materials to prevent sand or fines from migrating into the drain rock.
- Due to the potential for water seepage and moisture migration through concrete slab-on-grade floor and to reduce the potential for build-up of hydrostatic pressure, we recommend a drain system be constructed under slab-on-grade floors. In general, the under-slab drain system should consist of 3-inch-diameter (minimum) perforated pipe placed in at least 8-inches of drain rock and spaced at a maximum 24 feet apart. The subgrade should slope toward the perforated drainpipes and the pipes should have at least a one-percent slope.
- Crawl spaces must be built with permanent drainage, including sloped interior surfaces and/or a perimeter drain trench filled with drain rock. Positive drainage should be provided from all portions of the crawlspace to the lowest part of the crawlspace, and then under or through the perimeter footing to discharge down gradient from the structure and exterior flatwork. The

discharge should be into a properly designed infiltration trench, the storm drain system, or other approved exterior location.

- Radon is a naturally occurring, dense, odorless gas that is generated from radioactive degradation of uranium in granitic rocks decaying into isotopes which can contribute to lung cancer. Active or passive radon venting of below-grade spaces should be considered, including crawlspaces, to reduce potential for radon to diffuse into living spaces. The subfloor perforated pipe vent system under the slab-on-grade floor can be considered for passive radon mitigation.
- Finished grades should be sloped to prevent ponding of water and to direct surface water away from foundations. Impervious surfaces adjacent to the building foundation should slope away from the building at a minimum 5 percent gradient for at least 5 feet. The dripline trench should not be in direct communication with the foundation drain layer.

LIMITATIONS

This report has been prepared for design purposes for specific application to the currently proposed project in accordance with the generally accepted standards of practice at the time the report was written. If the scope of the proposed construction changes from those described, our recommendations should be reviewed by us and may require modification. No warranty, express or implied, is made.

All parties to the project including the designer, contractor, subcontractors, etc., should be made aware of this report in its entirety. The use of information contained in this report for bidding purposes should be done at the Contractor's option and risk.

941 and 947 Tahoe Boulevard - Geotechnical Assessment July 1, 2021 Project No. 21073.001 Page 13 of 13

CLOSURE

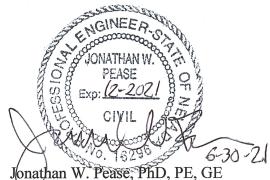
We trust the report provides you with the information you require. If there are any questions, please contact our office.

Sincerely, *Reno Tahoe Geo Associates, Inc.*

Kene Makaney

Shane Mulvaney Senior Geologist

Plates:	Plate 1 -	Site Map
	Plate 2 -	ReMi 1D & 2D Results
	Plate 3 -	Log of Test Pit TP-1
	Plate 4 -	Log of Test Pit TP-2
	Plate 5 -	Log of Test Pit TP-3
	Plate 6 -	Soil Classification Chart
	Plate 7 -	Grain Size Analysis
	Plate 8 -	Atterberg Limits
	Plate 9 -	Typical Back of Wall Drain

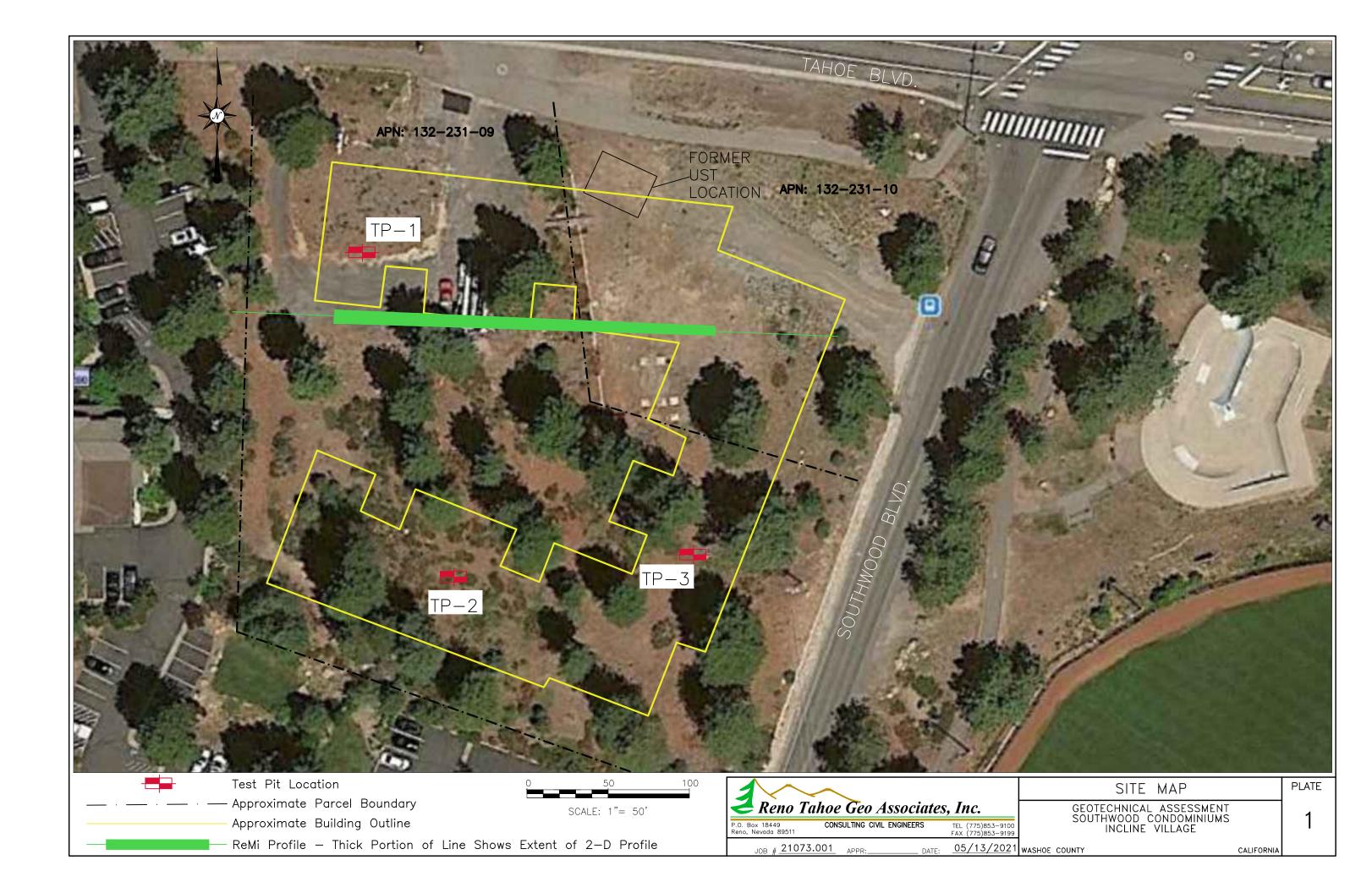


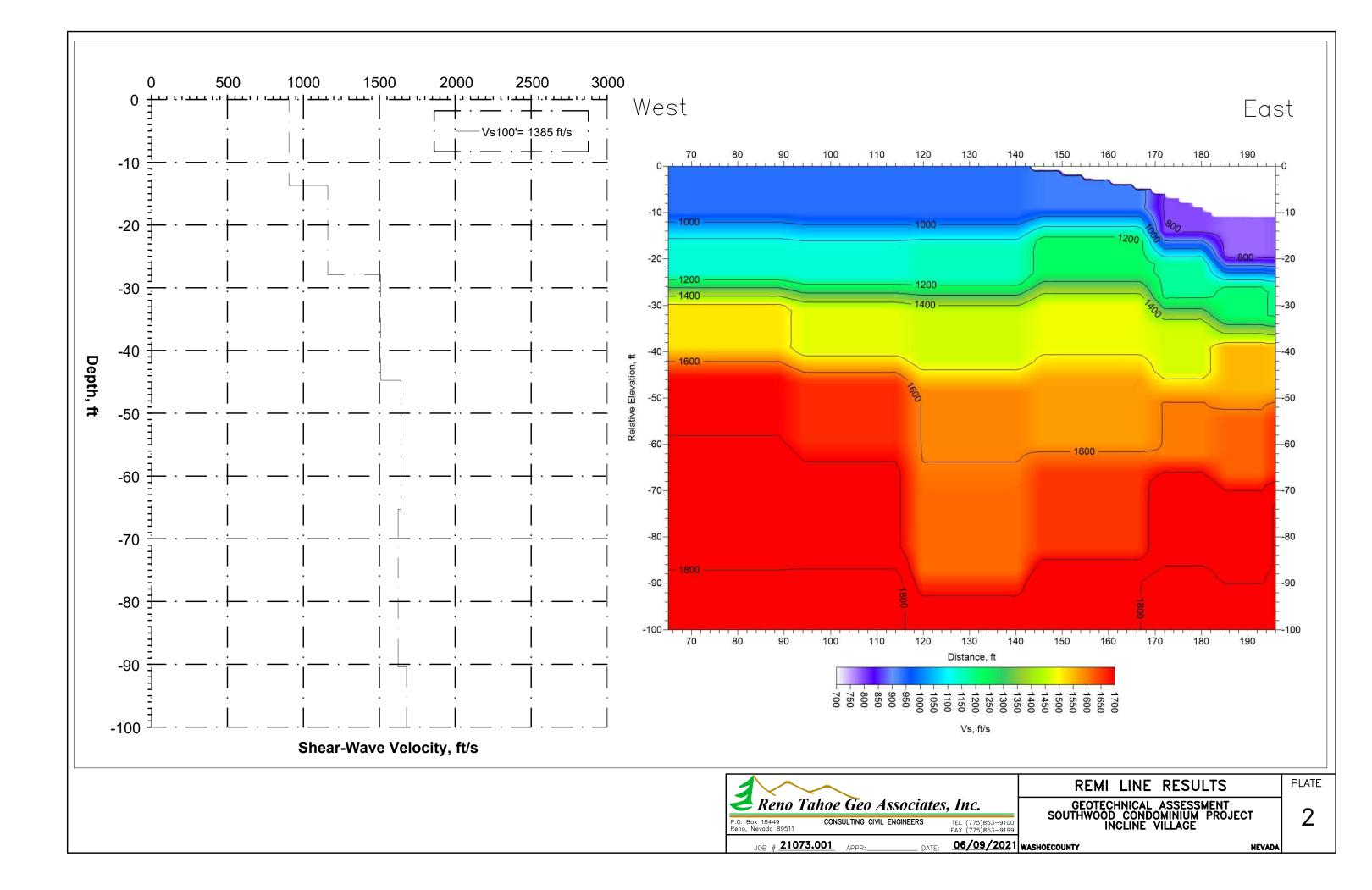
Jonathan W. Pease; PhD, PE, GE Principal Engineer NV 16296

Reno Tahoe Geo Associates, Inc.

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PLATES

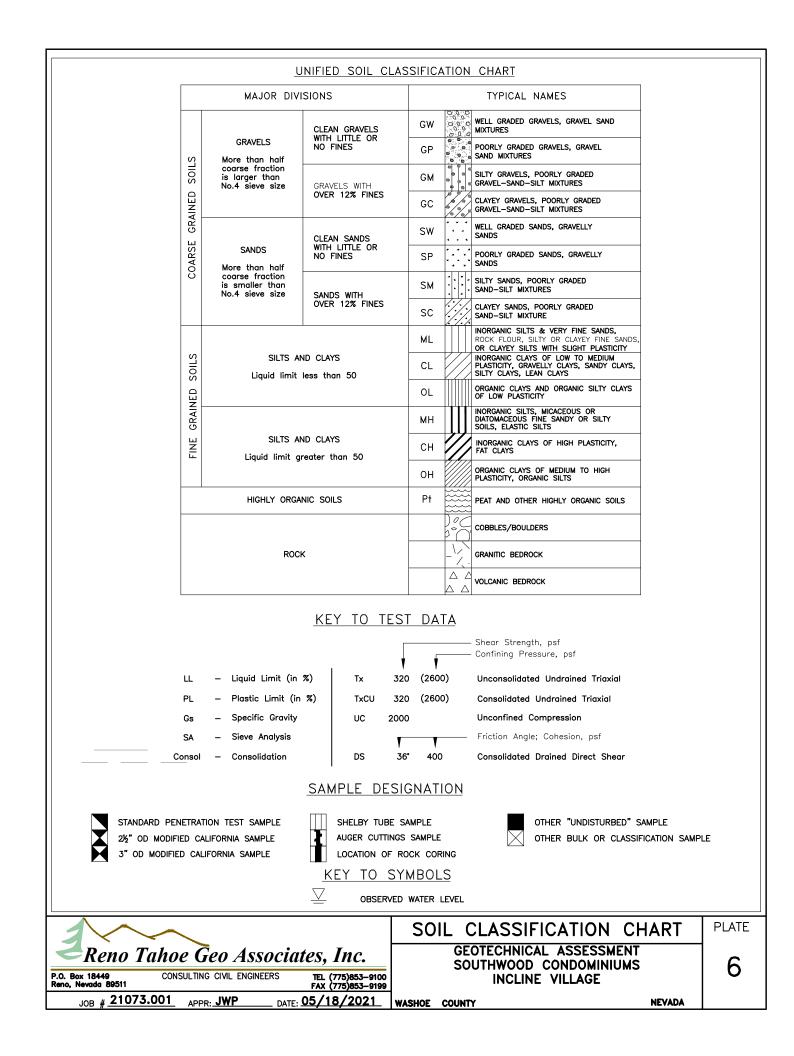




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			•			-			Slightly moist, loose, fine to coarse angular to subrounded gravel, non-plastic silt in fine to coarse granitic sand. 20% angular to	,
			•	:		10 —			subrounded cobbles and 20% subangular to subrounded boulders 3 feet size. (10YR 6/8)	s to
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1/21		· ·	•			_	$\left(\right)$		YELLOWISH BROWN LEAN CLAY (CL) Slightly moist to moist, fine sand in soft to firm, low plasticity clay.	-
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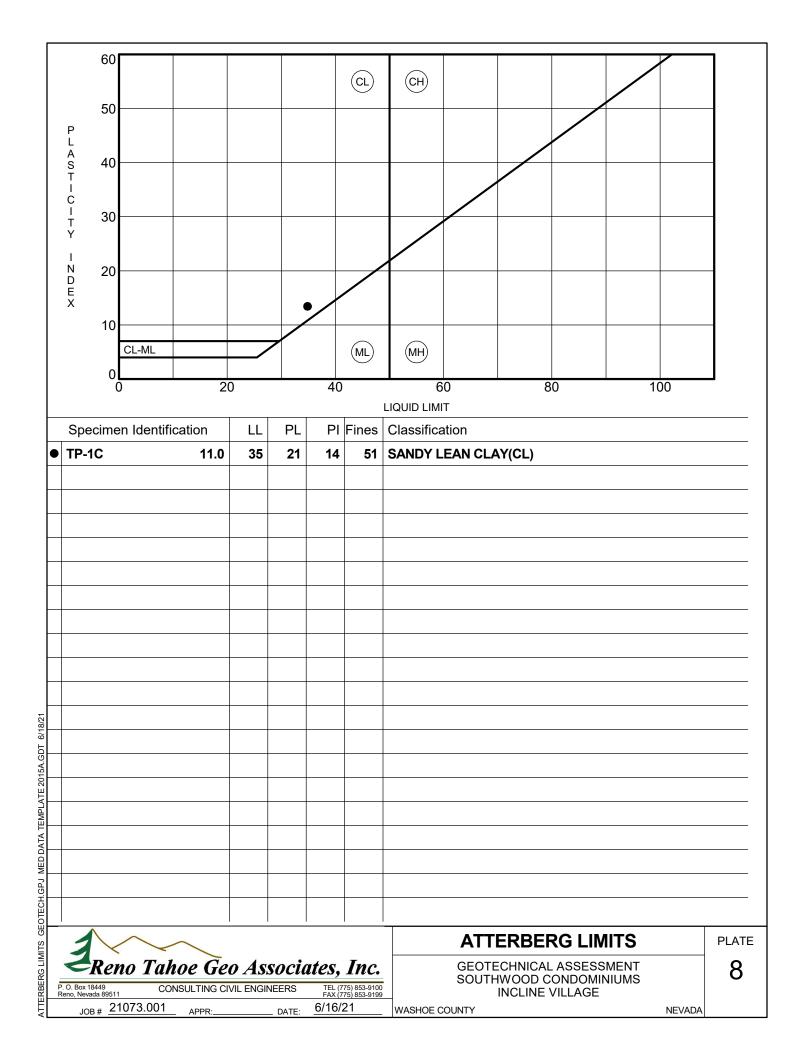
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				- - 2 - -	coarse sand. Pine duff overlying topsoil. (2.5YR 3/4) (est.15% G/ 60% S/ 25% F) DARK YELLOWISH BROWN SILTY SAND WITH COBBLES AND BOULDERS (SM) Dry to slightly moist, loose matrix, fine to coarse angular to subrounded gravel, non-plastic silt in fine to coarse granitic sand. 25% angular to subrounded cobbles and 20% subangular to subrounded boulders to 3 feet size. Abundant roots. (10YR 4/6) (est.20% G/ 60% S/ 20% F)
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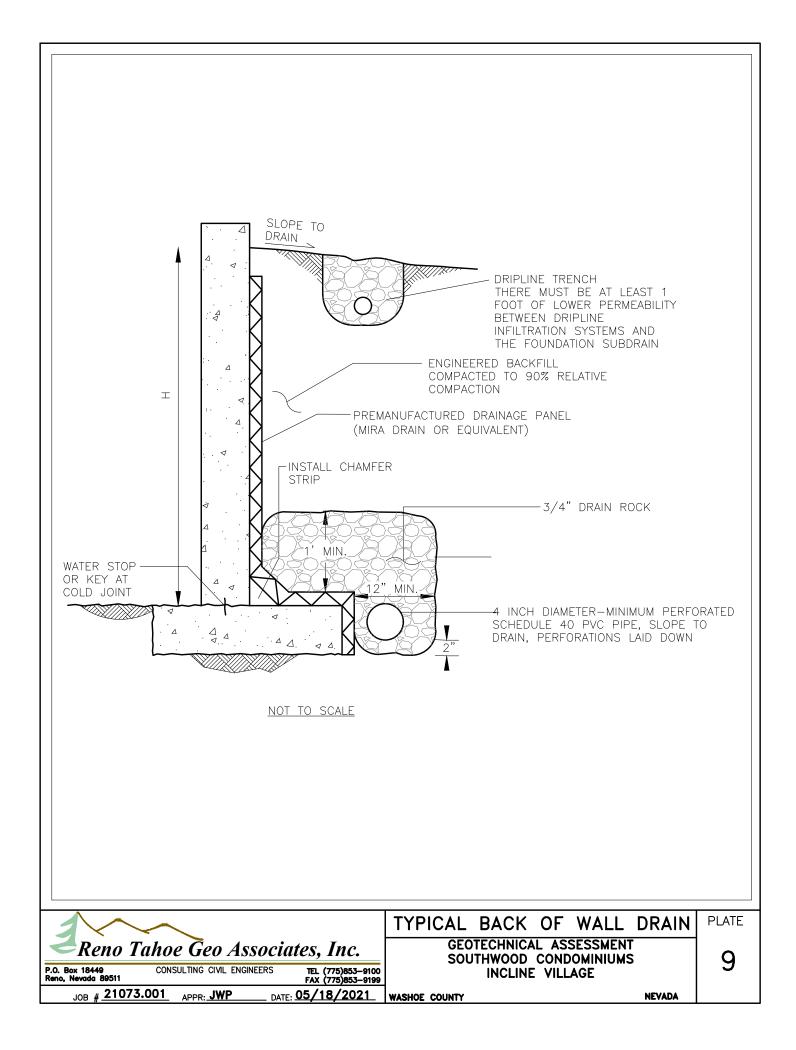
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					- 6				YELLOWISH RED SILTY SAND (SM) Slightly moist, loose to medium dense, non-plastic silt in fi Some dark yellowish brown (10YR 4/6) mottling. Minor an subrounded gravel. (5YR 5/8) (est.10% G/ 65% S/ 25% F)	ne sand. gular to
					- - 8				GRAY / LIGHT OLIVE GRAY SILTY SAND (SM) Dry, medium dense to dense, non-plastic silt in fine to coa Some angular to subangular cobbles and boulders. Excav at 9'. (5Y 6/1) (est.20% G/ 60% S/ 20% F)	rse sand. vator refusal
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Incline Residential Tahoe/Southwood *Transportation Study*

Prepared for

Greenwood Homes 940 Southwood Blvd. #101 Incline Village, NV 89451

Prepared by LSC Transportation Consultants, Inc. 2690 Lake Forest Road, Ste. C P.O. Box 5875 Tahoe City, CA 96145 530-583-4053

December 7, 2021

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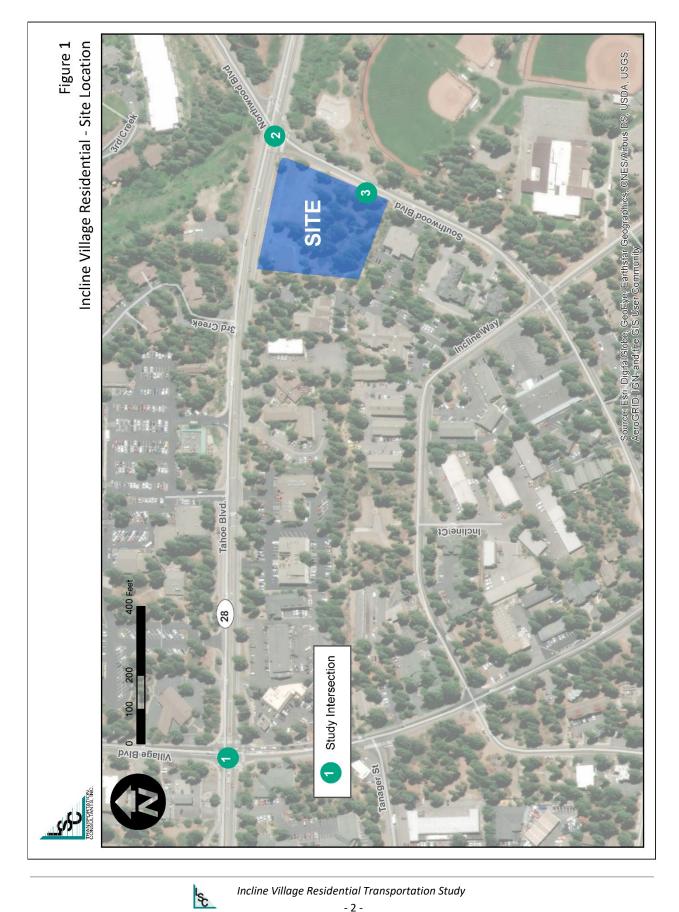
Figure 1: Incline Village Residential – Site Location	2
Figure 2: Peak Hour Warrant	. 16



The Incline Village Residential project is located on the southwest corner of SR 28 (Tahoe Boulevard) and Southwood Boulevard in Incline Village, Nevada. The project would consist of 40 multi-family townhomes. The site location is shown in Figure 1.

The purpose of this report is to present an analysis of the traffic and air quality impacts associated with the proposed project. Initially, existing traffic conditions near the proposed site are discussed. The proposed land uses associated with the project are then assessed in terms of the generation of new traffic. An appropriate distribution of traffic onto the adjacent roadway system is then identified. Using this distribution pattern, the forecasted generated trips are assigned to the nearby roadway system to identify the impact on intersection Level of Service (LOS). In addition, the following areas of impact reevaluated:

- 1. Site access conditions and driveway spacing
- 2. Traffic signal warrant
- 3. Regional Vehicle Miles Traveled (VMT) Analysis
- 4. Air quality impacts



The following discussion presents information regarding existing transportation conditions in the studyarea.

ROADWAY CHARACTERISTICS

The project site is served by the following existing roadways:

State Route 28 (Tahoe Boulevard) is the primary highway serving Lake Tahoe's north shore. It is atwo-lane roadway that runs through Incline Village, Nevada from Tahoe City, California to US 50. To the west of Incline Village, State Highway 28 terminates at the junction of State Route 89 in Tahoe City, California. To the east, the highway turns south and continues along the east shore of Lake Tahoe and ends at US 50. Within Incline Village itself, State Highway 28 is designated as Tahoe Boulevard, with a posted speed limit of 35 miles per hour. The section between Village Boulevard and the eastern Northwood Boulevard/Southwood Boulevard intersection contains a center two-way left turn lane; othersections generally provide one lane in each direction, with turn lanes at major intersections.

Village Boulevard is a two-lane roadway that intersects SR 28 and provides access to primarily residential neighborhoods to the south, and residential neighborhoods as well as government offices to he north. The posted speed limit is 25 miles per hour.

Northwood Boulevard and Southwood Boulevard are two-lane roadways forming a loop roadway around the central Incline Village area. This loop is designated as Southwood Boulevard to the south of SR 28 and Northwood Boulevard to the north of SR 28. To the west of Village Boulevard, the twoboulevards meet at a signalized intersection with SR 28. To the east of Village Boulevard, both meet at anunsignalized intersection with SR 28, controlled by stop signs on the Boulevard approaches to the highway. The posted speed limit is 25 miles per hour.

EXISTING TRAFFIC VOLUMES

This study is based on typical summer traffic conditions. PM turning-movement counts were conducted by LSC staff at the SR 28/Northwood Blvd/Southwood Blvd study intersection from 3:30 PM to 5:30 PM on Thursday, June 3, 2021. PM turning-movement counts were conducted by LSC at the SR 28/Village Blvd study intersection from 3:30 PM to 5:30 PM on Wednesday, June 2, 2021. Nevada Department of Transportation (NDOT) monthly variation was analyzed at the permanent location SR 28 (Tahoe Blvd) 915feet north of Lakeshore Drive/Pinion Drive. In 2019, July was determined to be the peak month. The volumes from our counts were increased using a growth factor of 1.2 to adjust the counts to peak monthconditions. The resulting 'existing no project' peak-hour traffic volumes are shown in Table 1.



Table 1: Incline Village Residential - Peak Hour Intersection Traffic Volumes	Peak H	our Inter.	section	Traffic	: Volume	Ş							
		Northbound	_		Southbound	_		Eastbound			Westbound		
Intersection	Left	Through	Right	Left	Through	Right	Left	Through	Right	Left	Through	Right	Total
Evitetian No Devicet													
SR 28/Village Blvd	113	267	86	131	185	73	63	479	104	109	458	120	2218
SR 28/Southwood Blvd/Northwood Blvd (East)	22	21	63	29	5	39	44	611	63	40	561	27	1533
Southwood Blvd/Site Access	0	105	0	0	118	0	0	0	0	0	0	0	223
Project Net Impact													
SR 28/Village Blvd	0	0	0	0	0	0	0	ŝ	0	0	2	0	2
SR 28/Southwood Blvd/Northwood Blvd (East)	æ	0	1	0	1	0	0	0	5	2	0	0	12
Southwood Blvd/Site Access	Ч	0	0	0	0	∞	4	0	1	0	0	0	14
Existing Plus Project													
SR 28/Village Blvd	113	267	86	131	185	73	93	482	104	109	460	120	2223
SR 28/Southwood Blvd/Northwood Blvd (East)	25	21	64	29	16	39	44	611	68	42	561	27	1545
Southwood Blvd/Site Access	1	105	0	0	118	∞	4	0	1	0	0	0	237
Source: LSC Transportation Consultants, Inc.													

Incline Village Residential Transportation Study

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EXISTING TRANSIT CONDITIONS

Transit services in the North Shore area are provided through the Tahoe Truckee Area Regional Transportation (TART). The bus service in this area is the TART Mainline. The Mainline Route travels the western shore of Lake Tahoe from Tahoma to the north shore at Incline Village. It operates between 6:00AM and 9:30 PM, providing one run per hour. Existing bus stops are conveniently located along SR 28 at Christmas Tree Village, Raley's, and Northwood Blvd and on Southwood Blvd at the Incline State Park within the vicinity of the project site.

In the summer of 2021, a pilot "microtransit" transit service is being operated, marketed as TART Connect. It provides free rides for passengers making app requests from 8 AM to Midnight 7 days a week. Three zones are being operated, including an Incline Village / Crystal Bay zone that encompasses the project site.

EXISTING BICYCLE AND PEDESTRIAN CONDITIONS

Bicycle Facilities

Bicycle paths, bicycle routes and bicycle lanes are provided in the vicinity of the project. A Class I bikeway (multipurpose walking and bicycling path) can be found along Village Blvd from College Drive south to Lake Shore Blvd and along the entirety of Lake Shore Blvd. A bikeway is also located starting at the eastern Southwood Blvd/SR 28 intersection that loops around clockwise and ends on Northwood Blvd at the Incline Elementary School. Class II bikeways (bike lanes) can be found along SR 28 from the western Lake Shore Blvd intersection to the eastern Lake Shore Blvd intersection.

Pedestrian Facilities

Within the vicinity of the site, multipurpose walking and bike paths are provided along SR 28 and Southwood Blvd. The SR 28/Northwood Blvd/Southwood Blvd intersection has pedestrian crosswalks on all four sides of the intersection as well as a Rectangular Rapid-Flashing Beacon (RRFB) in the East and West directions. Another RRFB is placed along SR 28 in front of the Raley's driveway. At the SR 28/VillageBlvd intersection, crosswalks can be found on the west, east and south approaches of the signalized intersection.

Overall Non-Auto Access

In summary, the site is served by relatively good transit and bicycle/pedestrian access opportunities. The location near major trip generators (such as shopping) also makes the site relatively conducive to non- auto travel. Specific non-auto reductions are discussed in Chapter 3.

EXISTING AIR QUALITY CONDITIONS

Air quality is a function of both local climate and local sources of air pollution. Air quality is the balance of the natural dispersal capacity of the atmosphere and emissions of air pollutants from human uses of the environment.

Regional Setting

Many important factors determine local and regional air quality, with the most critical being the quantity, type, and location of pollution sources. Climatic conditions, such as wind speed and direction, temperature gradients, and inversions and precipitation interact with the physical features of the landscape to determine the movement and dispersion of air pollutants.



<u>Climate</u>

The Lake Tahoe Air Basin is surrounded by various mountain ranges within the Sierra Nevada. The Tahoe Basin's climate is cool and dry in the summer and cold and wet in the winter. Temperatures can vary froma daily mean of 60 degrees Fahrenheit (15.6 degrees Celsius) in the summer to about 20 degrees Fahrenheit (-6.7 degrees Celsius) in the winter. Diurnal temperature ranges combine to form characteristics that affect air quality on a daily and seasonal basis. Temperature inversions with the regionare generally caused by nighttime cooling of the land surface, which occurs at a faster rate than the cooling of the overlying air. These inversions can trap air pollutants near their source by limiting vertical mixing. These conditions occur most frequently in the winter.

The enclosed nature of the basin and the large diurnal temperature range combine to form specific air basin characteristics that affect air pollution concentrations on a daily and seasonal basis. Relevant to the present discussion are the issues of mixing height and temperature inversions. The "mixing height" is the height or thickness of the air blanket available for dispersion of airborne pollutants emitted near the ground surface.

Normally, air temperature decreases with an increase in elevation. When a "temperature inversion" occurs, however, temperatures within a layer of air increase with height. The two issues are related inthat the presence of a temperature inversion reduces or lowers the mixing height normally available, thereby lessening the dispersion potential for pollutants in the air basin.

Inversions will trap pollutants near their emission source by precluding vertical mixing processes from dispersing the pollutants. Consequently, potential for high pollutant concentrations is greatest duringstrong, persistent, low-level radiation inversion conditions, which generally occur in the Lake Tahoe region during the winter months.

In the Lake Tahoe Air Basin, inversions are generally caused by nocturnal radiational cooling of the land surface, which occurs at a rate slower than the cooling of the overlying air. During summer months, the morning inversion is broken up by strong surface heating, usually by 9:00 AM to 10:45 AM. Thus, by early morning, mixing heights have typically increased to over 5,000 feet with strong vertical mixing. By midevening, the inversion slowly begins to form again, peaking during the early morning.

During winter months, surface heating is less pronounced, and the morning inversion may persist untilnoon (~50% of the time) or later. Consequently, the Lake Tahoe Basin exhibits a high potential for air pollution during the early morning hours, especially during the winter.

Standards and Thresholds

Federal, state, and regional standards exist for ambient air quality in the Tahoe Basin. The air quality plan element of the integrated regional transportation plan focuses on the need for air quality control strategies. The various federal, State of Nevada, and TRPA standards are listed in Table 2.



	Averaging	Feder	al Standards	Nevada Standards	TRPA Standards				
Pollutant	Time	Primary	Secondary	Concentration	Concentration				
Ozone (O ₃)	1 Hour	No Standard	No Standard	No Standard	0.08 ppm				
	8 Hour	0.070 ppm	Same as Primary	0.070 ppm	No Standard				
Carbon Monoxide (CO)									
	1 Hour	35 ppm	No Standard	35 ppm	No Standard				
				9 ppm below 5000'					
	8 Hour	9 ppm	No Standard	6 ppm above 5000'	6 ppm				
Nitrogen Dioxide (NO ₂)	1 Year	53 ppb	Same as Primary	53 ppb	Maintain NO _x emissions at or				
	1 1001	55 660	Same as i mary	33 660	below 1981 levels				
	1 Hour	100 ppb	No Standard	100 ppb	No Standard				
Sulfur Dioxide (SO ₂)	1 Year	No Standard	No Standard	0.030 ppm	No Standard				
	24 Hour	No Standard	No Standard	0.14 ppm	No Standard				
	3 Hour	No Standard	0.5 ppm	0.5 ppm	No Standard				
	1 Hour	75 ppb	No Standard	75 ppb	No Standard				
Particulate Matter	1 Year	No Standard	No Standard	No Standard	50 μg/m ³ in the portion of				
(PM ₁₀)					the region within Nevada				
	24 Hour	150 μg/m ³	Same as Primary	150 μg/m ³	150 $\mu\text{g/m}^3$ in the portion of				
					the region within Nevada				
Fine Particulate	1 Year	12 μg/m ³	15 μg/m ³	12 μg/m ³	15 μg/m ³ in the portion of				
Matter (PM _{2.5})		12 µ8/	10 µ6/ m	12 µ6/ m	the region within Nevada				
	24 Hour	35 μg/m ³	Same as Primary	35 μg/m ³	35 μg/m ³				
Sulfates	24 Hour	No Standard	No Standard	No Standard	No Standard				
Lead F	Rolling 3-month averag	e 0.15 μg/m ³	Same as Primary	0.15 μg/m ³	No Standard				
				10,					
Hydrogen Sulfide	1 Hour	No Standard	No Standard	0.08 ppm	No Standard				
Vinyl Chloride	24 Hour	No Standard	No Standard		No Standard				
Visibility	8 Hour	No Standard	No Standard	No Standard	Regional				
Reducing Particles	(Observation)				97 mi (156 km), 50% of the yea				
					71 mi (115 km), 90% of the yea				
					Sub-regional				
					48 mi (78 km), 50% of the year				
					19 mi (31 km), 90% of the year				

Source: NAC 445B.22097 State standards of quality for ambient air (NRS 445B.210), Nevada Administrative Code (accessed June 2021) Source: TRPA Regional Plan, Attachment 1: Resolution 82-11 Exhibit A, admended May 23, 2018



Attainment Designations

Air quality in most areas of the Lake Tahoe Air Basin is good. As shown in Table 3, the Lake Tahoe Air Basin met all the federal and state standards. The region was in non-attainment on the California side of the TRPA PM10 standard which is based on 2015 data (the most recent data available) but was shown as attainment on the Nevada side.

Т

Federal	Nevada	TRPA		
Unclassified/Attainment	Unclassified/Attainment	Attainment		
Unclassified/Attainment	Unclassified/Attainment	Attainment		
Unclassified/Attainment	Unclassified/Attainment	Attainment		
Unclassified/Attainment	Unclassified/Attainment	-		
Unclassified/Attainment	Unclassified/Attainment	Attainment ¹		
Unclassified/Attainment	Unclassified/Attainment	Attainment		
Unclassified/Attainment	Unclassified/Attainment	-		
-	Unclassified/Attainment	-		
-	-	Attainment		
ut non-attainment on Californ	ia side.			
Source: Tahoe Regional Planning Agency (TRPA) Threshold Evaluation Report, 2015.				
	Unclassified/Attainment Unclassified/Attainment Unclassified/Attainment Unclassified/Attainment Unclassified/Attainment Unclassified/Attainment Unclassified/Attainment unclassified/Attainment unclassified/Attainment	Unclassified/Attainment Unclassified/Attainment Unclassified/Attainment Unclassified/Attainment		



TRIP GENERATION

The first step in the analysis of future traffic impacts is to prepare an estimate of the number of trips generated by the existing site and the proposed project. Trip generation is the evaluation of the number of vehicle-trips that will either have an origin or destination at the project site. Daily Vehicle-Trip Ends (DVTE) and Peak Hour Vehicle-Trip Ends (PHVTE) need to be determined in order to analyze the potential impacts from the proposed project.

Full Buildout includes construction of the 40 multi-family units. The trip generation analysis for the proposed project land uses is summarized in Table 4.

Standard daily trip generation rates are provided in the Tahoe Regional Planning Agency's (TRPA) *Trip Table* (TRPA, 2020) and peak-hour rates are provided in the Institute of Transportation Engineers (ITE)*Trip Generation, 10th Edition Manual* (ITE, 2017). These standard rates are shown in Table 4.

Reduction for Non-Auto Trips

Non-auto trips, such as trips made to/from the site via bike, walking or transit, reduce the number of vehicle trips generated by the project. *2018 Summer TRPA Travel Mode Share Survey* data was reviewed.Data from the surveys conducted at locations at Incline Village near the Raley's and at the Incline Village Recreation Center. Based on responses from this group (with 60 data points), the non-automotive trip percentage was approximately 40 percent. Due to the project's location relative to commercial and shopping as well as the high school, the connecting bike and pedestrian paths, the nearby employment locations, a reduction of 20 percent non-auto travel is applied to the residential units. The non-auto reduction is less than that found at the commercial center (40 percent) due to the home to work trips and home to recreation trips which were not reflected in the commercial center area.

Trip Generation at Site Driveway

Multiplying the land use quantities by the trip rates and applying reductions for non-auto trips yields thevehicle trips generated at the site driveway for proposed project conditions. As shown in Table 4, the proposed land uses are forecasted to generate a total of approximately 174 one-way daily vehicle trips (DVTE) at the site driveway on a weekday, including 14 PM peak-hour vehicle-trips (9 inbound plus 5 outbound).

TRIP DISTRIBUTION AND ASSIGNMENT

The distribution of site-generated trips is defined based upon the following:

- 1. The site's location relative to complementary land uses and regional access points.
- 2. The observed pattern of existing traffic movements.
- 3. The driveway on SR 28 will be used exclusively for emergency access. As a result, all trips will be to/from the driveway on Southwood Boulevard.

Trip distribution patterns for vehicle trips made to/from the project are estimated and the results are shown in Table 5.



Table 4: Incline Village Residential - Trip Generation	Residential - T	rip Gen	eratioı	-				
						Vehicle Trips	Trips	
		ITE Land		Trip Generation Rates ¹	Reduction for	at Site Driveways	/eways	
	ITE Land Use	Use	Doily.	PMPeak Hour	Non-Auto	PMP	PM Peak Hour	
Description Quantity Units	Category	Code	Uaily	In Out Total	Access		In Out Total	
Multi Family 40 DU Residence	Multi Family Housing (Mid-Rise)	221	5.44	Fitted Curve	20%	174 9	5 14	
DU= Dwelling Unit								
Note 1: TRPA daily rates follow ITE for these land uses. ITE Peak hour rate.	or these land uses. ITE F	eak hour ra	te.					
Source: LSC Transportation Consultants, Inc., Tahoe Regional Planning Agency (TRPA) Trip Table, and Institute of Transportation Engineers Trip Generation (10th Edition)	Inc., Tahoe Regional Plann	ing Agency (TRPA) Trip	Table, and Institute of Trai	nsportation Engineers	s Trip Generation	<u>1</u> (10th Edition)	

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Table 5: Incline Village Residential - Trip Distribution				
To/From	Percent			
South on Southwood Blvd	15%			
North on Northwood Blvd	10%			
East on SR 28	20%			
SR 28 Between Village and Northwood/Southwood	20%			
West on SR 28	35%			
Total	100%			
Source: LSC Transportation Consultants, Inc.				

The site-generated traffic volumes are assigned through the study intersections by applying the distribution percentages to the peak-hour vehicle trips. The resulting PM peak-hour traffic volumes estimated to be generated by the full buildout of the project are shown in Table 1. The project-generatedpeak-hour intersection turning movement volumes are then added to the 'no-project' volumes, yielding the 'existing with project' peak-hour intersection traffic volumes presented in Table 1.



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LEVEL OF SERVICE

LOS is a quantitative and qualitative measure of traffic conditions on isolated sections of roadway or intersections. LOS ranges from "A" (with no congestion) to "F" (where the system fails with gridlock or stop-and-go conditions prevailing). Detailed LOS definitions are included in Appendix A. As is the standardfor traffic engineering analyses, intersection LOS is analyzed based upon the procedures presented in the*Highway Capacity Manual* (Federal Highways Administration, 2016) using the Synchro software application (Version 10.3, Trafficware). The LOS calculations are contained in Appendix B for further reference.

LOS Standards

The TRPA LOS standards for the Lake Tahoe Basin, established by the Tahoe Regional Planning Agency (TRPA), are set forth in the 2019 Regional Transportation Plan with the intent that the Region's highway systemand signalized intersections during peak periods shall not exceed the following:

- 1. LOS C on rural scenic/recreational roads,
- 2. LOS D in rural developed areas,
- 3. LOS D on urban roads, or
- 4. LOS D for signalized intersections LOS E may be acceptable during peak periods not to exceedfour hours per day.

The Regional Transportation Plan Mobility 2035 (TMPO/TRPA, 2012) also states that: "These vehicle LOS standards may be exceeded when provisions for multimodal amenities and/ or services (such as transit, bicycling, and walking facilities) are adequate to provide mobility for users at a level that is proportional to the project-generated traffic in relation to overall traffic conditions on affected roadways." (pp. 2 - 10). While the Tahoe Regional Planning Compact looks to "reduce the dependency on the private automobile," there are currently no adopted requirements or standards regarding the quality of service of other travel modes (i.e., transit, biking, or walking) that could potentially reduce the demand on the roadway system.

The TRPA does not have a specific adopted standard for unsignalized intersections.

The Washoe County LOS Standards are set forth in the 2050 Regional Transportation Plan with theintent that roadway facilities do not exceed the following:

- 1. LOS D for all regional roadway facilities projected to carry less than 27,000 ADT at the latest RTPhorizon
- 2. LOS E for all regional roadway facilities projected to carry 27,000 or more ADT at the latest RTPhorizon
- 3. LOS F for:
 - a. 4th St/Prater Way Evans Avenue to 15th St
 - b. Plumas St Plumb Ln to California Ave
 - c. Rock Blvd Glendale Ave to Victorian Ave
 - d. Virginia St Kietzke Ln to S McCarran Blvd
 - e. Virginia St Plumb Ln to Liberty St & 8th St to 17th St
 - f. Sun Valley Blvd 2nd Ave to 5th Ave
 - g. Intersection of N Virginia St and Interstate 80 ramps



Existing Year Intersection Level of Service

As shown in Table 6, all study intersections currently attain the LOS thresholds during the existing yearcondition without the project with the exception of SR 28/Southwood Blvd/Northwood Blvd. The stop-controlled intersection of SR 28/Southwood Blvd/Northwood Blvd/Northwod Blvd/Northwood Blvd/Northwood Blvd/Northwood B

With implementation of the proposed project the new site driveways intersecting SR 28 and Southwood Blvd will operate at an acceptable LOS A. The intersection of SR 28/Southwood Blvd/Northwood Blvd willremain at an unacceptable LOS F with a small increase in delay.

Table 6: Incline Village	Residential -	- Existing	Intersed	ction LC	OS Summ	ary
			PN	Λ	PI	М
			Existing N	o Project	Existing Pl	us Project
			Delay		Delay	
Intersection	Control Type	LOS Threshold	(sec/veh)	LOS	(sec/veh)	LOS
SR 28/Village Blvd	Signalized	D	15.1	В	15.1	В
SR 28/ Southwood Blvd/ Northwood Blvd (East)	TWSC	D	99.7	F	105.4	F
Southwood Blvd/Site Access	TWSC	D	0.0	А	9.7	А

BOLD text indicates that LOS standard is exceeded.

TWSC = Two-Way Stop-Control; AWSC = All-Way Stop-Control

NOTE 1: Level of service for signalized intersections is reported for the total intersection.

NOTE 2: Level of service for roundabouts and other unsignalized intersections is reported for the worst movement.

Source: LSC Transportation Consultants, Inc.



The project would generate approximately 174 new daily one-way vehicle trips and 14 PM peak-hourvehicle trips (9 inbound plus 5 outbound) at the site access driveway. The following areas of transportation impacts are evaluated in this section:

- Analysis of the Need for a New Traffic Signal
- Intersection Level of Service (LOS)
- Site Access Plans
- Vehicle Miles Traveled (VMT)

TRAFFIC SIGNAL WARRANT ANALYSIS

NDOT has established a series of "warrants" to define conditions in which a traffic signal should be provided. This is to ensure that signals are only provided in locations where the benefit outweighs the impacts of a signal (notably, the increase in traffic delays along the major roadway). The need for a new traffic signal at the stop-controlled SR 28/Northwood Blvd/Southwood Blvd (east) is evaluated using the procedure discussed in NDOT *Access Management System and Standards* (November 2017), which relieson the warrants for a traffic signal as defined in the Manual on Uniform Traffic Control Devices (MUTCD).

The MUTCD provides a series of 8 individual warrants, addressing traffic volumes in various periods, pedestrian conditions, safety conditions and other specific factor. Of these warrants, the first to be metin typical conditions (such as at this location) is the "peak hour warrant." This warrant is based on the volume per hour of the major street (total of both approaches) and the volume per hour on the minor street higher volume approach. These volumes are plotted in a chart; if the plotted value is higher than the specified curve, the location meets the peak-hour warrant. As shown in Figure 2, the existing-plus- project volumes fall below the curve, indicating that a traffic signal is not warranted without or with the project.

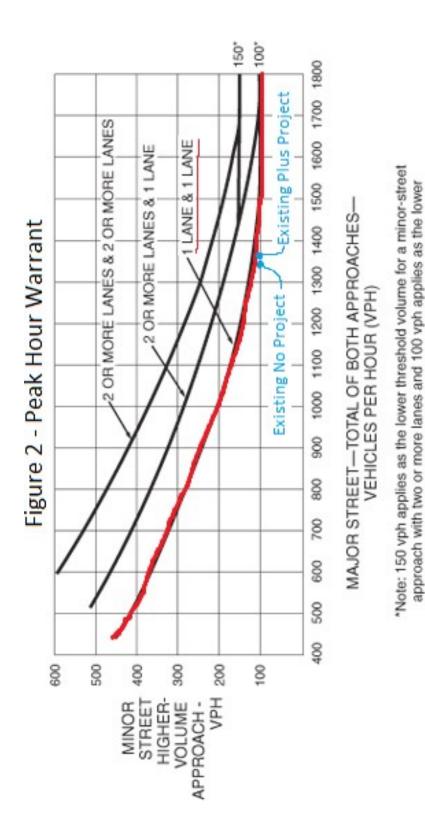
INTERSECTION LEVEL OF SERVICE (LOS)

The site driveway intersection and SR 28/Village operate at an acceptable LOS with the project. As such, no LOS mitigation is required for these intersections.

SR 28/Northwood Blvd/Southwood Blvd (East) operates at an unacceptable LOS F both with and withoutthe project. Even though a traffic signal would improve LOS, it is not warranted at this location.

Additionally, a roundabout would also improve LOS to acceptable levels. While a warrant system specific to roundabouts has not been developed, the signal warrants typically are used as a guideline, which would indicate that a roundabout is not warranted. A roundabout at this location would be an extensive and expensive project, particularly given the grades. In addition, drivers exiting the project onto Southwood and wishing to head west on SR 28 have the option, if they see a long northbound queue at the highway intersection, to make a right turn and access the highway via Village Boulevard. This tends tolimit the increase in delays. Another factor is that the proposed project's traffic would only increase total





threshold volume for a minor-street approach with one lane.



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volumes through the 28/Northwood/Southwood intersection by 0.8 percent. Given these factors, requiring installation of a roundabout would not be appropriate.

Another option for improving access would be to expand the northbound Southwood approach at SR 28 from the existing one-lane configuration. At present, drivers wishing to make a northbound right-turn movement are often behind drivers making the more difficult northbound through or northbound left movements. To evaluate the overall delay (measured in total vehicle-hours of delay) with an additional lane, LOS was evaluated assuming the additional lanes as shown in Table 7.

Table 7: SR 28/Northwood Blvd/Southwood Blvd Northbound Approach Delaywith Additional Lanes

	Northbound Lane	North	bound Volu Movement	•		bound De vement (s	, ,	Vehicle Hours of	% Change
Scenario	Configuration	Left	Through	Right	NBL	NBT	NBR	Delay	From Existin
	-				_			-	
Existing No Project	LTR	25	21	64		67.8		1.99	
Existing Plus Project	LTR	25	21	64		80.3		2.44	23%
Existing Plus Project	LT, R	25	21	64	101.7	101.7	14.7	1.54	-22%
Existing Plus Project	L, TR	25	21	64	87.7	28.2	28.2	1.27	-36%

This indicates the following:

- At present, northbound drivers in the peak hour experience a total of 1.99 vehicle-hours of delay.
- The additional traffic generated by the proposed project, with the existing single-lane northbound approach, would increase delay to 2.44 vehicle-hours (a 23 percent increase)
- If a right turn lane is provided (shared left/through and separate right turn lanes), total delaywould be 1.54 vehicle-hours of delay, or a 22 percent reduction from current delays.
- Alternatively, if a separate left turn lane is provided along with a shared through/right lane, totaldelay would be 1.27 vehicle-hours or 36 percent below existing levels.

As the right-of-way of Southwood Boulevard is 80 feet in width, this widening can occur within the existing right-ofway. It is therefore recommended that a separate northbound left-turn lane be provided.

SITE ACCESS PLANS

Driver sight distance conditions are evaluated at the site access point.

Driver Sight Distance

Driver sight distance was evaluated at the proposed access intersection. According to the NDOT Road Design Guide (2019), there are two types of sight distance standards that should be met at driveways or intersections for low-speed facilities (44 MPH or Less): stopping sight distance and intersection sight distance. Intersection sight distance



requirements are meant to ensure that adequate time is provided for the waiting driver at an unsignalized intersection or driveway to either cross all lanes of through traffic, cross the near lanes and turn left, or turn right, without requiring through traffic to radically alter their speed. Intersection sight distance requirements are based upon the need for a driver to discern a gap of up to 7.5 seconds in oncoming traffic to safely choose an adequate gap. The design intersection sight distance requirements are set forth in Table 9-7 of A Policy on Geometric Design of Highways and Streets (AASHTO Green Book, 2018).

Stopping sight distance is the distance an oncoming driver on the major roadway needs to perceive an object in the travel lane (such as a turning vehicle), react to the object, and come to a safe stop. Stopping sight distance requirement are set forth in the AASHTO Green Book.

LSC staff visited the site and determined the proposed driveway is expected to provide adequate driver stopping sight distance. For intersection sight distance, the Southwood site access is adequate so long as the final landscaping plans do not hinder the intersection sight distance.

Driveway Spacing

The proposed driveway spacing along Southwood Blvd was reviewed. Driveway spacing is adequate and no mitigation needs to be performed.

Site Access Summary

In summary, a review of the site access plans indicates the following:

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- 1. Driver sight distance is acceptable on Southwood Boulevard points so long as the final landscaping plans provide at least 440 feet of corner sight distance.
- 2. The proposed driveway spacing meets City standards.

VEHICLE MILES TRAVELED (VMT)

VMT analysis was conducted based on TRPA's "*TRPA Project Impact Assessment Guidelines*" (TRPA Draft, June 2021). This project is located in Project Impact Assessment Zone 69. The current project impact assessment process, based on daily vehicle trip ends (DVTE) identifies projects in town and regional centers that produce less than 200 DVTE:1,300 VMT as having an insignificant effect and so not requiring additional analysis." Because the project has less than the 200 DVTE requirement, the project is considered to have an insignificant effect. VMT is calculated but does not have to be considered against the standard of significance.

The projects VMT is calculated as the 'zone VMT per capita' multiplied by the 'zone persons per household' multiplied by the number of proposed units. As shown in Table 8, the resulting VMT from the residential units would total 850 VMT.

Table 8: Incline	Table 8: Incline Village Residential - VMT Analysis												
Тгір Туре	Zone VMT per Capita ¹	Zone Persons per Household	Number of Proposed Units	Average Annual Daily VMT									
Residential	9.24	2.30	40	850									
Note 1: TRPA zone VM Source: LSC Transportat													

CONCLUSIONS

- The project is forecasted to generate a total of approximately 174 one-way daily vehicle trips (DVTE) at the site driveways on a weekday, including 14 PM peak-hour vehicle-trips (9 inbound plus 5 outbound).
- The LOS at the site access driveway and SR 28/Village Blvd would remain acceptable with the project.
- The LOS at the SR 28/Northwood Blvd/Southwood Blvd intersection does not meet LOS standards without the project, which would be exacerbated by the proposed project. A review of improvement options indicates that total delay can be reduced from existing delays on the key northbound approach by providing a separate northbound left-turn lane. While delays exceeding the LOS standard will still occur, this will be an overall improvement from existing conditions.
- The proposed site access driveway spacing on Southwood Boulevard meets the City Standards.
- The proposed driveway on Southwood Boulevard is expected to provide adequate driver sight distance so long as the final landscaping plans do not hinder the corner sight distance.
- The project is exempt from a full VMT analysis and will generate about 850 total VMT.

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Appendix A LOS DESCRIPTIONS

DESCRIPTIONS OF LEVELS OF SERVICE

The concept of level of service is defined as a qualitative measure describing operational conditions within a traffic stream, and their perception by motorists and/or passengers. A level of service definition generally describes these conditions in terms of such factors as speed and travel time, freedom to maneuver, traffic interruptions, comfort and convenience, and safety. Six levels of service are defined for each type of facility for which analysis procedures are available. They are given letter designations, from A to F, with level of service A representing the best operating conditions and level of service F the worst.

Level of Service Definitions

In general, the various levels of service are defined as follows for uninterrupted flow facilities:

- Level of service A represents free flow. Individual users are virtually unaffected by the presence of others in the traffic stream. Freedom to select desired speeds and to maneuver within the traffic stream is extremely high. The general level of comfort and convenience provided to the motorist, passenger, or pedestrian is excellent.
- Level of service B is in the range of stable flow, but the presence of other users in the traffic stream begins to be noticeable. Freedom to select desired speeds is relatively unaffected, but there is a slight decline in the freedom to maneuver within the traffic stream from LOS A. The level of comfort and convenience provided is somewhat less than at LOS A, because the presence of others in the traffic stream begins to affect individual behavior.
- Level of service C is in the range of stable flow, but marks the beginning of the range of flow in which the operation of individual users becomes significantly affected by interactions with others in the traffic stream. The selection of speed is now affected by the presence of others, and maneuvering within the traffic stream requires substantial vigilance on the part of the user. The general level of comfort and convenience declines noticeably at this level.
- Level of Service D represents high-density, but stable, flow. Speed and freedom to maneuver are severely restricted, and the driver or pedestrian experiences a generally poor level of comfort and convenience. Small increases in traffic flow will generally cause operational problems at this level.
- Level of service E represents operating conditions at or near the capacity level. All speeds are reduced to a low, but relatively uniform value. Freedom to maneuver within the traffic stream is extremely difficult, and it is generally accomplished by forcing a vehicle or pedestrian to "give way" to accommodate such maneuvers. Comfort and convenience levels are extremely poor, and driver or pedestrian frustration is generally high. Operations at this level are usually unstable, because small increases in flow or minor perturbations within the traffic stream will cause breakdowns.
- Level of service F is used to define forced or breakdown flow. This condition exists wherever the amount of traffic approaching a point exceeds the amount which can traverse the point. Queues form behind such locations. Operations within the queue are characterized by stop-and-go waves, and they are extremely unstable. Vehicles may progress at reasonable speeds for several hundred feet or more, then be required to stop in a cyclic fashion. Level of service F is used to describe the operating conditions within the queue, as well as the point of the breakdown. It should be noted, however, that in many cases operating conditions of vehicles or pedestrians discharged from the queue may be quite good. Nevertheless, it is the point at which arrival flow exceeds discharge flow which causes the queue to form, and level of service F is an appropriate designation for such points.

Appendix B LOS OUTPUT

HCM 6th Signalized Intersection Summary 1: Village Blvd & SR 28

06/18/2021

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	- ኘ	ef 👘		- ሽ	- î>		- ሽ	ef 👘			ef 👘	
Traffic Volume (veh/h)	93	479	104	109	458	120	113	267	86	131	185	73
Future Volume (veh/h)	93	479	104	109	458	120	113	267	86	131	185	73
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach	1070	No	1070	1070	No	1070	4070	No	4070	4070	No	1070
Adj Sat Flow, veh/h/ln	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870
Adj Flow Rate, veh/h	101	521	113	118	498	130	123	290	93	142	201	79
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Percent Heavy Veh, %	2	2	2	2	2	2	2	2	2	2	2	2
Cap, veh/h	300	707	153	298	679	177	415	493	158	336	465	183
Arrive On Green	0.47	0.47	0.47	0.47	0.47	0.47	0.36	0.36	0.36	0.36	0.36	0.36
Sat Flow, veh/h	798	1489	323	793	1430	373	1099	1357	435	1000	1278	502
Grp Volume(v), veh/h	101	0	634	118	0	628	123	0	383	142	0	280
Grp Sat Flow(s),veh/h/ln	798	0	1812	793	0	1803	1099	0	1792	1000	0	1780
Q Serve(g_s), s	5.8	0.0	14.0	7.0	0.0	13.9	4.7	0.0	8.6	6.6	0.0	5.9
Cycle Q Clear(g_c), s	19.7	0.0	14.0	21.0	0.0	13.9	10.6	0.0	8.6	15.2	0.0	5.9
Prop In Lane	1.00	0	0.18	1.00	•	0.21	1.00	•	0.24	1.00	0	0.28
Lane Grp Cap(c), veh/h	300	0	860	298	0	856	415	0	652	336	0	647
V/C Ratio(X)	0.34	0.00	0.74	0.40	0.00	0.73	0.30	0.00	0.59	0.42	0.00	0.43
Avail Cap(c_a), veh/h	308	0	879	306	0	874	415	0	652	336	0	647
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	0.00	1.00	1.00	0.00	1.00	1.00	0.00	1.00	1.00	0.00	1.00
Uniform Delay (d), s/veh	18.4 0.7	0.0	10.5 3.2	19.0 0.9	0.0 0.0	10.5 3.2	15.9 1.8	0.0 0.0	12.7 3.9	18.9 0.8	0.0 0.0	11.9
Incr Delay (d2), s/veh	0.7	0.0 0.0	0.0	0.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.5 0.0
Initial Q Delay(d3),s/veh %ile BackOfQ(50%),veh/In	1.0	0.0	4.8	1.2	0.0	4.7	1.3	0.0	3.7	1.5	0.0	2.1
Unsig. Movement Delay, s/veh		0.0	4.0	1.2	0.0	4./	1.5	0.0	3.1	1.5	0.0	Ζ.Ι
LnGrp Delay(d),s/veh	19.1	0.0	13.7	19.8	0.0	13.6	17.7	0.0	16.6	19.7	0.0	12.3
LIGIP Delay(d), siven	B	0.0 A	13.7 B	19.0 B	0.0 A	13.0 B	В	0.0 A	10.0 B	19.7 B	0.0 A	12.3 B
Approach Vol, veh/h	D	735	D	В	746	D	Ь	506	D	D	422	
Approach Delay, s/veh		14.5			14.6			16.9			422	
Approach LOS		14.5 B			14.0 B			10.9 B			14.0 B	
Approach LOS					D						D	
Timer - Assigned Phs		2		4		6		8				
Phs Duration (G+Y+Rc), s		22.0		27.5		22.0		27.5				
Change Period (Y+Rc), s		4.0		4.0		4.0		4.0				
Max Green Setting (Gmax), s		18.0		24.0		18.0		24.0				
Max Q Clear Time (g_c+I1), s		12.6		21.7		17.2		23.0				
Green Ext Time (p_c), s		1.4		1.1		0.2		0.5				
Intersection Summary												
HCM 6th Ctrl Delay			15.1									
HCM 6th LOS			В									

Intersection Int Delay, s/veh 10.6 EBL EBT EBR WBL WBT WBR NBL NBT NBR SBL SBT SBR Movement **4** 21 **4** 15 Lane Configurations ኘ Þ ٦ ₽ Traffic Vol, veh/h 44 611 63 40 561 27 22 63 29 39 Future Vol, veh/h 44 611 63 40 561 27 22 21 63 29 15 39 Conflicting Peds, #/hr 0 0 0 0 0 0 0 0 0 0 0 0 Sign Control Stop Free Free Free Free Free Free Stop Stop Stop Stop Stop RT Channelized -None _ None None None --_ _ --Storage Length 150 150 --------_ -Veh in Median Storage, # -0 0 _ _ 0 _ _ 0 ---Grade, % 0 0 0 0 --------Peak Hour Factor 92 92 92 92 92 92 92 92 92 92 92 92 Heavy Vehicles, % 2 2 2 2 2 2 2 2 2 2 2 2 Mvmt Flow 48 664 68 43 610 29 24 23 68 32 16 42

Major/Minor	Major1			Major2			Minor1			Minor2				
Conflicting Flow All	639	0	0	732	0	0	1534	1519	698	1551	1539	625		
Stage 1	-	-	-	-	-	-	794	794	-	711	711	-		
Stage 2	-	-	-	-	-	-	740	725	-	840	828	-		
Critical Hdwy	4.12	-	-	4.12	-	-	7.12	6.52	6.22	7.12	6.52	6.22		
Critical Hdwy Stg 1	-	-	-	-	-	-	6.12	5.52	-	6.12	5.52	-		
Critical Hdwy Stg 2	-	-	-	-	-	-	6.12	5.52	-	6.12	5.52	-		
Follow-up Hdwy	2.218	-	-	2.218	-	-	3.518	4.018	3.318	3.518	4.018	3.318		
Pot Cap-1 Maneuver	945	-	-	873	-	-	95	119	440	92	116	485		
Stage 1	-	-	-	-	-	-	381	400	-	424	436	-		
Stage 2	-	-	-	-	-	-	409	430	-	360	386	-		
Platoon blocked, %		-	-		-	-								
Mov Cap-1 Maneuver	945	-	-	873	-	-	71	107	440	60	105	485		
Mov Cap-2 Maneuver	-	-	-	-	-	-	71	107	-	60	105	-		
Stage 1	-	-	-	-	-	-	362	380	-	402	415	-		
Stage 2	-	-	-	-	-	-	341	409	-	271	366	-		
Approach	EB			WB			NB			SB				
HCM Control Delay, s	0.6			0.6			67.8			99.7				
HCM LOS							F			F				
Minor Lane/Major Mvn	nt	NBLn1	EBL	EBT	EBR	WBL	WBT	WBR	SBLn1					
Capacity (veh/h)		163	945	-	-	873	-	-	117					
HCM Lane V/C Ratio		0.707	0.051	-	-	0.05	-	-	0.771					
HCM Control Delay (s))	67.8	9	-	-	9.3	-	-	99.7					
		г	٨			٨			_					

 HCM Control Delay (s)
 F
 A
 S.S
 S.S

 HCM Lane LOS
 F
 A
 A
 F

 HCM 95th %tile Q(veh)
 4.2
 0.2
 0.2
 4.4

Intersection

Int Delay, s/veh	0					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	Y			ب ا	et –	
Traffic Vol, veh/h	0	0	0	105	118	0
Future Vol, veh/h	0	0	0	105	118	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage	,# 0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	0	0	114	128	0

Major/Minor	Minor2		Major1	Ма	jor2	
Conflicting Flow All	242	128	128	0	-	0
Stage 1	128	-	-	-	-	-
Stage 2	114	-	-	-	-	-
Critical Hdwy	6.42	6.22	4.12	-	-	-
Critical Hdwy Stg 1	5.42	-	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-	-	-	-
Follow-up Hdwy	3.518	3.318	2.218	-	-	-
Pot Cap-1 Maneuver	746	922	1458	-	-	-
Stage 1	898	-	-	-	-	-
Stage 2	911	-	-	-	-	-
Platoon blocked, %				-	-	-
Mov Cap-1 Maneuver	746	922	1458	-	-	-
Mov Cap-2 Maneuver	746	-	-	-	-	-
Stage 1	898	-	-	-	-	-
Stage 2	911	-	-	-	-	-
Approach	EB		NB		SB	
HCM Control Delay, s	0		0		0	

HCM LOS А

Minor Lane/Major Mvmt	NBL	NBT EE	3Ln1	SBT	SBR
Capacity (veh/h)	1458	-	-	-	-
HCM Lane V/C Ratio	-	-	-	-	-
HCM Control Delay (s)	0	-	0	-	-
HCM Lane LOS	А	-	А	-	-
HCM 95th %tile Q(veh)	0	-	-	-	-

HCM 6th Signalized Intersection Summary 1: Village Blvd & SR 28

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	<u>۲</u>	ef 👘		<u>۲</u>	ef 👘		<u> </u>	ef 👘		- ሽ	ef 👘	
Traffic Volume (veh/h)	93	482	104	109	460	120	113	267	86	131	185	73
Future Volume (veh/h)	93	482	104	109	460	120	113	267	86	131	185	73
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870
Adj Flow Rate, veh/h	101	524	113	118	500	130	123	290	93	142	201	79
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Percent Heavy Veh, %	2	2	2	2	2	2	2	2	2	2	2	2
Cap, veh/h	300	709	153	297	681	177	414	493	158	335	464	182
Arrive On Green	0.48	0.48	0.48	0.48	0.48	0.48	0.36	0.36	0.36	0.36	0.36	0.36
Sat Flow, veh/h	796	1491	322	791	1431	372	1099	1357	435	1000	1278	502
Grp Volume(v), veh/h	101	0	637	118	0	630	123	0	383	142	0	280
Grp Sat Flow(s),veh/h/ln	796	0	1812	791	0	1803	1099	0	1792	1000	0	1780
Q Serve(g_s), s	5.8	0.0	14.1	7.0	0.0	14.0	4.7	0.0	8.6	6.6	0.0	5.9
Cycle Q Clear(g_c), s	19.8	0.0	14.1	21.1	0.0	14.0	10.6	0.0	8.6	15.2	0.0	5.9
Prop In Lane	1.00		0.18	1.00		0.21	1.00		0.24	1.00		0.28
Lane Grp Cap(c), veh/h	300	0	862	297	0	857	414	0	651	335	0	646
V/C Ratio(X)	0.34	0.00	0.74	0.40	0.00	0.73	0.30	0.00	0.59	0.42	0.00	0.43
Avail Cap(c_a), veh/h	307	0	878	303	0	873	414	0	651	335	0	646
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	0.00	1.00	1.00	0.00	1.00	1.00	0.00	1.00	1.00	0.00	1.00
Uniform Delay (d), s/veh	18.4	0.0	10.5	19.1	0.0	10.5	15.9	0.0	12.8	19.0	0.0	11.9
Incr Delay (d2), s/veh	0.7	0.0	3.3	0.9	0.0	3.2	1.8	0.0	3.9	0.8	0.0	0.5
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/In	1.0	0.0	4.8	1.2	0.0	4.7	1.3	0.0	3.7	1.5	0.0	2.1
Unsig. Movement Delay, s/veh												
LnGrp Delay(d),s/veh	19.1	0.0	13.8	19.9	0.0	13.7	17.8	0.0	16.7	19.8	0.0	12.4
LnGrp LOS	В	А	В	В	А	В	В	А	В	В	А	<u> </u>
Approach Vol, veh/h		738			748			506			422	
Approach Delay, s/veh		14.5			14.7			16.9			14.9	
Approach LOS		В			В			В			В	
Timer - Assigned Phs		2		4		6		8				
Phs Duration (G+Y+Rc), s		22.0		27.6		22.0		27.6				
Change Period (Y+Rc), s		4.0		4.0		4.0		4.0				
Max Green Setting (Gmax), s		18.0		24.0		18.0		24.0				
Max Q Clear Time (g_c+I1), s		12.6		21.8		17.2		23.1				
Green Ext Time (p_c), s		1.4		1.1		0.2		0.5				
Intersection Summary												
HCM 6th Ctrl Delay			15.1									
HCM 6th LOS			В									

Intersection Int Delay, s/veh 11.9 EBL EBT EBR WBL WBT WBR NBL NBT NBR SBL SBT SBR Movement **4** 16 **₽** 21 Lane Configurations ኘ Þ ٦ ₽ 561 Traffic Vol, veh/h 44 611 68 42 27 25 64 29 39 Future Vol, veh/h 44 611 68 42 561 27 25 21 64 29 16 39 Conflicting Peds, #/hr 0 0 0 0 0 0 0 0 0 0 0 0 Sign Control Stop Stop Free Free Free Free Free Free Stop Stop Stop Stop RT Channelized -None _ None None None ------Storage Length 150 150 --------_ -Veh in Median Storage, # -0 0 --0 _ -0 ---Grade, % 0 0 0 0 --------Peak Hour Factor 92 92 92 92 92 92 92 92 92 92 92 92 Heavy Vehicles, % 2 2 2 2 2 2 2 2 2 2 2 2 Mvmt Flow 48 664 74 46 610 29 27 23 70 32 17 42

Major/Minor	Major1		1	Major2		l	Minor1		l	Minor2			
Conflicting Flow All	639	0	0	738	0	0	1543	1528	701	1561	1551	625	
Stage 1	-	-	-	-	-	-	797	797	-	717	717	-	
Stage 2	-	-	-	-	-	-	746	731	-	844	834	-	
Critical Hdwy	4.12	-	-	4.12	-	-	7.12	6.52	6.22	7.12	6.52	6.22	
Critical Hdwy Stg 1	-	-	-	-	-	-	6.12	5.52	-	6.12	5.52	-	
Critical Hdwy Stg 2	-	-	-	-	-	-	6.12	5.52	-	6.12	5.52	-	
Follow-up Hdwy	2.218	-	-	2.218	-	-	3.518	4.018	3.318	3.518	4.018	3.318	
Pot Cap-1 Maneuver	945	-	-	868	-	-	94	117	439	91	114	485	
Stage 1	-	-	-	-	-	-	380	399	-	421	434	-	
Stage 2	-	-	-	-	-	-	405	427	-	358	383	-	
Platoon blocked, %		-	-		-	-							
Mov Cap-1 Maneuver	945	-	-	868	-	-	69	105	439	59	102	485	
Mov Cap-2 Maneuver	-	-	-	-	-	-	69	105	-	59	102	-	
Stage 1	-	-	-	-	-	-	361	379	-	400	411	-	
Stage 2	-	-	-	-	-	-	335	404	-	269	363	-	
Approach	EB			WB			NB			SB			
HCM Control Delay, s	0.5			0.6			80.3			105.4			
HCM LOS							F			F			
Minor Lane/Major Mvm	nt	NBLn1	EBL	EBT	EBR	WBL	WBT	WBR	SBLn1				
Capacity (veh/h)		155	945	-	-	868	-	-	115				
HCM Lane V/C Ratio		0.771	0.051	-	-	0.053	-	-	0.794				
HCM Control Delay (s))	80.3	9	-	-	9.4	-	-	105.4				

HCM Control Delay (s)	80.3	9	-	-	9.4	-	-	105.4	
HCM Lane LOS	F	А	-	-	А	-	-	F	
HCM 95th %tile Q(veh)	4.8	0.2	-	-	0.2	-	-	4.6	

Intersection

Int Delay, s/veh	0.2					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	Y			ب ا	et 👘	
Traffic Vol, veh/h	4	1	1	105	118	8
Future Vol, veh/h	4	1	1	105	118	8
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage	,# 0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	4	1	1	114	128	9

Major/Minor	Minor2	l	Major1	Ma	ajor2	
Conflicting Flow All	249	133	137	0	-	0
Stage 1	133	-	-	-	-	-
Stage 2	116	-	-	-	-	-
Critical Hdwy	6.42	6.22	4.12	-	-	-
Critical Hdwy Stg 1	5.42	-	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-	-	-	-
Follow-up Hdwy	3.518	3.318	2.218	-	-	-
Pot Cap-1 Maneuver	739	916	1447	-	-	-
Stage 1	893	-	-	-	-	-
Stage 2	909	-	-	-	-	-
Platoon blocked, %				-	-	-
Mov Cap-1 Maneuver	738	916	1447	-	-	-
Mov Cap-2 Maneuver	738	-	-	-	-	-
Stage 1	892	-	-	-	-	-
Stage 2	909	-	-	-	-	-
Approach	FB		NR		SB	

Approach	EB	NB	SB	
HCM Control Delay, s	9.7	0.1	0	
HCM LOS	А			

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	SBT	SBR
Capacity (veh/h)	1447	-	768	-	-
HCM Lane V/C Ratio	0.001	-	0.007	-	-
HCM Control Delay (s)	7.5	0	9.7	-	-
HCM Lane LOS	А	А	Α	-	-
HCM 95th %tile Q(veh)	0	-	0	-	-

9.8

Intersection

Int Delay, s/veh

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations	٦	4		۲	4			र्स	1	•	4	•===	
Traffic Vol, veh/h	44	611	68	42	561	27	25	21	64	29	16	39	
Future Vol, veh/h	44	611	68	42	561	27	25	21	64	29	16	39	
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop	
RT Channelized	-	-	None										
Storage Length	150	-	-	150	-	-	-	-	150	-	-	-	
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	-	0	-	
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-	
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92	
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2	
Mvmt Flow	48	664	74	46	610	29	27	23	70	32	17	42	

Major/Minor	Major1			Major2			Minor1			Mi	nor2	nor2
Conflicting Flow All	639			738	0	0	1543	1528	701	156	51	1 1551
Stage 1	-	· -	-	-	-	-	797	797	-	717		717
Stage 2	-	· -	-	-	-	-	746	731	-	844		834
Critical Hdwy	4.12	-	-	4.12	-	-	7.12	6.52	6.22	7.12		6.52
Critical Hdwy Stg 1	-	· -	-	-	-	-	6.12	5.52	-	6.12		5.52
Critical Hdwy Stg 2	-	· -	-	-	-	-	6.12	5.52	-	6.12	Ę	5.52
Follow-up Hdwy	2.218	-	-	2.218	-	-	3.518	4.018	3.318	3.518	4.0)18
Pot Cap-1 Maneuver	945	-	-	868	-	-	94	117	439	91	11	4
Stage 1	-		-	-	-	-	380	399	-	421	434	ŀ
Stage 2	-	· -	-	-	-	-	405	427	-	358	383	
Platoon blocked, %		-	-		-	-						
Mov Cap-1 Maneuver		-	-	868	-	-	69	105	439	59	102	
Mov Cap-2 Maneuver			-	-	-	-	69	105	-	59	102	
Stage 1	-	· -	-	-	-	-	361	379	-	400	411	
Stage 2	-	· -	-	-	-	-	335	404	-	269	363	
Approach	EB			WB			NB			SB		
HCM Control Delay, s	s 0.5			0.6			51.1			105.4		
HCM LOS							F			F		
Minor Lane/Major Mvi	mt	NBLn1	NBLn2	EBL	EBT	EBR	WBL	WBT	WBR	SBLn1		
Capacity (veh/h)		82	439	945	-	-	868	-	-	115		
HCM Lane V/C Ratio		0.61	0.158	0.051	-	-	0.053	-	-	0.794		
HCM Control Delay (s	5)	101.7	14.7	9	-	-	9.4	-	-	105.4		
HCM Lane LOS		F	В	А	-	-	А	-	-	F		
HCM 95th %tile Q(vel	h)	2.8	0.6	0.2			0.2			4.6		

9.2

Intersection

Int Delay, s/veh

HCM 95th %tile Q(veh)

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations	k			K		WDIX	K		HDR	ODL		OBIC	
Ū.		•	<u></u>	40	For a	07		1	C 4	00	4 }	20	
Traffic Vol, veh/h	44	611	68	42	561	27	25	21	64	29	16	39	
Future Vol, veh/h	44	611	68	42	561	27	25	21	64	29	16	39	
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop	
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None	
Storage Length	150	-	-	150	-	-	150	-	-	-	-	-	
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	-	0	-	
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-	
Peak Hour Factor	92	92	92	92	92	92	92	92	92	92	92	92	
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2	
Mvmt Flow	48	664	74	46	610	29	27	23	70	32	17	42	

Major/Minor	Major1			Major2			Minor1			Minor2			
Conflicting Flow All	639	0	0	738	0	0	1543	1528	701	1561	1551	625	
Stage 1	-	-	-	-	-	-	797	797	-	717	717	-	
Stage 2	-	-	-	-	-	-	746	731	-	844	834	-	
Critical Hdwy	4.12	-	-	4.12	-	-	7.12	6.52	6.22	7.12	6.52	6.22	
Critical Hdwy Stg 1	-	-	-	-	-	-	6.12	5.52	-	6.12	5.52	-	
Critical Hdwy Stg 2	-	-	-	-	-	-	6.12	5.52	-	6.12	5.52	-	
Follow-up Hdwy	2.218	-	-	2.218	-	-	3.518	4.018	3.318	3.518	4.018	3.318	
Pot Cap-1 Maneuver	945	-	-	868	-	-	94	117	439	91	114	485	
Stage 1	-	-	-	-	-	-	380	399	-	421	434	-	
Stage 2	-	-	-	-	-	-	405	427	-	358	383	-	
Platoon blocked, %		-	-		-	-							
Mov Cap-1 Maneuver	945	-	-	868	-	-	69	105	439	59	102	485	
Mov Cap-2 Maneuver	-	-	-	-	-	-	69	105	-	59	102	-	
Stage 1	-	-	-	-	-	-	361	379	-	400	411	-	
Stage 2	-	-	-	-	-	-	335	404	-	269	363	-	
Approach	EB			WB			NB			SB			
HCM Control Delay, s	0.5			0.6			41.7			105.4			
HCM LOS							E			F			
Minor Lane/Major Mvn	nt	NBLn1	NBLn2	EBL	EBT	EBR	WBL	WBT	WBR	SBLn1			
Capacity (veh/h)		69	246	945	-	-	868	-	-	115			
HCM Lane V/C Ratio		0.394	0.376	0.051	-	-	0.053	-	-	0.794			
HCM Control Delay (s))	87.7	28.2	9	-	-	9.4	-		105.4			
HCM Lane LOS		F	D	A	-	-	A	-	-	F			

0.2

-

4.6

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1.7

0.2

1.5



MEMORANDUM

Date:	1/09/2023
To:	Collaborative Design Studio
From:	Mary Horvath, PE
Subject:	947 Tahoe Boulevard Proposed Infiltration Facilities

The 947 Tahoe Boulevard development is going to include approximately 58,000 square feet of impervious area which will generate a volume of 4,800 cubic feet of runoff in the 20-year, 1-hour storm event (1-inch of precipitation depth). The preliminary design includes underground storage/infiltration with a total treatment capacity of approximately 7,200 cubic feet. The infiltration facilities will be 24" or 30" High Density Polyethylene (HDPE) perforated pipe within drain rock galleries that will lie beneath the driveways and landscaped portions of the site.

Figure 1 shows the preliminary drainage of the site to four infiltration galleries:

- A within the southern driveway (South Gallery)
- B within a landscape area near the west side of the development (West Gallery)
- C within the landscaped portion of the site along the eastern boundary (East Gallery)
- D a small crossroad trench at the eastern exit of the site (Transverse Drain)

The TRPA BMP Calculation Spreadsheet is attached showing the volume of runoff compared to the volume of the proposed infiltration galleries. The BMP void calculator is also included.

The grading and drainage design sheets as well as the infiltration gallery details are attached.

Reno, NV 1885 S. Arlington Ave., Suite 111 Reno, NV 89509 (775) 329-4955

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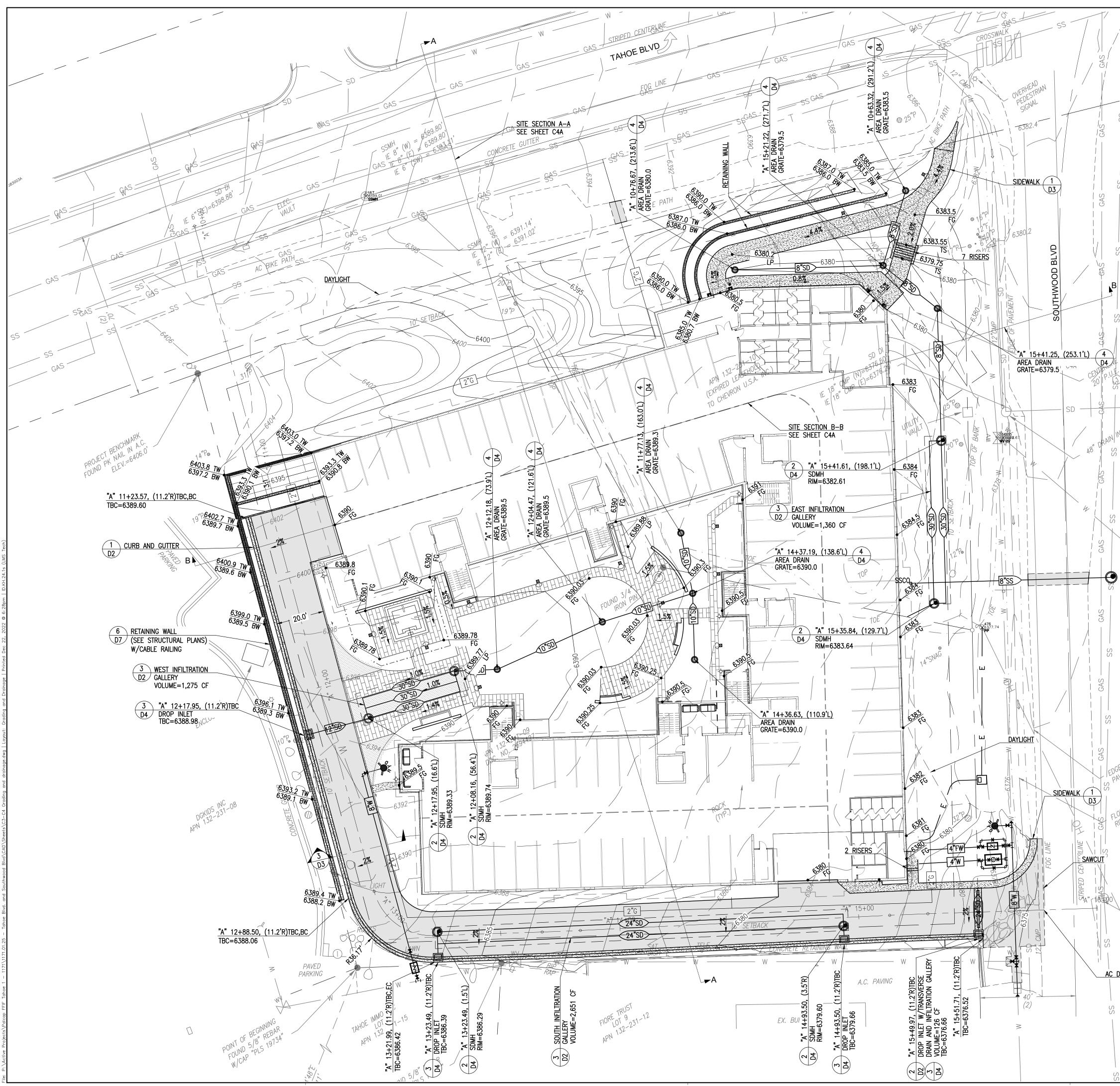
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Contributing Surface	A 0	B West	C East	D T.D.	1	1			1	1		1	_	1		1			
Contributing Surface # of Stories	A South	0		0											т				т
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Area (ft2) Area (ft ²)	27829 27829	13426 13426	15090 15090	1432 1432	0	0	0	0	0	0	0		0	0	1		0	0	I
Runoff (ft ³)		1118.8	1257.5	119.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0		0.0	0.0	0.0
Treatment Label:	Α	В	С	D											-				
Length (ft.) Width (in.)	174.3 112	45.0 166	70.5 114	16.0 48											-				
Depth (in.)	40	48	48	40															
On-Site Ksat (ⁱⁿ / _{hr})																			
mapped Ksat (ⁱⁿ / _{hr}) Prefab Void Space (%)	4.0	4.0 100%	4.0 100%	4.0 100%	4.0	4.0	4.0	4.0	4.0	4.0	4.0		4.0	4.0			4.0	4.0	
Average Void Space (%)	56%	52%	56%	52%															
Effective Volume (yd ³)	200.6	92.4	99.2	9.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	-		0.0	0.0	
Treatment Capacity (ft ³)		1543.2	1783.9	168.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	-	0.0	0.0	0.0
Drain Rock Quantity (yd ³) Excess Runoff (ft ³)	147.1 0.0	73.9 0.0	72.8 0.0	7.6 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0		0.0	0.0	0.0		0.0	0.0	0.0
Excess Capacity (ft ³)		424.4	526.4	49.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0				0.0			-	0.0
				ī		1	1				1	-		1		-			
Contributing Surface # of Stories			т					т					т						т
Length (ft.)			0					0					0						0
Width (ft.)			t a					t a					t a						t a
Area (ft2)	0	0	1		0	0	0	I		0	0	0	1		0	0	0	0	Т
Area (ft ²) Runoff (ft ³)	0.0	0.0	0.0		0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0
Treatment Label:				1															
Length (ft.)													-						
Width (in.) Depth (in.)													-						
On-Site Ksat (ⁱⁿ / _{hr})																			
mapped Ksat (ⁱⁿ / _{hr})	4.0	4.0			4.0	4.0	4.0			4.0	4.0	4.0			4.0	4.0	4.0	4.0	
Prefab Void Space (%) Average Void Space (%)													-						
Effective Volume (yd ³)	0.0	0.0	-		0.0	0.0	0.0			0.0	0.0	0.0	-		0.0	0.0	0.0	0.0	
Treatment Capacity (ft ³)	0.0	0.0	0.0		0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0
Drain Rock Quantity (yd ³) Excess Runoff (ft ³)	0.0	0.0	0.0		0.0	0.0	0.0	0.0 0.0		0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0
Excess Capacity (ft ³)			0.0	1				0.0					0.0					-	0.0
			Basin						•					NI.	otes				
	2:1 (1	rock lined	d or vege		I	5:1 (ma	wable)							IN	oles				
Contributing Surface																			
Length (ft.)																			
Width (ft.) Area (ft2)																			
Area (ft ²)	0	0	0	0	0	0	0	0											
Runoff (ft ³)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0											
T (() ()																			
Treatment Label: Top Length (ft.)																			
Treatment Label: Top Length (ft.) Top Width (ft.)																			
Top Length (ft.) Top Width (ft.) Depth (in.)																			
Top Length (ft.) Top Width (ft.) Depth (in.) Bottom Length (ft.)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0											
Top Length (ft.) Top Width (ft.) Depth (in.)	0.0	0.0 0.0 0.0	0.0 0.0 0.0	0.0 0.0 0.0	0.0 0.0 0.0	0.0 0.0 0.0	0.0 0.0 0.0	0.0 0.0 0.0											
Top Length (ft.) Top Width (ft.) Depth (in.) Bottom Length (ft.) Bottom Width (ft.) Volume (yd ³) On-Site Ksat	0.0	0.0	0.0	0.0	0.0	0.0	0.0 0.0	0.0											
Top Length (ft.) Top Width (ft.) Depth (in.) Bottom Length (ft.) Bottom Width (ft.) Volume (yd ³) On-Site Ksat Mapped Ksat	0.0 0.0 4.0	0.0 0.0 4.0	0.0 0.0 4.0	0.0 0.0 4.0	0.0 0.0 4.0	0.0 0.0 4.0	0.0 0.0 4.0	0.0 0.0 4.0											
Top Length (ft.) Top Width (ft.) Depth (in.) Bottom Length (ft.) Bottom Width (ft.) Volume (yd ³) On-Site Ksat Mapped Ksat Treatment Capacity (ft ³)	0.0 0.0 4.0 0.0	0.0 0.0 4.0 0.0	0.0 0.0 4.0 0.0	0.0 0.0 4.0 0.0	0.0 0.0 4.0 0.0	0.0 0.0 4.0 0.0	0.0 0.0 4.0 0.0	0.0 0.0 4.0 0.0											
Top Length (ft.) Top Width (ft.) Depth (in.) Bottom Length (ft.) Bottom Width (ft.) Volume (yd ³) On-Site Ksat Mapped Ksat	0.0 0.0 4.0 0.0	0.0 0.0 4.0	0.0 0.0 4.0	0.0 0.0 4.0	0.0 0.0 4.0	0.0 0.0 4.0	0.0 0.0 4.0	0.0 0.0 4.0											
Top Length (ft.) Top Width (ft.) Depth (in.) Bottom Length (ft.) Bottom Width (ft.) Volume (yd ³) On-Site Ksat Mapped Ksat Treatment Capacity (ft ³) Excess Runoff (ft ³)	0.0 0.0 4.0 0.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0 0.0	Troatm	onte					Review	ver Coi	mments	;	
Top Length (ft.) Top Width (ft.) Depth (in.) Bottom Length (ft.) Bottom Width (ft.) Volume (yd ³) On-Site Ksat Mapped Ksat Treatment Capacity (ft ³) Excess Runoff (ft ³)	0.0 0.0 4.0 0.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0 0.0 rce Co	0.0 0.0 4.0 0.0 0.0	reatm	ents					Review	ver Con	mments	3	
Top Length (ft.) Top Width (ft.) Depth (in.) Bottom Length (ft.) Bottom Width (ft.) Volume (yd ³) On-Site Ksat Mapped Ksat Treatment Capacity (ft ³) Excess Runoff (ft ³) Excess Capacity (ft ⁴) Deck Tree Deck Label Area (ft2)	0.0 0.0 4.0 0.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0 0.0 A	0.0 0.0 4.0 0.0 0.0 0.0 SOU rea Label Area (ft2)	0.0 0.0 4.0 0.0 0.0 0.0 rce Co	0.0 0.0 4.0 0.0 0.0 0.0	reatm	ents					Review	ver Cor	mments	3	
Top Length (ft.) Top Width (ft.) Depth (in.) Bottom Length (ft.) Bottom Width (ft.) Volume (yd ³) On-Site Ksat Mapped Ksat Treatment Capacity (ft ³) Excess Runoff (ft ³) Excess Capacity (ft ³) Deck Tree Deck Label Area (ft2) Slope (%)	0.0 0.0 4.0 0.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0 0.0 A	0.0 0.0 4.0 0.0 0.0 0.0 0.0 Sou rea Label Area (ft2) Slope (%)	0.0 0.0 4.0 0.0 0.0 0.0 rce Co	0.0 0.0 4.0 0.0 0.0 0.0	Freatm	ents					Review	ver Cor	mments	3	
Top Length (ft.) Top Width (ft.) Depth (in.) Bottom Length (ft.) Bottom Width (ft.) Volume (yd ³) On-Site Ksat Mapped Ksat Treatment Capacity (ft ³) Excess Runoff (ft ³) Excess Capacity (ft ⁴) Deck Tree Deck Label Area (ft2)	0.0 0.0 4.0 0.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0	0.0 0.0 4.0 0.0 0.0 0.0 A	0.0 0.0 4.0 0.0 0.0 0.0 SOU rea Label Area (ft2)	0.0 0.0 4.0 0.0 0.0 0.0 rce Co	0.0 0.0 4.0 0.0 0.0 0.0	<u>reatm</u>	ents					Review	ver Cor	mments	5	

 Gravel Treatment Width (ft.)
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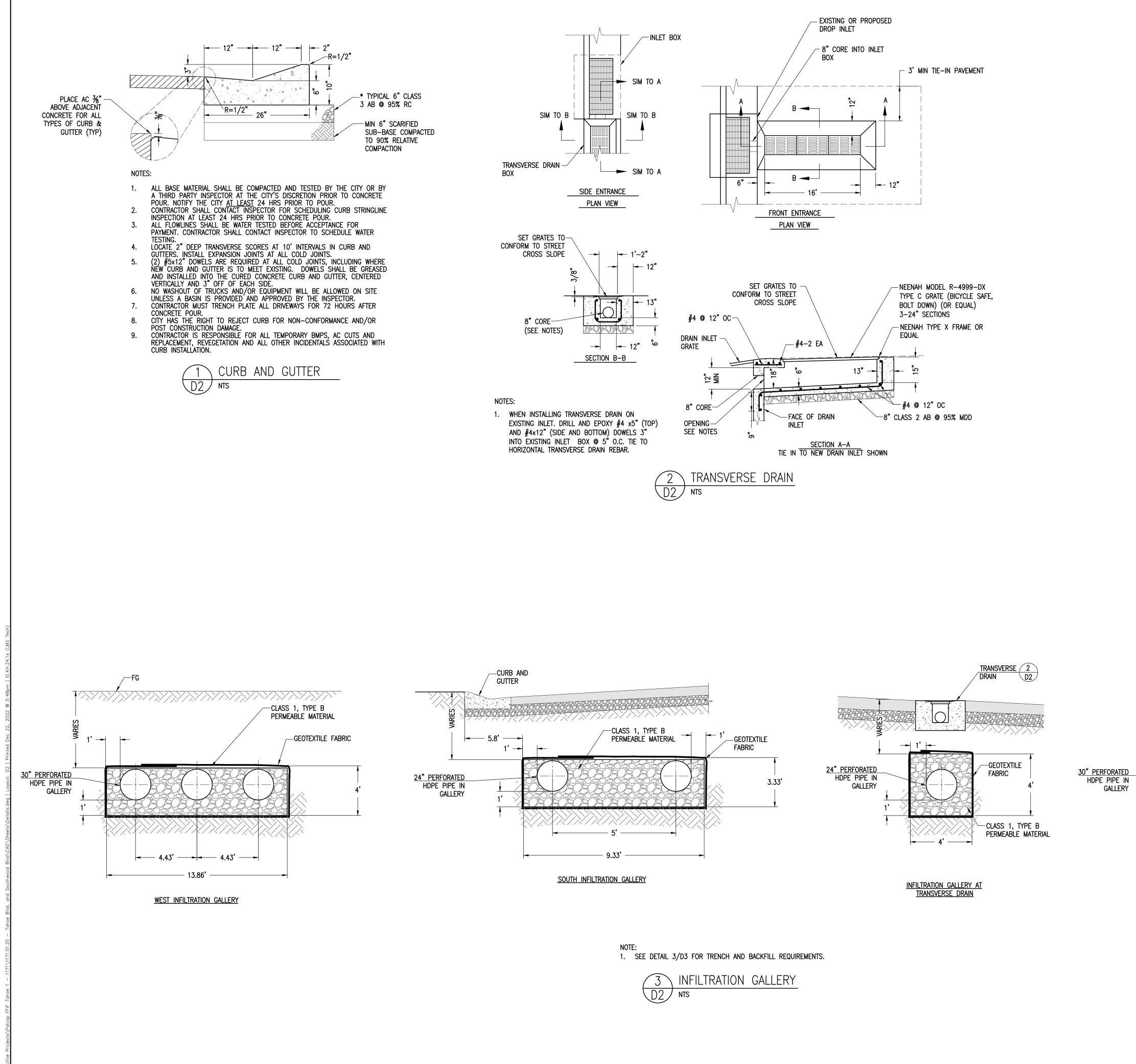
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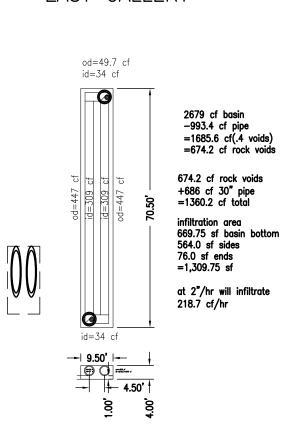
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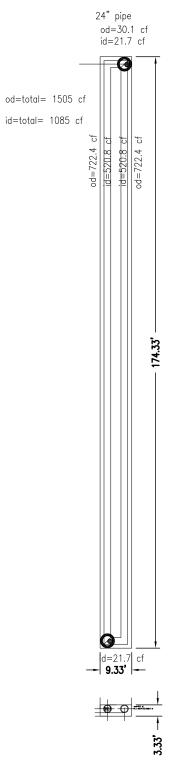


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EAST GALLERY

SOUTH GALLERY



5420.7 cf basin -1505 cf pipe =3915.7 cf(.4 voids) =1566.3 cf rock voids

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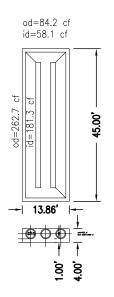
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at 2"/hr will infiltrate 476 cf/hr

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30" pipe



2493 cf basin -956.5 cf pipe =1536.5 cf(.4 voids) =614.6 cf rock voids 614.6 cf rock voids +660.1 cf 30° pipe =1275 cf total need 1114 infiltration area 669.75 sf basin bottom 564.0 sf sides 76.0 sf ends =1,309.75 sf at 2°/hr will infiltrate 218.7 cf/hr

NTITY INFORMATION			
Entity Name:	PAL CAP FFIF TAHOE 1, LLC	Entity Number:	E9511692020-1
Entity Type:	Domestic Limited-Liability Company (86)	Entity Status:	Active
Formation Date:	10/01/2020	NV Business ID:	NV20201906691
Termination Date:	Perpetual	Annual Report Due Date:	10/31/2022
Series LLC:		Restricted LLC:	
EGISTERED AGENT INF Name of Individual or Legal Entity:	INCLINE LAW GROUP, LLP	Status:	Active
	INCLINE LAW GROUP, LLP	Status:	Active
CRA Agent Entity Type:		Registered Agent Type:	Commercial Registered Agent
Туре:	NV20131679505	Registered Agent Type: Office or Position:	Commercial Registered Agent
Туре:			Commercial Registered Agent
Type: NV Business ID: Jurisdiction:			Commercial Registered Agent
Type: NV Business ID: Jurisdiction:	NEVADA 264 VILLAGE BLVD STE 104,		Commercial Registered Agent
Type: NV Business ID: Jurisdiction: Street Address:	NEVADA 264 VILLAGE BLVD STE 104,		Commercial Registered Agent

OFFICER INFORMATION

□ VIEW HISTORICAL DATA

Title	Name	Address	Last Updated	Status
Manager	Randall Fleisher	8333 Douglas Ave #900, Dallas, TX, 75225, USA	04/14/2021	Active
Manager	Charles L. Butler, II	8333 Douglas Ave #900, Dallas, TX, 75225, USA	04/14/2021	Active

Page 1 of 1, records 1 to 2 of 2



Consulting Civil Engineers P.O. Box 18449 Reno, Nevada 89511 PH (775) 853-9100 FAX (775) 853-9199

September 7, 2021 Project No. 21073.001

Tahoe Regional Planning Agency 128 Market Street Stateline, Nevada 89449

Subject: Soils/Hydrologic Scoping Report Proposed Condominium Complex 941 and 947 Tahoe Boulevard Incline Village, Washoe County, Nevada (APN's: 132-231-09 and 132-231-10)

Dear Reviewer:

Reno Tahoe Geo Associates, Inc, (RTGA) is requesting approval of an excavation depth for the attached soils/hydrology application based on previous approvals for nearby parcels, information within our files, and relevant published soil, and geological and topographic information. This letter is transmitted with the completed scoping application and describes the soil and hydrologic conditions at the location of the proposed Southwood Condominium Complex to be located at 941 and 947 Tahoe Boulevard, Incline Village, Washoe County (APN's: 132-231-09 and 132-231-10), (Plates 1 and 2). This letter includes our professional opinion that the proposed excavation will not intercept groundwater.

REFERENCES

The following published and unpublished references were reviewed and serve as the basis of our understanding of the project type and scope:

- Tahoe Regional Planning Agency (TRPA) Spatial Data Downloader, produced by the TRPA accessed May 2021;
- TRPA, 1987 Plan Area Statement Maps, www.trpa.org, assessed May 24, 2021;
- George J. Saucedo, et al., 2005. *Geologic Map of the Lake Tahoe Basin California and Nevada;*

- Natural Resources Conservation Service (NRCS) *Web Soil Survey in Google Earth*, accessed June 2021;
- *Washoe County Real Property Assessment Data*, Washoe County website accessed June 2021;
- Soil Hydrologic Approval Waiver, IVGID Ballfield Improvement Project, 948 Incline Way, Washoe County, NV, APN 127-030-15, TRPA File Number LCAP2019-066, Tahoe Regional Planning Agency, dated April 23, 2019;
- Soil Hydrologic Approval Waiver, 900 Tahoe Boulevard, Washoe County, NV, APN 132-012-04, TRPA File Number LCAP2019-135, Tahoe Regional Planning Agency, dated June 25, 2019;
- Soil Hydrologic Approval, Incline Business Park LLC, 919 Incline Court, Washoe County, NV, APN 132-232-15, TRPA File Number LCAP2009-0209, Tahoe Regional Planning Agency, dated September 17, 2009;
- Soil Hydrologic Investigation Approval, 930 Tahoe Boulevard, Washoe County, NV, APN 132-012-02, TRPA File Number LCAP2018-00182, Tahoe Regional Planning Agency, dated July 23, 2018;
- Approval of Excavation for Proposed Project Based on Completed Investigation, Educational Field Studies Office, 926 Incline Way, Washoe County, APN 132-231-15, TRPA File #970281, Tahoe Regional Planning Agency, dated June 3, 1997.

SITE CONDITIONS

The project site is shown on Plate 2. The proposed project site consists of two adjoining parcels located on the southwest corner of the east intersection of Southwood Boulevard and Tahoe Boulevard in Incline Village, Washoe County, Nevada. The corner parcel (947 Tahoe Boulevard) was formerly occupied by a Chevron gas station. The adjoining parcel (941 Tahoe Boulevard) is located on the south and west sides of the corner parcel and formerly had a building used as a restaurant located in the north-central portion of the lot near Tahoe Boulevard. There are existing driveways on both lots. An approximately 4-foot-high retaining wall is located on the west edge of the corner lot along its north–south property line. The formerly developed portions of each lot are approximately level, and the levelled portion of the corner lot is approximately 8 feet lower than the levelled portion of the western lot. The southern portion of this parcel does not appear to have undergone any historic development. Geotechnical test pit locations are shown on Plate 2.

The site is vegetated, where it has not been disturbed, with pine trees, manzanita shrubs, and other xeric upland species. No hydrophilic vegetation (such as firs, willows, or alders) was observed.

941 and 947 Tahoe Blvd. - Soils/Hydrologic Application Project No. 21073.001 September 7, 2021 Page 3 of 8

There is a single willow bush on the edge of Southwood Boulevard at the driveway entrance to the site, at about Elevation 6,379 feet, adjacent to a storm drain inlet. No other hydrophilic vegetation was noted along the right-of-way for Southwood and Tahoe Boulevard.

PROPOSED IMPROVEMENTS

We understand that a new, five-story condominium complex will be founded with a basement garage. The plan will be approximately C-shaped with three legs approximately 140 to 250 feet long and 60 feet wide. The front face of the building will be approximately 100 feet from Tahoe Boulevard and 30 feet from Southwood Boulevard. The garages will be built on two levels, with an entrance from the uphill, northwest corner to the upper garage level, and an entrance at the southeast corner into a lower garage level. The developer would like to extend the lower parking level under the south and east wings, and as far as approved, under the north wing as well.

The building outline and topographic contours for the site are shown on Plate 3. From Tahoe Boulevard the combined parcels slope from Elevation 6,406 feet at the northwest corner down to Elevation 6,380 feet at the southeast corner where they meet Southwood Boulevard, resulting in an overall site elevation change of 27 feet and an average slope of approximately 7 percent to the southeast. The existing grade within the building footprint varies from Elevation 6,403 feet to 6,382 feet.

The plan (Plate 3) shows the location of two cross sections cut on Plate 4. The finished floor level of the bottom garage level is proposed to be Elevation 6,384, and the bottom footings assuming cantilever concrete retaining walls would conservatively 4 feet lower or Elevation 6,380 feet. Total excavation depth would be 23 feet from existing grade at 6,304 feet. The southern wing would have a maximum excavation depth of approximately 14 feet due to being situated further down the slope.

NEARBY STREAM ENVIRONMENTS

Plate 5 is a map showing that the nearest Stream Environment Zone (SEZ). No springs, seeps, or hydrophilic plants are present on the subject site. Most of the vegetation is dry upland species such as pine and manzanita. The nearest SEZ, Land Capability Zone (Zone 1b) is a minor tributary of Third Creek which drains northwest to southeast approximately 160 feet northeast of the site. The

941 and 947 Tahoe Blvd. - Soils/Hydrologic Application Project No. 21073.001 September 7, 2021 Page 4 of 8

tributary of Third Creek is incised about 8 to 10 feet below adjacent upland ground surface and Tahoe Boulevard at the intersection with Northwood Boulevard. Based on the topographic elevations using a level survey, the creek level is approximately Elevation 6,378.50 to 6375 feet just north of the intersection. There are rushes and meadow grass to 4378 to 4381 feet on the edge of the creek which represent the stream environment zone vegetation. It is expected that the creek is recharging the adjacent groundwater, so that groundwater surface will dip away from the creek bed and will decrease in elevation under the site.

SOIL AND GEOLOGIC CONDITIONS

Based on published information by NRCS and site observation, the native soils have been categorized as Inville gravelly coarse sandy loam, 2 to 9 percent slopes, stony, and with the hydrologic soil group A. The soil is well drained, with a saturated permeability of 2 to 6 inches per hour. According to Saucedo et al. (2005), the site is underlain by undivided glacial outwash deposits of Holocene or Pleistocene age (Plate 7).

RTGA performed geotechnical test pits in June 2021, which are included on Plates 8 through 10. Test pit TP-1 near the northeast corner of the north wing extended to 15 feet depth, the maximum depth available to the excavator. Soils were generally a yellow brown to brownish yellow silty sand to sandy clay throughout, which was only slightly darker hue at the bottom of the test pits (7.5YR 5/6) compared to soils at 2 feet depth (10YR 6/8). A lower-permeability clay layer at 11 to 13 feet depth showed weathered sand and gravel particles but did not include mottling.

TP-2 under the south wing did not encounter the lower permeability layer nor any mottling to 13 feet or Elevation 6,375 feet, the maximum depth explored. There is no sign of hydrophilic vegetation along the adjacent edge of Southwood Boulevard with a surface at Elevation 6,376 feet at this location. TP-3 at the southeast corner of the proposed building encountered mottled soil at 5 feet depth or approximately Elevation 6,379 feet, however there is no surface evidence of hydrophilic vegetation at this location which would occur if seasonal or recent past groundwater was this high.

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PROPOSED EXCAVATION DEPTH

The elevations of the building basement garage relative to the site contours are shown on Plates 3 and 4. The garage floor of the eastern leg is expected to be at about Elevation 6,384 feet and maximum depth of excavations for footings are expected to be no more than 4 feet lower (6,380 feet). For the entire length of the east leg, the depth of excavation would be approximately 5 feet on the downhill edge and 10 feet on the uphill edge, but is above the grade of adjacent Southwood Drive, which varies from Elevation 6,376 to 6,380 feet ground surface along the entire eastern edge.

The northwest wing of the building at Elevation 6,380 feet as shown on the top of Plate 4 profile X1 would be approximately 23 feet to bottom of excavation at the northwest corner but is roughly 5 feet depth at the northeast corner and is at adjacent grade of Southwood Boulevard at the east corner.

The southwest wing of the building as shown on the bottom of Plate 4 profile X2 would be approximately 15 feet to bottom of excavation at the northwest corner and 5 feet depth at the southeast corner but is above the adjacent grade of Southwood Boulevard a short distance from the east corner.

A review of TRPA records indicates eight previously approved soils/hydrologic applications, within 1,200 feet of the subject site (Plate 6). Approval letters for five requests show excavation depths ranging from 6 to 12 feet (Attachment 2). Approvals for three other parcels, APN's 132- 231-05, 132-231-06, and 132-231-18 were not found during our online search. None of the parcels showed a similar depth of approved excavation, however that may reflect the maximum depth required rather than the actual limit due to high groundwater.

We recommend that the east leg of the building parallel to Southwood Boulevard can be excavated to Elevation 6,376 feet without additional exploration, where the west edge of Southwood Boulevard shows no sign of spring activity or hydrophilic vegetation within 30 feet of the building footprint. It is logical that the maximum depth of excavation for the eastern leg of the building is above water level, as Southwood Boulevard is below the foundation level.

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We recommend the southeastern wing of the building under the southern undeveloped portion of the site shows no evidence of hydrophilic vegetation to Elevation 6,380 feet and test pit TP-2 has no clayey or mottled layers, therefore excavation to Elevation 6,380 feet should be approved without additional excavation.

TABLE 1: NEARBY PROJECTS AND APPROVED EXCAVATION DEPTHS							
Location	Proximity to Project Site	Approved TRPA Excavation Depth	Subsurface Exploration Method				
926 Incline Way TRPA File # 970281 APN 132-231-15	190 ft Southwest	9 Feet	Test Pit				
948 Incline Way TRPA File LCAP2019-0066 APN 127-030-15	220 ft Southeast	12 Feet	Waived				
930 Tahoe Boulevard TRPA File LCAP2018-0182 APN: 132-012-02	680 ft Northwest	7.5 Feet	Test pit				
919 Incline Court TRPA File # LCAP2009-0209 APN: 132-232-15	725 ft Southwest	6 Feet	Test Pit				
900 Tahoe Boulevard TRPA File # LCAP2019-0135 APN: 132-012-04	1,200 ft Northwest	7 Feet	Waived				

We recommend the northeastern wing of the building depth of maximum past groundwater was not present in the test pit to 15 feet depth or Elevation 6,387 feet. While there are strong chroma soils in test pit TP-1, they are do not vary substantially from 2 to 15 feet, as shown on the photo in Plate 11. We do not propose that the groundwater level is at 2 feet depth based on chroma, therefore the same coloring is not indicative of past shallow groundwater at 15 feet either. Vegetation at the ground surface is dry and not hydrophilic.

941 and 947 Tahoe Blvd. - Soils/Hydrologic Application Project No. 21073.001 September 7, 2021 Page 7 of 8

Alternatively, it is possible that the site was a shallow marsh area developing high chroma soils prior to grading of Tahoe Boulevard, diversion of the creek, and the culvert crossing at the intersection. However, based on the dry vegetation that has grown up on the site over the past 50-plus years, we consider any groundwater lowering and vegetation changes due to Lakeshore Boulevard are permanent at this point and should not reflect recent activity of high groundwater level.

We request approval of a maximum excavation depth to 23 feet depth to support the garage excavation. Excavation of test pits deeper than about 15 feet depth is impractical, and soil borings would be required if more information is requested.

APPLICATION CHECKLIST

- a) Land Capability: Class 6 based on 2008 verification.
- b) *Proposed Maximum Excavation (below existing grade):* 12 feet for the east leg to Elevation 6,376 feet, 15 feet for the south wing or Elevation 6,380 feet, and 11 feet for the north wing or Elevation 6,391 feet.
- c) *Explanation of methodology in selection of test pits:* No additional exploration is proposed.
- d) Volume of Spoil Material: Approximately 7,000 cubic yards.

Temporary Spoil Storage: Hauled off site to an approved fill location.

- e) *Stream Environment Zones:* The excavation described above is not in a Stream Environment Zone. The nearest possible SEZ is an unnamed shallow channel which drains to Third Creek located approximately 160 feet northeast across Tahoe Boulevard (Plate 5).
- f) Cross-Section through Proposed Excavation: See Plate 4.
- g) Nearby Approved Parcels: See Plate 6
- h) *Statement of Need:* The proposed excavation is required to allow new construction of spread footings and parking for multiple condominium units.
- i) *Photographs:* See Plates 11, 12, 13, 14, and 15.
- j) Vegetation: Pine trees and manzanita. No hydrophilic or wetland species were observed.
- k) Soil Type: Inville gravelly coarse sandy loam, 2 to 9 percent slopes, stony.
- 1) *Geologic Information:* Quaternary outwash deposits includes Tioga and Tahoe age deposits as well as pre-Tahoe and possibly younger (Holocene) glacial deposits.
- m) Topography: 20H:1V in proposed building area.

941 and 947 Tahoe Blvd. - Soils/Hydrologic Application Project No. 21073.001 September 7, 2021 Page 8 of 8

CLOSURE

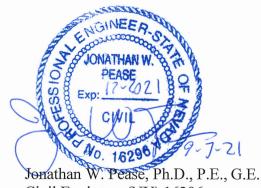
We trust that the information provided in this report provides the necessary information to favorably review this scoping report. If you have any questions regarding this report, please contact our office.

Sincerely,

Reno Tahoe Geo Associates, Inc.

Thave Matsaring

Shane Mulvaney Senior Geologist

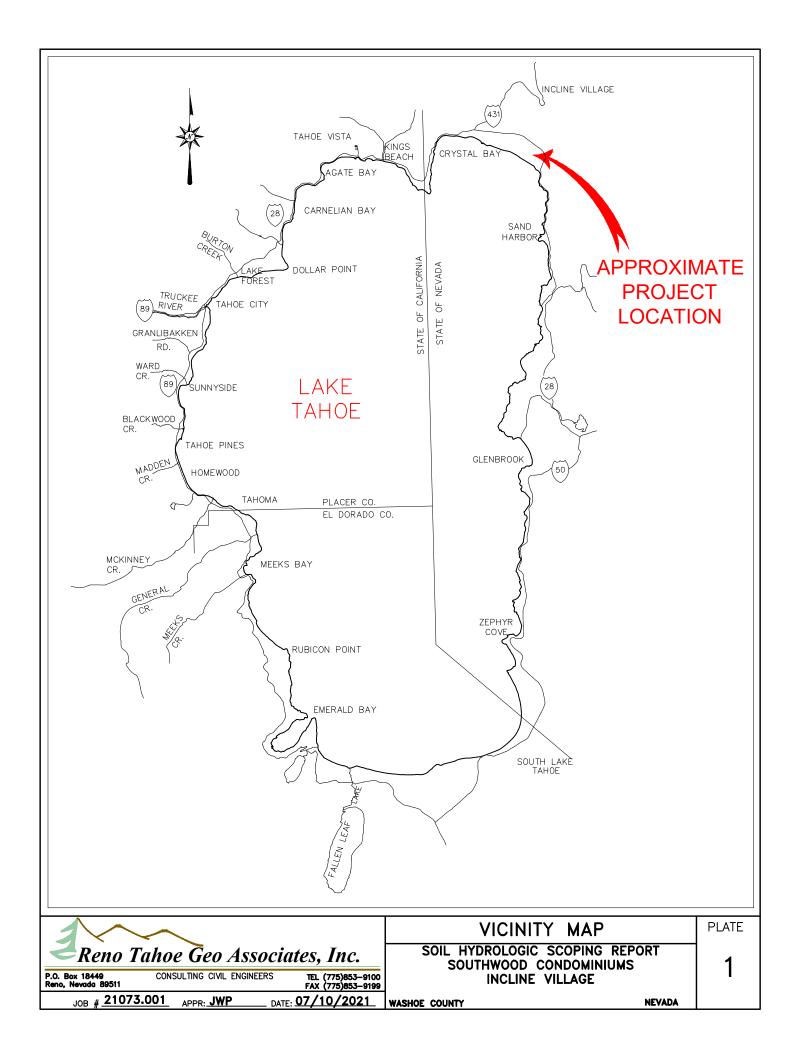


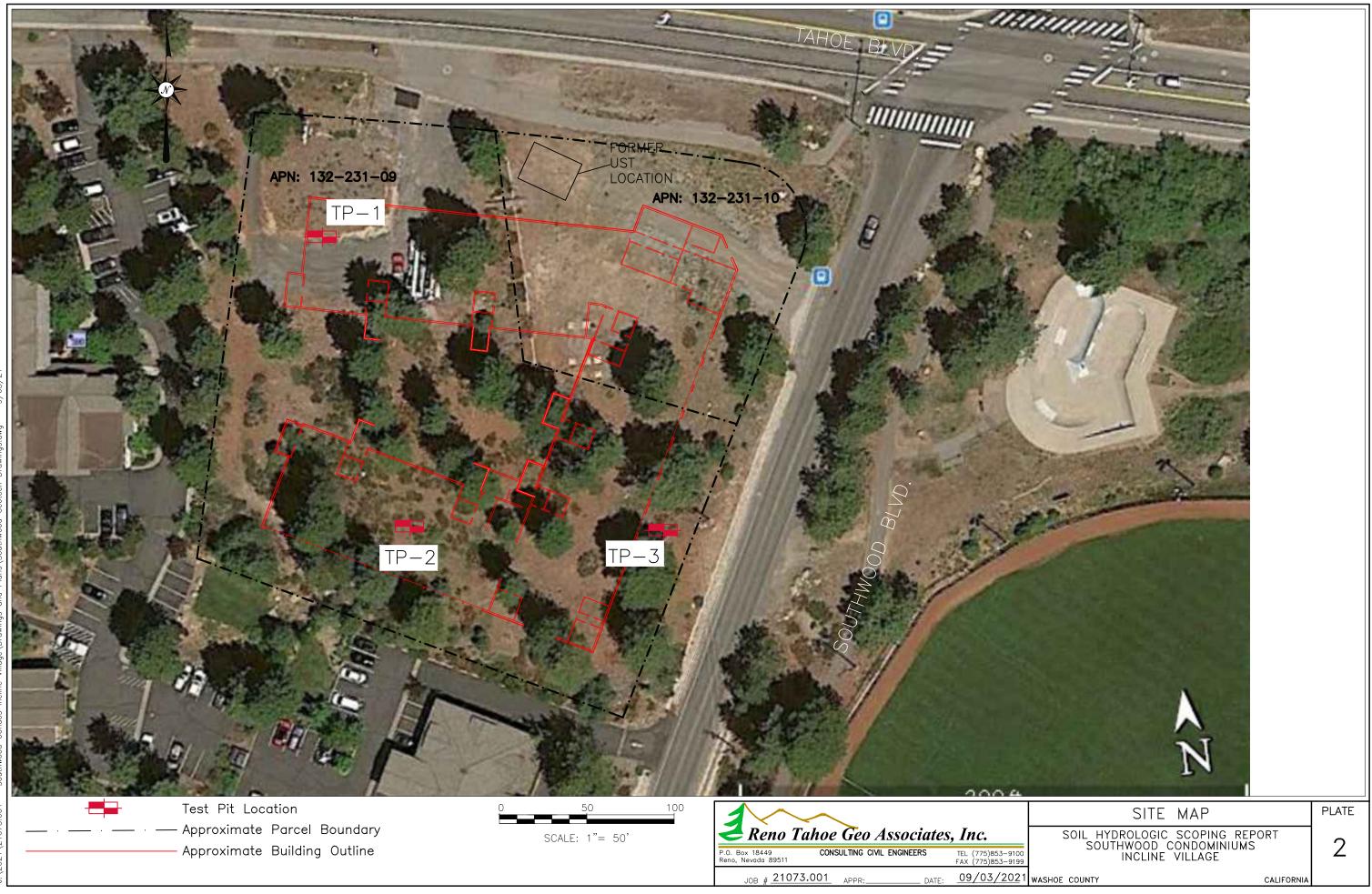
Civil Engineer, (NV) 16296

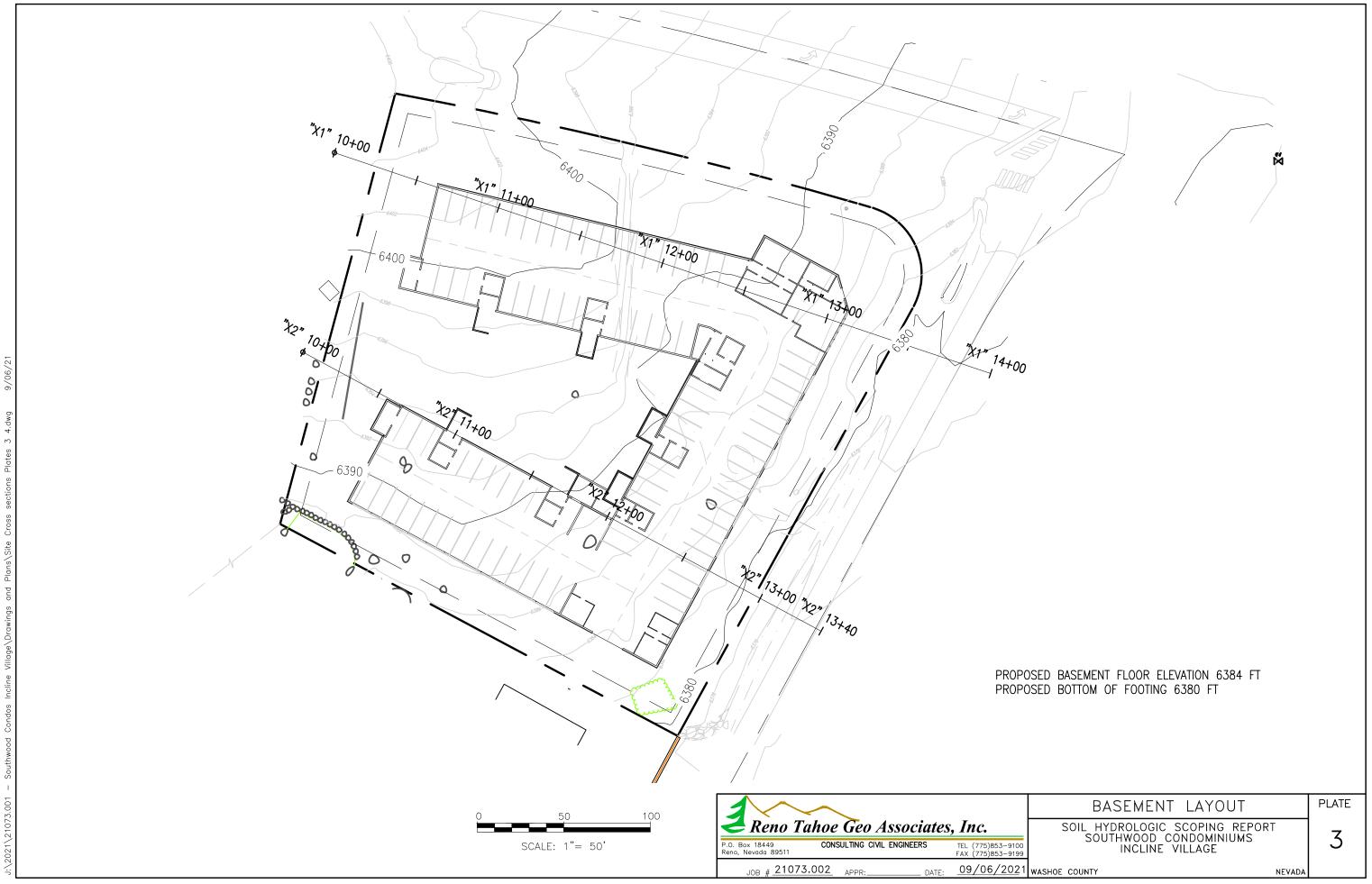
Plates: Plate 1	Vicinity Map	
Plate 2	Site Plan	
Plate 3	Basement Layout	
Plate 4	Cross-Sections	
Plate 5	SEZ Locations	
Plate 6	Nearby Soils/Hydrologic Approvals Plate 7	Geologic Map
Plates 8-10	Logs of Test Pits	
Plate 11	Photo of Test Pit TP-1	
Plates 12–16	Site Photos	

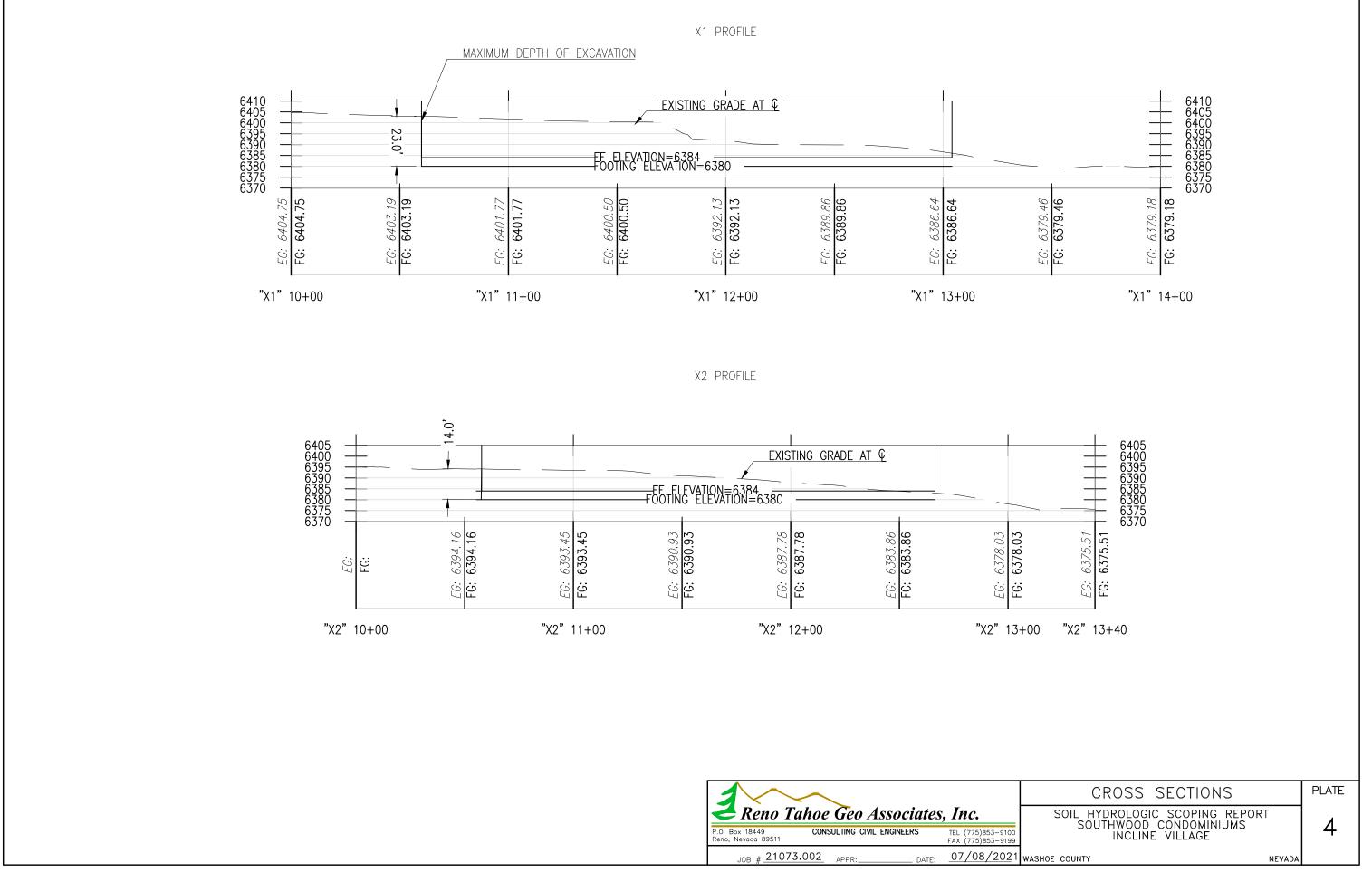
Attachments: TRPA Soils/Hydrologic Approval Letters for Nearby Parcels Soils/Hydrology Scoping Report Application

PLATES

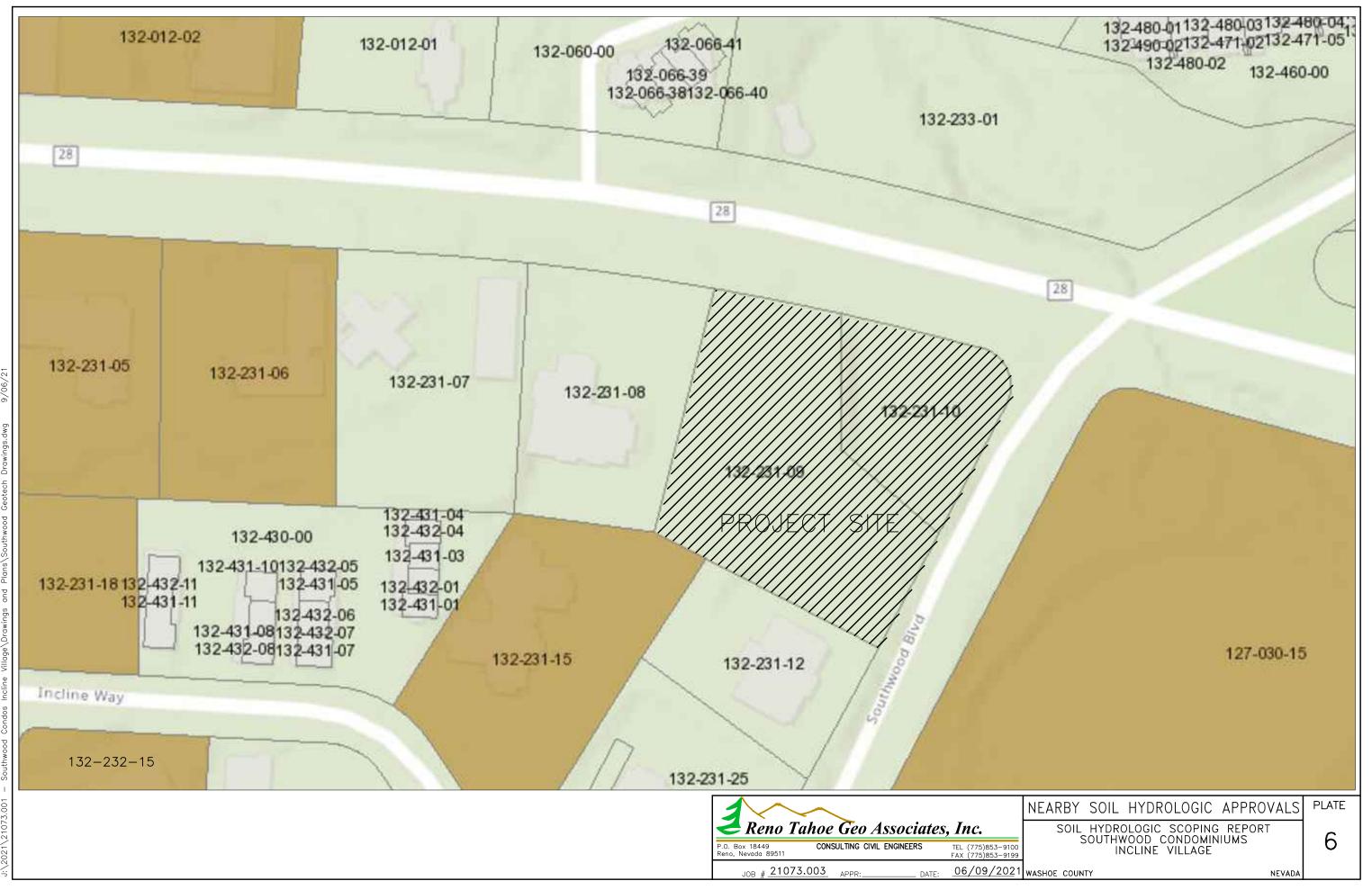


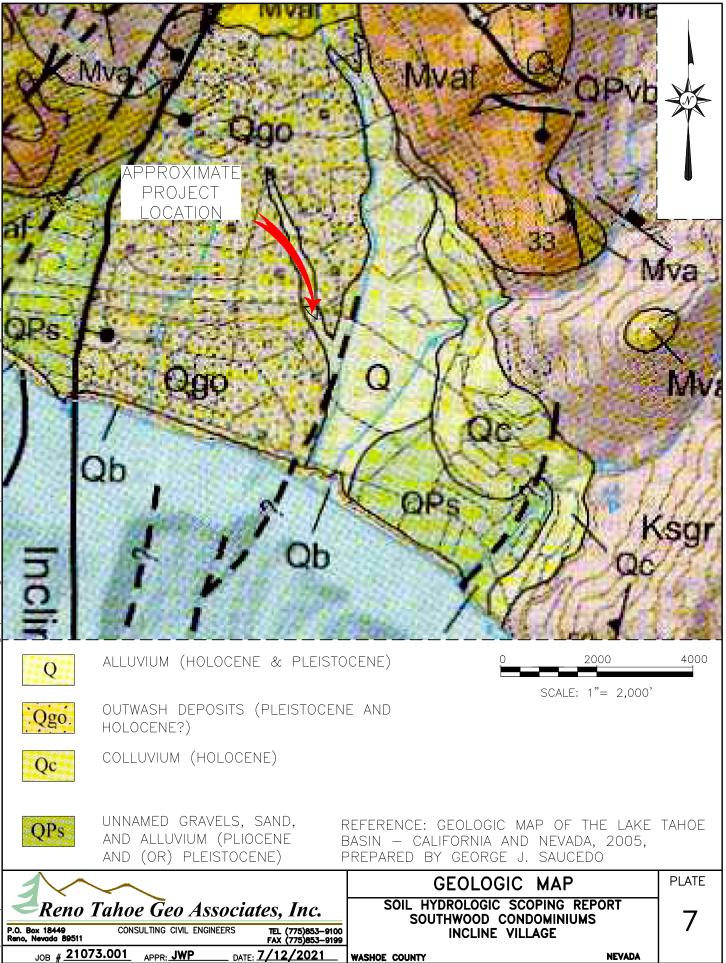








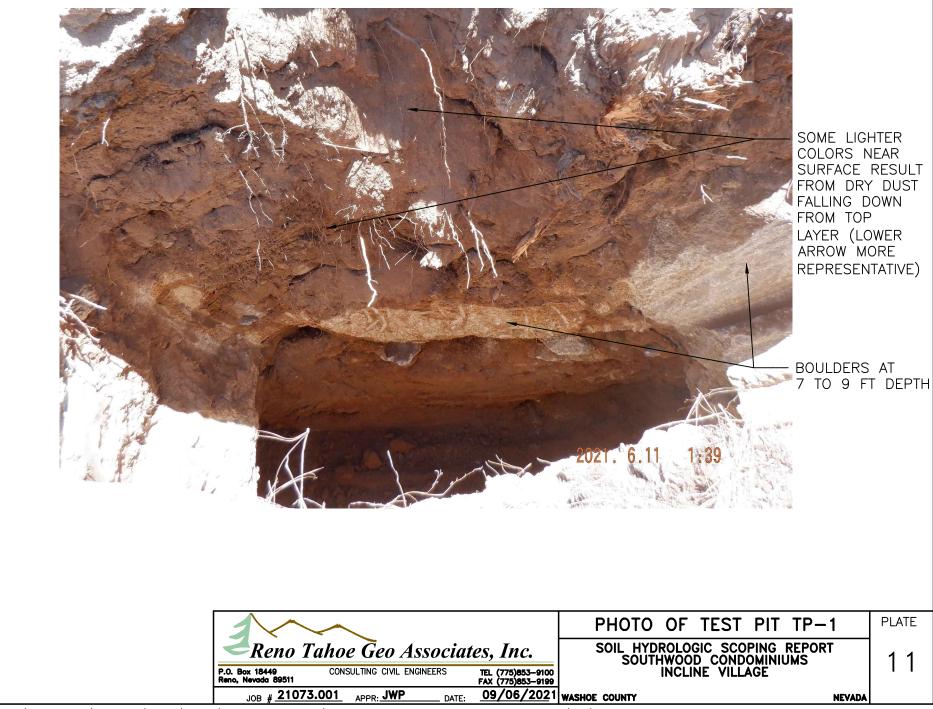




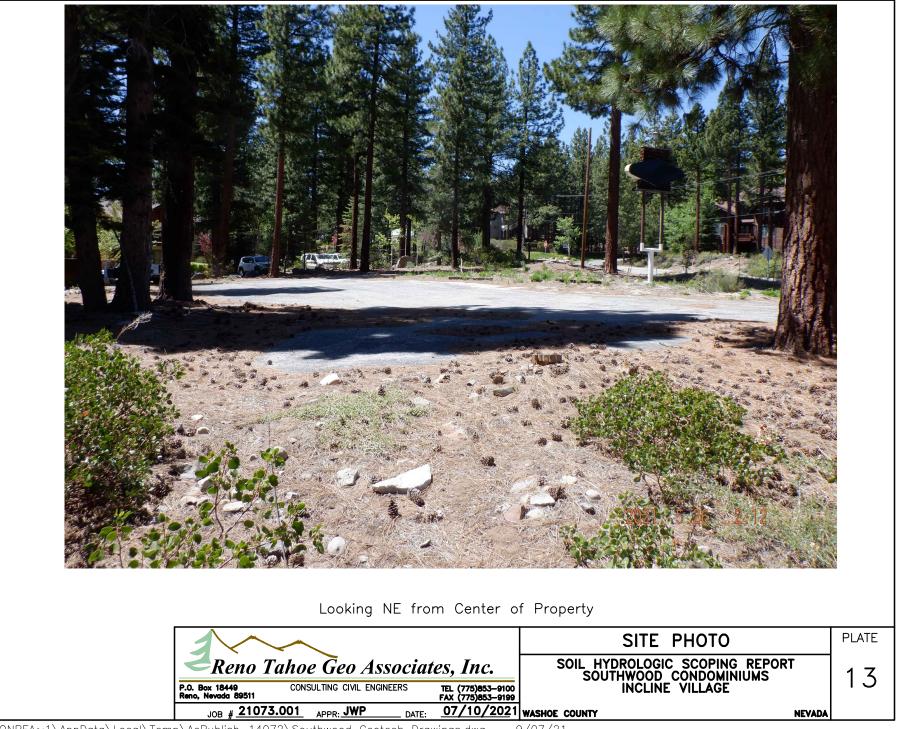
		Ś			≻				LOG OF TEST PI	T TP-1		
		ŇO	F	Т (%	ISIT	£,			LOCATION NORTHWEST QUADRANT OF SITE			
	LABORATORY TESTS	FIELD BLOWS (6in	3LOWS/FT	MOISTURE CONTENT (9	DENSITY	DEPTH (ft)	РГП					
		FIEL /6in	BLOV		DRY (pcf)	ded	SAMPLE		EQUIPMENT LINK-BELT 145 X 4			
		÷	:	:		0-	1	<u> </u>	ELEVATION <u>6402.0</u> DATE <u>6/10/21</u>			
		:	•	: :		-		<u>1/ 1/</u>	Pine duff overlying silty sand (decomposed granite) fill. (10 (est.15% G/ 55% S/ 30% F)	0YR 7/1)		
		:	•			-	1		DARK YELLOWISH BROWN SILTY SAND WITH BOULDE AND COBBLES (SM)	RS		
		:	•	: :		-	łX		Dry to slightly moist, loose, fine to coarse angular to subro gravel, non-plastic silt in fine to coarse granitic sand. 20%	ounded		
		:	•	: :		2 —	<u> </u>		subrounded cobles and 20% subangular to subrounded to 3 feet size. Abundant roots. (10YR 3/4)	poulders to		
		:	•	: :		-			(est.20% G/ 60% S/ 20% F)			
		:	•	:		-		A	BROWNISH YELLOW SILTY SAND WITH BOULDERS AN COBBLES (SM)			
			•			-			Dry to slightly moist, loose to medium dense, fine to coars to subrounded gravel, non-plastic silt in fine to coarse grar	nitic sand.		
		:	•	: :		4 —			20% angular to subrounded cobbles and 20% subangular subrounded boulders to 6+ feet size. Abundant roots. (10)			
		:				_	A		(est.30% G/ 50% S/ 20% F)			
		:				-	ĮĮ	•				
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				: :		6 —	[4			
		:	•			_						
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			: :		-							
					8 —			LIGHT GRAY Single boulder of indeterminate size. Hard, lenticular gran	ite mass.			
					-			Difficult to excavate. (10YR 7/1)				
		:	•	: :		_				-		
				:					BROWNISH YELLOW SILTY SAND WITH BOULDERS AN COBBLES (SM)			
		:	•			10 —			Slightly moist, loose, fine to coarse angular to subrounded non-plastic silt in fine to coarse granitic sand. 20% angula	ar to		
				· · · ·				· •	subrounded cobbles and 20% subangular to subrounded b 3 feet size. (10YR 6/8)	poulders to		
9/7/21	SA, Percent Passing #200 =51%					_			(est.30% G/ 50% S/ 20% F)			
		•	•			_	Λ		YELLOWISH BROWN LEAN CLAY (CL) Slightly moist to moist, fine sand in soft to firm, low plastic	ity clay with		
15A.G		: :		12 —	IV		dark yellowish brown (10YR4/6) and olive (5YR5/5) flecks (decomposed fine gravel). (10YR 5/8)					
TE 201	Liquid Limit = 35 Plasticity Index = 14	:	•	: :		12]					
EMPLA		-	•			_	$\left \right\rangle$					
ΑΤΑ ΤΙ		:	•	: :	•	_	Λ	M	STRONG BROWN SILTY, CLAYEY SAND (SC-SM) Moist, loose, thin low to medium plasticity clay and non-plastic silt	astic silt		
IED D.		:	•	: :		14 —	IV		layers in fine to coarse sand. Fine to medium subangular subrounded gravel. (7.5YR 5/6)	to		
GPJ N		:	•	: :		14]		(est.20% G/ 50% S/ 30% F)			
SOUTHWOOD SOILS HYDRO.GPJ MED DATA TEMPLATE 2015A.GDT			•			_	7)					
		•	•			_			TERMINATED @ 15'			
					16			No Free Water Observed				
DOWH.					16 —							
		•		. :				L	LOG OF TEST PIT TP-1	PLATE		
1 LOG LETTER SIZE	Reno Tahoe Geo Associates, Inc.											
LETTE	P. O. Box 18449 CONSUL	D. Box 18449 CONSULTING CIVIL ENGINEERS TEL (775) 853-9100						SOUTHWOOD CONDOMINIUMS INCLINE VILLAGE				
1 LOG	Reno, Nevada 89511	PR:		DATE:	6/11/2			WASHO	DE COUNTY NEVADA			

		FIELD BLOWS /6in BI OWS/FT	MOISTURE CONTENT (%)	DRY DENSITY (pcf)	⊣ (ft) F		LOG OF TEST PI	<u>T TP-2</u>
	LABORATORY TESTS	ELD In In		۲ ق()	DEPTH (ft) SAMPLE		EQUIPMENT LINK-BELT 145 X 4	
		. E. S. E	i ≥ŏ.	<u>⊐</u> ≗.		<u>ا</u> م	ELEVATION <u>6388.0</u> DATE <u>6/10/21</u>	
					0		DARK REDDISH BROWN SILTY SAND (SM) Dry, loose, angular to subrounded gravel, non-plastic silt, coarse sand. Pine duff overlying topsoil. (2.5YR 3/4) (est.15% G/ 60% S/ 25% F) DARK YELLOWISH BROWN SILTY SAND WITH COBBLI BOULDERS (SM) Dry to slightly moist, loose matrix, fine to coarse angular t subrounded gravel, non-plastic silt in fine to coarse graniti 25% angular to subrounded cobbles and 20% subangular subrounded boulders to 3 feet size. Abundant roots. (10Y (est.20% G/ 60% S/ 20% F)	ES AND o c sand. to
		· · · · · · · · · · · · · · · · · · ·		÷	-			
					4			
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		· · ·	· · · · · · · · · · · · · · · · · · ·	•	_			
			•	-		YELLOWISH BROWN SILTY SAND WITH COBBLES AND)	
					- 8 - -		BOULDERS (SM) Dry to slightly moist, loose matrix, fine to coarse angular to subrounded gravel, non-plastic silt in fine to coarse graniti 30% angular to subrounded cobbles and 5% subangular to boulders to 3 feet size. (10YR 5/6) (est.25% G/ 55% S/ 20% F)	c sand.
T 9/7/21					10			
SOUTHWOOD SOILS HYDRO.GPJ MED DATA TEMPLATE 2015A.GDT					- 12			
TEMP			· · · · · · · · · · · · · · · · · · ·	• • •	_		TERMINATED @ 13'	
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ER SIZE	Reno Tahoe	Gen A	ssocia	tos	Inc		SOIL HYDROLOGIC SCOPING REPORT	
LETTER		TING CIVIL ENG			853-9100 853-9199		SOUTHWOOD CONDOMINIUMS INCLINE VILLAGE	9
1 LOG	21072 001	PPR:	DATE:	<u>6/11/20</u>		WASHOE		

	LABORATORY TESTS	FIELD BLOWS /6in	BLOWS/FT MOISTURE	DRY DENSITY (pcf)	DEPTH (ft)	SAMPLE		LOG OF TEST PIT	<u>T TP-3</u>		
					0 — 2 — - -			DARK REDDISH BROWN SILTY SAND (SM) Dry, loose, angular to subrounded gravel, non-plastic silt, i coarse sand. Pine duff overlying topsoil. Scattered surfici to 5 feet size. (2.5YR 3/4) (est.15% G/ 55% S/ 30% F) DARK YELLOWISH BROWN SILTY SAND WITH COBBLE BOULDERS (SM) Dry, loose, fine to coarse angular to subrounded gravel, no silt, fine to coarse granitic sand. Estimate 15% angular to subrounded cobbles. Common boulders to 3 feet size. (10 (est.15% G/ 65% S/ 20% F) grades yellowish brown	al boulders		
					- 4			grades yellowish brown			
					- - 6 -	-		YELLOWISH RED SILTY SAND (SM) Slightly moist, loose to medium dense, non-plastic silt in fi Some dark yellowish brown (10YR 4/6) mottling. Minor an subrounded gravel. (5YR 5/8) (est.10% G/ 65% S/ 25% F)	ne sand. gular to		
					- - 8 — -			GRAY / LIGHT OLIVE GRAY SILTY SAND (SM) Dry, medium dense to dense, non-plastic silt in fine to coa Some angular to subangular cobbles and boulders. Excav at 9'. (5Y 6/1) (est.20% G/ 60% S/ 20% F)	rse sand. ⁄ator refusal		
					- - 10 —	-		TERMINATED @ 9' No Free Water Observed			
ATE 2015A.GDT 9/7/21					- - 12 —	-					
J MED DATA TEMPL/					- - 14 —	-					
SOUTHWOOD SOILS HYDRO.GPJ MED DATA TEMPLATE 2015A.GDT 9/7/21					- - - 16 —	-					
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	Pana Takaa	Car	10000	atos	Inc	-		LOG OF TEST PIT TP-3 SOIL HYDROLOGIC SCOPING REPORT	PLATE		
1 LOG LETTER SIZE	P. O. Box 18449 Reno, Nevada 89511 CONSULTING CIVIL ENGINEERS 21072 001 CONSULTING CIVIL ENGINEERS 21072 001 CONSULTING CIVIL ENGINEERS CONSULTING CIVIL ENG							SOUTHWOOD CONDOMINIUMS IU INCLINE VILLAGE			
ĬŢ	_{JOB #} 21073.001 _{AF}	PR:	DATE	<u>6/11/2</u>	2021	- I	WASHOE COUNTY NEVADA				













	SITE PHOTO	PLATE
<i>Reno Tahoe Geo Associates, Inc.</i>	SOIL HYDROLOGIC SCOPING REPORT	16
P.O. Box 18449 CONSULTING CIVIL ENGINEERS TEL (775)853-9 Reno, Nevada 89511 FAX (775)853-9		
JOB # 21073.001 APPR: JWP DATE: 07/07/20	21 washoe county nevada	

ATTACHMENTS



Mail PO Box 5310 Stateline, NV 89449-5310 Location 128 Market Street Stateline, NV 89449 Contact Phone: 775-588-4547 Fax: 775-588-4527 www.trpa.org

April 23, 2019

Andrew Haney Incline Village General Improvement District 1220 Sweetwater Incline Village, NV 89451

SOIL HYDROLOGIC APPROVAL – WAIVER IVGID BALLFIELD IMPROVEMENT PROJECT 948 INCLINE WAY, WASHOE COUNTY, NEVADA APN 127-030-15, TRPA FILE NUMBER LCAP2019-0066

Dear Mr. Haney:

Tahoe Regional Planning Agency (TRPA) staff has reviewed the Soils/Hydrologic Scoping Report Application submitted in association with the Incline Village General Improvement District Ballfield Improvement project. The proposed excavation of **12 feet below ground surface** is for installation of two pole foundations for the scoreboard. Although the excavation may intercept groundwater, the excavation is allowed pursuant to TRPA Code of Ordinances Sections 33.3.6.A.2.a (accommodation of engineering requirements for above-ground structures).

Please note that it is possible that variations in the soil or groundwater conditions could exist that are different than what has been investigated or reported. Although it is not anticipated that groundwater will be encountered during the proposed fall construction time period, if conditions are found to be wetter than expected, contact TRPA to discuss options for dewatering.

Pursuant to Rule 11.2 of the TRPA Rules of Procedure, this soils/hydrological approval may be appealed within twenty-one (21) days from the time TRPA releases any final decision.

If you have any questions, please contact me by phone at (775) 589-5247 or by email at jroll@trpa.org.

Sincerely,

Julie Roll Senior Planner



Mail PO Box 5310 Stateline, NV 89449-5310

Location 128 Market Street Stateline, NV 89449 Contact Phone: 775-588-4547 Fax: 775-588-4527 www.trpa.org

June 25, 2019

Ryan Burlt Construction 1455 Deming Way #1 Sparks, NV 89431

SOIL HYDROLOGIC APPROVAL - WAIVER 900 TAHOE BOULEVARD, WASHOE COUNTY, NEVADA APN 132-012-04, TRPA FILE NUMBER LCAP2019-0135

Dear Mr. Burlt:

The Tahoe Regional Planning Agency (TRPA) staff has reviewed the Soils/Hydrologic Scoping Report Application submitted in association with the Bank of America light fixture upgrade. The proposed excavation of 7 **feet below ground surface** is for installation of six light poles in the bank parking lot. It is not expected that groundwater will be encountered in this location and the excavation is allowed pursuant to TRPA Code of Ordinances Sections 33.3.6.A.2.a (accommodation of engineering requirements for above-ground structures) and 33.3.6.A.2.d (public health and safety).

Please note that it is possible that variations in the soil or groundwater conditions could exist that are different than what has been investigated or reported. If conditions are found to be wetter than expected, contact TRPA immediately to discuss options for dewatering.

Pursuant to Rule 11.2 of the TRPA Rules of Procedure, this soils/hydrological approval may be appealed within twenty-one (21) days from the time TRPA releases any final decision.

If you have any questions, please contact me by phone at (775) 589-5247 or by email at jroll@trpa.org.

Sincerely,

NPV

Julie Roll Senior Planner

C. Laura Fabrizio 3328 Newbliss Cir. Ormond Beach, FL 23174

TAHOE REGIONAL PLANNING AGENCY

128 Market Street Stateline, Nevada www.trpa.org P.O. Box 5310 Stateline, Nevada 89449 (775) 588-4547 Fax (775) 588-4527 Email: trpa@trpa.org

September 17, 2009

Huldrege & Kull Pam Raynak 10775 Pioneer Trail #213 Truckee, CA 96161

RE: SOIL HYDROLOGIC APPROVAL INCLINE BUSINESS PARK LLC, 919 INCLINE CT., WASHOE COUNTY APN 132-232-15, TRPA FILE NUMBER LCAP2009-0209

Dear Ms. Raynak:

The Tahoe Regional Planning Agency (TRPA) staff's Land Capability Program has reviewed the Soils/Hydrologic Scoping Report Application submitted September 2, 2009. Upon reviewing the application and site visit to observe a test pit, **TRPA staff hereby** approves the excavation for an infiltrating BMP to 6 feet below ground surface.

Please note that it is possible that variations in the soil or groundwater conditions could exist at the site that are different than what has been investigated or reported. Also, changes in site conditions could occur at some time in the future due to variations in rainfall, snowfall, temperature, regional water usage, or other factors. These variations and/or changes could cause the groundwater level to be higher than interpreted. Because of this, the applicant is required to notify the TRPA immediately if significantly different subsurface conditions are encountered than what has been interpreted from the investigation.

This letter only approves the depth of the excavation and does not represent approval for the project.

The TRPA has the following recommendations for the project:

- 1. Temporary Best Management Practices (BMPs) are to be installed and maintained prior to excavation and during all phases of the proposed project.
- 2. All excavated materials shall be hauled away from the site to a legally acceptable location. No fills or recontouring, other than backfill for the cut-retaining structures, shall be allowed.
- 3. Blasting of rocks should be kept to an absolute minimum to avoid damage to surrounding rocks and vegetation.

Pursuant to Rule 11.2 of the TRPA Rules of Procedure, this soils/hydrological approval may be appealed within twenty-one (21) days from the time TRPA releases any final decision. Thank you for your cooperation. Should you have any questions about these matters, please contact this office at (775) 589-5313.

Sincerely,

Heather Gustafson Senior Planner / Land Capability Program Manager Environmental Review Services Tahoe Regional Planning Agency



Mail PO Box 5310 Stateline, NV 89449 5310 Location 128 Market Street Stateline, NV 89449 Contact Phone: 775-5884547 Fax: 775 5884527 www.trpa.org

July 23, 2018

Kevin Provance Black & Veatch 5885 Meadows Rd, Ste. 700 Lake Oswego, OR 97035

SOIL HYDROLOGIC INVESTIGATION - APPROVAL 930 TAHOE BOULEVARD, WASHOE COUNTY, NEVADA APN: 132-012-02 TRPA FILE NUMBER LCAP2018-0182

Dear Mr. Provance:

Tahoe Regional Planning Agency (TRPA) staff reviewed the Soils/Hydrologic Report Application submitted June 26, 2018. Field conditions were evaluated onsite by TRPA contractor Phil Scoles on July 17, 2018 (exposed excavation on this date). The soil thickness is greater than 7 feet deep. No evidence of ground water (i.e. iron staining, gray soil, etc.) was observed; however, the decaying stones and boulders contain oxidized iron deposits. Such deposits are not evidence of a seasonal water table – they are a product of the natural breakdown of the rock mineralogy. There are also several soil/hydrologic investigations that occurred nearby that also lacked groundwater in the upper 9 feet (or deeper). Based on the field investigation, TRPA staff hereby approves an excavation of 7.5 feet below ground surface for the proposed retaining wall parallel to the east property line (behind the Tesla Supercharging Station currently under construction).

Please note that it is possible that variations in the soil or groundwater conditions could exist at the site that are different than what has been investigated or reported. Also, changes in site conditions could occur at some time in the future due to variations in rainfall, snowfall, temperature, regional water usage, or other factors. These variations and/or changes could cause the groundwater level to be higher than interpreted. *Because of this, the applicant is required to notify the TRPA immediately if significantly different subsurface conditions are encountered than what has been interpreted from the investigation.*

This letter only approves the depth of the excavation and does not represent approval for the project. TRPA has the following recommendations for the project:

- 1. Temporary Best Management Practices (BMPs) are to be installed and maintained prior to excavation and during all phases of the proposed project.
- 2. All excavated materials shall be hauled away from the site to a legally acceptable location. No fills or recontouring, other than backfill for the cut-retaining structures, is allowed.

3. Blasting of rocks should be kept to an absolute minimum to avoid damage to surrounding rocks and vegetation.

Pursuant to Rule 11.2 of the TRPA Rules of Procedure, this soils/hydrological approval may be appealed within twenty-one (21) days from the time TRPA releases any final decision (August 13, 2018).

If you have any questions, please contact me by phone at (775) 589-5249 or by email at jroll@trpa.org.

Sincerely,

tie M

Julie Roll Senior Planner Current Planning Department

Cc: Andrew Levy Tesla Motors, Inc. 3500 Deer Creek Road Palo Alto, CA 94304

> Joel Korotkin 6029 Monet Way El Dorado Hills, CA 95762

TAHOE REGIONAL PLANNING AGENCY

308 Dorla Court Elks Point, Nevada P.O. Box 1038 Zephyr Cove, Nevada 89448-1038

(702) 588-4547 Fax (702) 588-4527 Email: trpa@sierra.net

June 3, 1997

MR PAUL KALETA BASIN STRATEGIES POST OFFICE BOX 11945 ZEPHYR COVE NEVADA 89448

Dear Mr. Kaleta:

APPROVAL OF EXCAVATION FOR PROPOSED PROJECT BASED ON COMPLETED INVESTIGATION, EDUCATIONAL FIELD STUDIES OFFICE, 926 INCLINE WAY, WASHOE COUNTY, APN 132-231-15, TRPA FILE #970281

The Tahoe Regional Planning Agency (TRPA) staff's Ground Water Technical Advisory Committee (GWTAC) has reviewed the final report, dated May 30, 1997, that was prepared by Darlene Barlow of Nortech. The GWTAC hereby approves the final report and agrees with the conclusions that no evidence was found to show that the proposed excavation to a total depth of 9.0 feet below ground surface (bgs) would intercept the highest recorded groundwater levels.

No groundwater, mottled, gleyed, or reduced areas in the soil profile were observed in the soil test pits to indicate seasonal groundwater levels. The GWTAC approves the depth of the proposed excavation to not exceed 9.0 feet bgs for the project.

Please note that it is possible that variations in the soil or groundwater conditions could exist at the site that are different than what has been investigated or interpreted. Also, changes in site conditions could occur at some time in the future due to variations in rainfall, snowfall, temperature, regional water usage, or other factors. These variations and/or changes could cause the groundwater level to be higher than interpreted. Because of this, the applicant is required to have a TRPA GWTAC member inspect the completed excavation to verify that it does not intercept existing or historic groundwater levels.

This letter only approves the depth of the excavation and does not represent approval for the project. A copy of this letter has been forwarded to the appropriate project reviewing department for inclusion in the project file. The project reviewing department will review the project for conformance with other applicable ordinances to determine if a conditional permit can be issued and will use this letter as an approval of the depth of the excavation only.

The TRPA GWTAC has the following recommendations for the project:

1. All excavated materials shall be hauled away from the site to a legally acceptable location. No fills, or recontouring, other than backfills for the cut-retaining structures, shall be allowed.

Planning for the Protection of our Lake and Land

Mr. Paul Kaleta June 3, 1997 Page Two





2. The excavation for the project shall be visually inspected by a TRPA GWTAC member to verify that the excavation is above the highest recorded existing or seasonal groundwater level. If groundwater is intercepted, then the excavation and foundation design shall be immediately revised to not intercept groundwater. The revised depth shall be subject to approval by the GWTAC.

Thank you for your cooperation. Should you have any questions about these matters, please contact this office at (702) 588-4547.

Sincerely,

Douglas F. Smith TRPA GWTAC Lead Geologist California Registered Geologist No. 6540

Joseph Pepi TRPA GWTAC Lead Soil Scientist Certified Professional Soil Scientist, No. 2372

DFS/jsd

c: Ms. Darlene Barlow, PE, NORTECH, 390 Freeport Blvd. #12, Sparks NV 89431 Bear Ridge Developers, Inc., PO Box 7097, Incline Village NV 89452-7097 Paul Pettersen, TRPA Senior Planner

132-231-15-3jun97-3